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#### · ABSTRACT

This publication contains student and teacher instructional materials for a course in residential solar systems. The text is designed either as a basic solar course or as a supplement to extend student skills in areas such as architectural drafting, air conditioning and refrigeration, and plumbing. The materials are presented in four units covering the following topics: fundamentals of solar systems; active solar heating systems; load calculations and solar cooling; and passive solar and other solar concepts. Each unit contains a unit objective, specific objectives, suggested activities, and instructional materials, such as an objective sheet, information sheet, transparency masters, assignment sheets, answers to assignment sheets, job sheets, a unit test, and answers to the test. Suggested references are listed, and the units are liberally illustrated. (NC)



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# RESIDENTIAL SOLAR SYSTEMS

by

Dan Fulkerson

Developed by the

Mid-America Vocational Curriculum Consortium, Inc.

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#### **PREFACE**

The concept of using solar energy is not a new one; however, the feasibility of using solar applications on residential structures has only now come of age. With increased emphasis being placed in this area, several problems presently exist in our vocational training programs.

Of paramount importance is the need to find quality instructional materials which are up-to-date, economical, and easy to use, as well as flexible enough to fit into many types of programs.

Residential Solar Systems attempts to solve this problem by presenting highly technical solar system processes in an easy to understand format. The materials are presented in four, well illustrated units, and the assignment and job sheets are practical and fun to do. This text is basically designed to supplement other instructional materials and to extend student skills in areas such as architectural drafting, air conditioning and refrigeration, and plumbing, yet it is complete enough to serve almost any basic solar program.

Progress in residential solar applications is crawling along at a time when the urgency created by diminishing fossil-fuel supplies dictates a need to run. We hope that *Residential Solar Systems* will help students and put advances in solar technology to work in residential America.

Ann Benson
Executive Director
Mid-America Vocational
Curriculum Consortium



#### **ACKNOWLEDGEMENTS**

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We also express appreciation to the U.S. Department of Energy for their many efforts in solar energy research and application and the many excellent publications those efforts have produced. We have utilized much material from the Department of Energy's Solar Energy Project and several of the publications in that series, as well as other materials developed for the Department of Energy under grants and contracts.

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(NOTE: This is an alphabetized list of references used in completing this text.)

Logan, Joe D. Solar Energy: Passive Systems. St. Louis, MO: Milliken Publishing Co., 1980.

Passive Design Ideas for the Energy Conscious Consumer. Rockville, MD 20850: National Solar Heating and Cooling Information Center, 1979.

Sheet Metal and Air Conditioning Contractors National Association. Fundamentals of Solar Heating. Washington, D.C. 20545: U.S. Department of Energy, 1978.

Solar Energy Applications Laboratory, Colorado State University. Solar Heating and Cooling of Residential Buildings, Design Systems, Washington, D.C. 20402: U.S. Department of Commerce, 1977.

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The American Planning Association. Protecting Solar Access for Residential Development: A Guidebook for Planning Officials. Washington, D.C.)20402: U.S. Department of Housing and Urban Development and U.S. Department of Energy, 1979.

#### **ADDITIONAL REFERENCES**

(NOTE: This is an alphabetized list of additional references which would be beneficial as supplemental teaching aids.)

Direct Use of the Sun's Energy. Farrington Daniels; Ballantine Books, 1nc., 457 Hahn Rd., Westminster, MD 21157.

Energy for Survival. Wilson Clark (1974); Doubleday & Co., Inc., 277 Park Ave., New York, NY 10017.

Energy Primer. Portola Institute; Whole Earth Truck Store, 558 Santa Cruz Ave., Menlo Park, CA 94025.



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Illustrated Solar Energy Guide of Flat-Plate Collectors for Practical Home Application. E.I. & I. Associates, P.O. Box 37, Newbury Park, CA 91320. .

Solar Energy and Shelter Design. Bruce Anderson (1973); Total Environmental Action, Church Hill, Harrisville, NH 03450.

Solar Energy for Man. B.J. Brinkworth (1973); John Wiley & Sons, Inc., One Wiley Dr., Somerset, NJ 08873.

Solar Science Projects. D.S. Halacy, Jr.; Scholastic Book Services, 900 Sylvan Ave., Englewood Cliffs, NJ 07632.



#### FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

#### UNIT OBJECTIVE

After completion of this unit, the student should be able to match types of solar systems with their applications, solve problems concerning rules of thumb for collector tilt and collector orientation, and list components of a typical flat plate solar collector. The student should also be able to construct and use a device to measure solar altitude and solar azimuth and evaluate the use of flat black paint in collecting sensible heat. This knowledge will be evidenced by correctly performing the procedures outlined in the assignment and job sheets and by scoring 85 percent on the unit test.

#### SPECIFIC OBJECTIVES -

After completion of this unit, the student should be able to:

- Match terms related to fundamentals of solar systems with their correct definitions.
- 2. Arrange in order the basic sequence of a solar system operation.
- 3. Match types of solar systems with their applications.
- 4. Circle the words which best complete statements concerning elements of solar geometry and their meanings.
- 5. Solve a problem concerning rules of thumb for collector tilt.
- 6. Solve a problem concerning rules of thumb for collector orientation.
- 7. Complete a list of statements concerning components of a typical flat plate collector.
- 8. Complete a list of statements concerning how the "greenhouse effect" makes a flat plate collector absorb heat.
- 9. Solve a problem concerning the efficiency of flat plate collectors.
- 10. List two sensible heat storage mediums.
- 11. Select true statements concerning guidelines for sensible heat storage.
- 12. Select true statements concerning insolation variables to consider in solar system planning.
- 13. Determine collector tilt for specific latitudes.
- 14. Determine collector orientation for specific situations.
- 15. Demonstrate the ability to:
  - a. Construct and use a device to measure solar altitude and solar azimuth.
  - Evaluate the use of flat black paint in collecting sensible heat.



### FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

#### SUGGESTED ACTIVITIES

- I. Provide student with objective sheet.
- II. Provide student with information, assignment and job sheets.
- III. Make transparencies.
- IV. Discuss unit and specific objectives.
- V. Discuss information and assignment sheets.
- VI. Discuss and demonstrate the procedures outlined in the job sheets.
- VII. Invite a local or area architect who has designed a solar application to talk to the class about the advantages and problems with solar systems in your specific locale.
- VIII. Locate a business or residence in your area where a solar system is in use and invite the person most familiar with the system to talk to the class about its performance.
- IX. Check with your local library, nearby university, or community college to find books or other literature about solar, and prepare a list so students will know what reference materials are available in the area.
- X. Arrange a visit to a solar supply house or an area business that manufactures collectors or other solar components and have students make brief reports on what they find there.
- Arrange to have a representative of your state energy department visit the class and talk about the status of solar and other alternative energy efforts within the state.
- XII. Show available films or slide presentations about solar systems.
- XIII. Give test.

#### INSTRUCTIONAL MATERIALS

- I. Included in this unit:
  - A. Objective sheet
  - -B. Information sheet



#### C. Transparency masters

- 1. TM 1-- Liquid Heat Storage Options
- 2. TM 2-- Rock-Bed Heat Storage Unit

#### D. Assignment sheets

- 1. Assignment Sheet #1-Determine Collector Tilt for Specific Latitudes
- 2. Assignment Sheet #2-Determine Collector Orientation for Specific Situations
- E. Answers to assignment sheets
- F. Job sheets
  - 1. Job Sheet #1-Construct and Use a Device to Measure Solar Altitude and Solar Azimuth
  - Job Sheet #2--Evaluate the Use of Flat Black Paint in Collecting Sensible Heat
- G. Test
- H. Answers to test

#### II. References:

- A. Solar Energy Systems. New York, NY 10174: Copper Development Association, Inc., 1979.
- B. Solar Energy Applications Laboratory, Colorado State University. Solar Heating and Cooling of Residential Buildings, Design Systems. Washington, D.C. 20402: U.S. Department of Commerce, 1977.
- C. Passive Design Ideas for the Energy Conscious Consumer. Rockville, MD 20850: National Solar Heating and Cooling Information Center, 1979.
- D. Solar Energy Project, Earth Science Activities. Washington, D.C. 20545: U.S. Department of Energy, 1979.

#### III. Additional references:

(NOTE: These materials would be beneficial as supplemental teaching aids and can be obtained by writing the below listed addresses.)

- A. Solar Science Projects. D.S. Halacy, Jr.; Scholastic Book Services, 900 Sylvan Ave., Englewood Cliffs, NJ 07632.
- B. Energy Primer. Portola Institute; Whole Earth Truck Store, 558 Santa Cruz Ave., Menlo Park, CA 94025.
- C. Direct Use of the Sun's Energy. Farrington Daniels; Ballantine Books, Inc., 457 Hahn Rd., Westminster, MD 21157.



- D. Energy for Survival. Wilson Clark (1974); Doubleday & Co., Inc., 277 Park Ave., New York, NY 10017.
- E. Solar. Energy and Shelter Design. Bruce Anderson (1973); Total Environmental Action, Church Hill, Harrisville, NH 03450.
- F. Solar Energy for Man. B.J. Brinkworth (1973); John Wiley & Sons, Inc., One Wiley Dr., Somerset, NJ 08873.
- G. Illustrated Solar Energy Guide of Flat-Plate Collectors for Practical Home Application. E.I. & I. Associates, P.O. Box 37, Newbury Park, CA 91320.

### FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

#### INFORMATION SHEET

#### Terms and definitions

- A. Absorptivity-The ratio of blar energy absorbed by a surface compared to the total amount of solar energy striking the surface
- B. Glazing-Glass panes or plastic sheets used to cover solar collectors
- Greenhouse effect—The tendency of some transparent materials, such as glass, to both transmit and block radiation, resulting in both direct and indirect heat gain

Example:

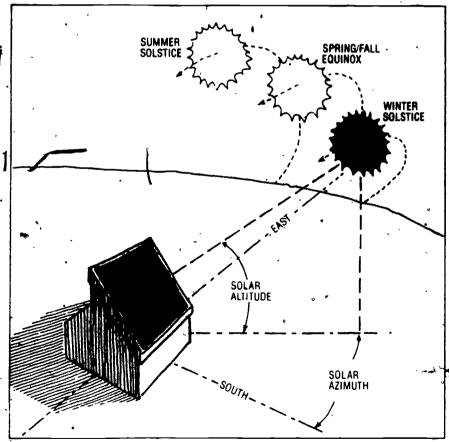
Sunlight shining into a room through a glass window produces a direct heat gain to the immediate area the sun's rays strike, but the radiation is absorbed and stored and also results in an indirect heat gain to adjacent spaces

- D. Heat transfer-The transfer of heat from one substance or region to another
- E. Sensible heat-Heat that can be physically felt of "sensed" or absorbed by a liquid or solid mass
- F. Thermal mass-The potential heat storage capacity of a given substance or system
- G. Insolation-The total solar energy received at any given point on the earth's surface
- H. Diffuse radiation-Portions of the sun's radiation diffused or scattered by atmospheric particles, clouds, and pollutants; accounts for about 45% of total insolation on a bright, clear day
- Direct radiation-The remainder of radiation not reflected, absorbed, or diffused that passes more or less directly to the earth's surface from the sun
- J. Btu-British thermal unit; the amount of heat required to raise the temperature of one pound of water one degree Fahrenheit
- K. Infrared rays--Long-wave rays in solar radiation that are characterized by their heating effect when they strike a surface on the earth
- L. Re-emit--The tendency of a material or substance to discharge infrared rays which it has absorbed; sometimes called re-radiation
- II. Basic sequence of a solar system operation
  - A. Available energy must be collected
  - B. Collected energy must be stored
  - C. Stored energy must be distributed

- III. Types of solar systems and their applications
  - A. Active system-A solar heating or cooling system that uses external mechanical power to move or store solar heat
  - B. Passive system-A solar heating or cooling system that does not use external mechanical power to (move at store solar heat
  - C. Hybrid system-A solar Heating or cooling system which combines both active and passive systems
- IV. Elements of solar geometry and their meanings (Figure 1)
  - A. Solar altitude. The angle of the sun's position in the sky with respect to the earth
  - B. Solar azimuth. The position of the sun with respect to compass directions

(NOTE: Because solar altitude and solar azimuth vary with each day of the year according to latitude, the elements in combination affect both tilt angle and orientation of solar collectors.)

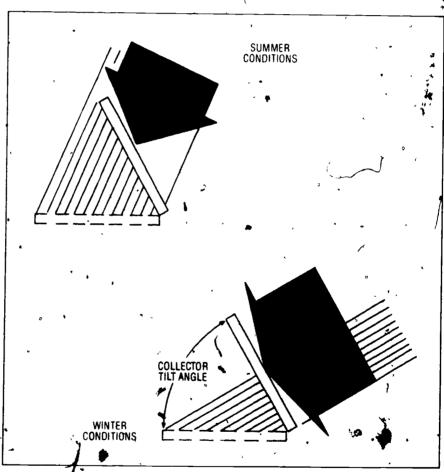
#### FIGURE 1



Courtesy Copper Development Association Inc.

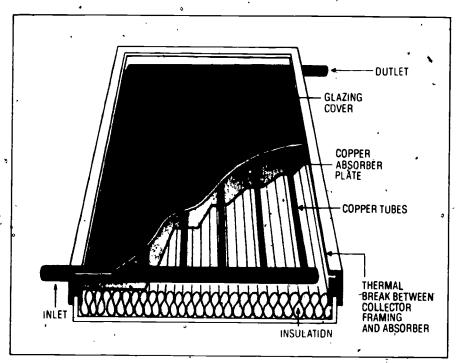
- V. Rules of thumb for collector tilt (Figure 2)
  - A. To collect the most radiation in winter, tilt the collector at an angle equal to the latitude plus 15 degrees
  - B. To collect the most radiation in summer, tilt the collector at an angle equal to the latitude minus 15 degrees
  - C. To collect the most radiation averaged over the year, tilt the collector at an angle approximately equal to the latitude

#### FIGURE 2



- VI. Rules of thumb for collector orientation
  - A. In winter, a south-facing orientation receives more radiation than a southeast or southwest orientation
  - B. In summer, a south-facing orientation receives slightly less radiation than a south-southeast or a south-southwest orientation
  - C. In areas that experience morning haze, peak collection may be experienced by a collector which faces 10 to 15 degrees west of south
- VII. Components of a typical flat plate collector (Figure 3)
  - A. Flat plate collectors typically use liquid as the heat transfer medium
  - B. Flat plate collectors typically have blackened copper cometimes other metals) absorber plates with an integrated or attached array of copper tubes
  - C. Beneath the absorber plate is an insulating material that retards loss of the absorbed heat through the back of the collector panel





VIII. ... How the "greenhouse effect" makes a flat plate collector absorb heat

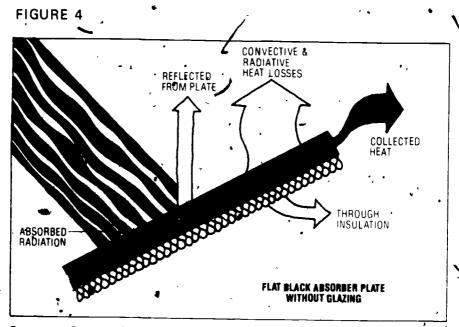
- A. In order to collect as much energy as possible, collectors are often covered with a glazing material of glass or plastic which are highly transparent to incoming solar radiation
- B. These covers serve as insulation over the absorber plate and keep convective heat losses down
- C. Since glass or certain plastics are virtual paque to the outgoing long-wave infrared radiation, the radiation phenomenon in known as the "greenhouse effect"

Example:

Greenhouses function because of the effect, but on a larger scale, the earth itself creates a "greenhouse effect" by absorbing solar radiation and turning it into longer wavelength infrared rays; these longer infrared rays cannot easily pass back through the atmosphere into space because certain substances, like carbon dioxide and water in the atmosphere, absorb them; when this energy is prevented from escaping back into space, the "greenhouse effect" occurs.

IX. Efficiency of flat plate collectors

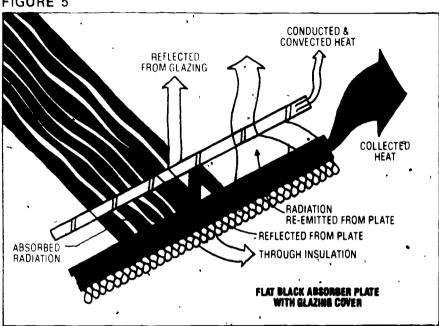
A. In a collector with a flat black absorber plate without glazing, much of the radiation absorbed by the absorber plate is re-emitted or lost from the top surface and some is lost through the back insulation (Figure 4)





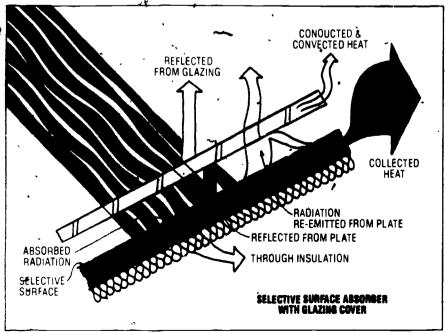
B. In a collector with a flat black absorber plate with glazing cover, the radiation absorbed by the black plate is re-emitted as in the preceding collector, but the glass cover blocks loss of the re-emitted radiation to the outside; there is some loss through conduction and convection, but more heat is retained with a glazing cover (Figure 5)

FIGURE 5



C. In a collector with a selective surface absorber—with glazing cover, a very thin layer of selected material is applied to the top of the absorber plate; since the layer's thickness is approximately equal to the wavelength of the incoming solar radiation, the selective surface re-radiates much less absorbed energy and is more efficient than other types of collectors (Figure 6)

FIGURE 6





- X. Sensible heat storage mediums
  - A. Water

: .

B. Solid materials such as rock, brick, or adobe -

(NOTE: Sensible heat storage is related to the principle of unit heat capacity and the amount of energy required to raise the temperature of a unit volume of a given substance 1°F; although latent heat storage working on the principle of changing the physical properties of a substance would afford smaller solar storage, it is not treated in this unit because the field is still highly experimental; eutectic salts are utilized in latent heat storage, but means of establishing their stability are still being examined.)

#### XI. . Guidelines for sensible heat storage

A. The capacity of sensible heat storage materials is equal to the specific heat of the material times its density (Figure 7)

Example:

Water has a specific heat of 1.0 and a density of 62.5 lb./cu. ft.; therefore, one cu. ft. of water will rise in temperature 1°F when 62.5 Btu is applied

FIGURE 7

| •  | Specific Heat Density<br>BTU/Lb. *R Lb./Rt.* | 81   | STU/R.3/4. |                 |  |
|--|--|------|------------|-----------------|--|
| •  |  |      | No Voids   | 30% Volds       |  |
| Water  | 1.0  | 62.5 | 62.5       | (62.5)          |  |
| Water (30%)—<br>Ethylene Glycol<br>(70%) Mixture<br>(230°F.) | .8   | 64.4 |            |                 |  |
|  | · <del>-</del>                               | 64.1 | 51         | 36              |  |
| Scrap Iron   | 112  | 489  | 55         | 38              |  |
| Magnetite  | 165  | 320  | 53         | 37              |  |
| Scrap Aluminum   | .215   | 168  | 4 36       | 25              |  |
| Concrete   | 27   | 140  | 38 -       | 26              |  |
| Rock (Basalt)  | .20  | 180  | 36         | 25              |  |
| Brick '  | 2  | 140  | 28         | 20              |  |
| Rock Sait (NaCl)<br>(30-70% by weight at 230°F)              | 219  | 136  | 30 *       | 21 <sup>°</sup> |  |



- B. Liquid storage materials are most commonly used with liquid flat plate collectors
- C. Solid storage materials are most commonly used with air flat plate collectors
- D. A larger volume of solid materials is required to attain the same amount of heat storage as water because the specific heat is much lower for solid materials than for water
- E. With solid storage materials, an additional allowance must also be made for the circulation of air around the materials to facilitate heat transfer; this requires a solid-to-void ratio
- F. A common solid-to-void ratio for solid sensible heat storage materials is 70 percent solid to 30 percent void

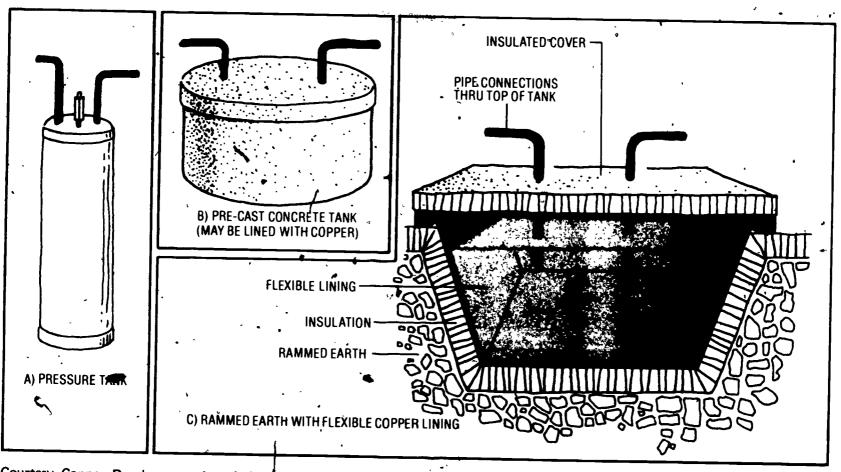
(NOTE: This means that solid heat storage volumes will be two to three times liquid heat storage volumes for the same storage capacity; greater fan motor horsepower is also required to circulate air through a solid storage medium, and larger ductwork is required; these items become important design considerations when selecting a system.)

- G. Liquid systems frequently use storage containers made of pre-cast concrete, concrete block, pressure-preserved wood, or rammed earth, and most site-built storage tanks have flexible liners to prevent leaks (Transgarency 1)
- H. For liquid storage, the most appropriate storage size is 1 1/2 gallons of water per square foot of collector
- 1. Rock-bed storage should be sized to provide 50 to 100 pounds of rock per square foot of collector, and the rock size should be .75 to 1.5 inches; these sizes insure that the interior of individual rocks can be heated and a good heat flow maintained
- J. Rock-bed storage bins can be constructed of wood or pre-cast concrete, but they should be properly sized, insulated, waterproofed against the intrusion of ground water, and sealed with a sealant that will hold up in the high operating temperatures (Transparency 2)
- XII. Insolation variables to consider in solar system planning
  - A. Latitude-Over the course of a year, latitude has the greatest single effect on insolation received at any location
  - B. Cloud cover-Brings about the greatest day to day variation in insolation at any particular locality, and is the least predictable of any of the pariables
  - C. Atmospheric turbidity--Haze, smoke, fog, or dust that contributes to the reduction in the transparency of the atmosphere and a reduction in insolation

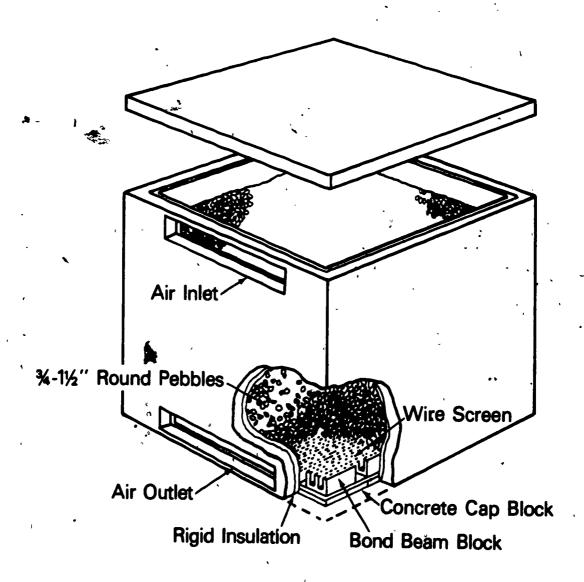


- D. Altitude-Increased altitude increases the amount of insolation received
- E. Obstructions Nearby trees and tall buildings can block off the direct rays of sunlight during part of the day, and even if they do not directly block the rays, they may interfere with diffused radiation that would otherwise be received
- F. Orientation of the land surface--It is good to remember that most insolation data is for a horizontal surface; planning for sloping sites requires appropriate modifications in data, especially if the slopes are north-facing

# **Liquid Heat Storage Options**



# **Rock-Bed Heat Storage Unit**



Courtesy U.S. Department of Energy





#### FUNDAMENTÀLS OF SOLAR SYSTEMS . UNIT I

# ASSIGNMENT SHEET #1-DETERMINE COLLECTOR TILT FOR SPECIFIC LATITUDES

| A. | Determine collector tilt for an application designed to collect the most radiation in winter at a latitude of 40°N              |
|----|---|
|    | Answer  |
| B. | Determine collector tilt for an application designed to collect the most radiation in summer at a latitude of 32°N              |
|    | Answer  |
| C. | Determine collector tilt for an application designed to collect the most radiation averaged over the year at a latitude of 36°N |
|    | Answer  |
|    |   |

# FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

# ASSIGNMENT SHEET #2-DETERMINE COLLECTOR ORIENTATION FOR SPECIFIC SITUATIONS

| A.         | For an application designed to collect the most radiation in winter, should the collect tor be oriented facing south, southeast, or southwest?      | C.     |
|------------|---|--------|
|            | Answer 4  |        |
| <b>B</b> . | For an application designed to collect less radiation in summer, should the collector b oriented facing south, south-southeast, or south-southwest? | Эе     |
| -          | Answer  |        |
| c.         | For an application in an area that experiences morning haze, should the collector be oriented due south or 10 to 15 degrees west of south?          | ت<br>ز |
|            | Answer  | -      |
|            |   | å      |

### FUNDAMENTALS OF SOLAR SYSTEMS

ANSWERS TO ASSIGNMENT SHEETS

Assignment Sheet #1

- A. 55° B. 17° C. 36°

Assignment \$heet #2

- A.
- В.
- South South 10 to 15 degrees west of south

### FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

### JOB SHEET #1-CONSTRUCT AND USE A DEVICE TO MEASURE SOLAR ALTITUDE AND SOLAR AZIMUTH

- I. Tools and materials
  - A. Small pegboard
  - B. 3/8-inch wood dowels
  - C. Magnetic compass
  - D. Bubble level
  - E. Clock or watch
  - F. Paper and pencil
  - G. Straightedge
  - H. Protractor

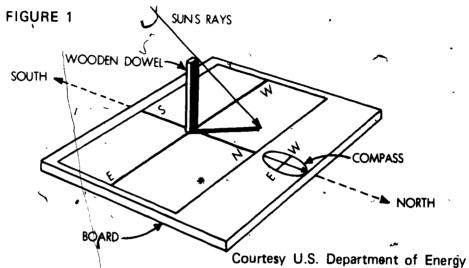
#### Procedure

- A. Locate the mid-point of one long edge of the pegboard
- B. Place the dowel into the hole six rows in from the mid-point
- C. Place a piece of paper on the board by pushing it down over the dowel (Figure 1)
- D. Remove the paper from the board
- E. Draw two lines on the paper so that both lines pass through the center of the hole with one line parallel to the long side of the paper and one line parallel with the short side of the paper (Figure 1)
  - (NOTE: These two lines should be perpendicular to each other, at right angles or 90°.)
- F. Mark the ends N-S, E-W to show compass directions to use in lining the board (Figure 1)
- G. Set the board in a horizontal position where it will receive the direct rays of the sun most of the day



#### **JOB SHEET #1**

H. Align the board with the compass as shown in Figure 1



- I. Use the bubble level to check that the board is level; if needed, level the board
- J. Measure and record the height of the dowel above the top surface of the board
- K. Begin at zero minutes, and at each 15 minute interval, draw a line on the paper showing the position of the shadow

(NOTE: Be careful to mark the end of the shadow accurately; since positions of the shadows are needed throughout the day, students from other classes may have to work with previously collected data.)

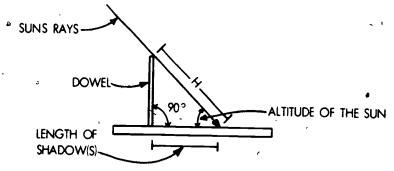
L. Record the time and date for each shadow drawn

(NOTE: The time should be in increments of 15 minutes.)

#### **JOB SHEET #1**

- M. Measure the angles of solar altitude and solar azimuth with the following procedure:
  - 1. The first angle is the angle between the shadow (s) on the paper and the slanting angle (H) of the triangle as shown in Figure 2; this angle is called the solar altitude

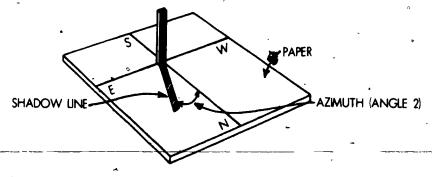
#### FIGURE 2



Courtesy U.S. Department of Energy.

- 2. On a separate sheet of paper, draw a right angle triangle so that the vertical side is equal to the dowel height and the horizontal side is equal to the shadow length
- 3. Drawiline (H) and measure angle 1, then record date, time, and altitude of the sun, in degrees, on the diagram
- 4. The second angle tells how much east or west of the N-S line the sun is; this angle is called the solar azimuth (Figure 3)

#### FIGURE 3



Courtesy U.S. Department of Energy



5. Measure angle 2, and record it directly on the apparatus

(NOTE: Angle 2 in Figure 3 should be recorded as approximately 30W because the actual position of the sun is west which causes the shadow to be cast to the east; if the actual position of the sun were in the east and the shadow fell the same number of degrees to the west, angle 2 in Figure 3 would be recorded as 30°E; remember that the actual position of the sun is the directional reference for the solar azimuth.)

N. Prepare a data table for the sun's positions, and enter the information in the following chart:

| Date: Sun's Altitude in degrees  Time Sun's Altitude in degrees  |     |
|--|-----|
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# JOB SHEET #1

| 1.             | At what time of day is the sun's shadow shortest?  |
|----------------|--|
| 2.             | What does this mean?   |
| 3.             | If you wanted to collect the most energy from the sun, how w you position a solar collector?   |
| <b>4.</b>      | Since most collectors are fixed, which direction should a colle in your area face for best year-round performance?   |
|                |  |
|                | (NOTE: Consider when you are likely to need the most heat.)  |
| <b>.</b><br>5. | (NOTE: Consider when you are likely to need the most heat.)  Could you use your collected data for helping determine the window placement for a home in your locale? |
| ,              | Could you use your collected data for helping determine the  |

.3\*\*

# FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

# JOB SHEET #2-EVALUATE THE USE OF FLAT BLACK PAINT IN COLLECTING SENSIBLE HEAT

| l        | Too              | ls and materials   |
|----------|------------------|--|
| •        | A.               | Small can of flat black paint  |
|          | В.               | Paintbrush -   |
| <u> </u> | C.               | Paint thinner for cleaning brush   |
|          | D.               | Clean towel  |
|          | <b>. E.</b>      | Two 3-pound coffee cans, with plastic lids   |
|          | F.               | Thermometer  |
| 11.      | Proc             | edure .  |
|          | _A.              | Paint the outside of one of the coffee cans and plastic lids with flat black paint and allow the paint to dry  |
|          | <b>В</b> .       | Fill the two coffee cans almost full with equal amounts of water and put the lids on   |
|          | <b>C.</b>        | Place the two cans in direct sunlight far enough apart that one will not shade the other   |
| }        | D.               | Allow the two cars to sit in direct sunlight for at least four hours   |
|          | , <b>E.</b><br>, | Record the outdoor temperature at the end of the testing period  |
| •        | F.               | Take the two cans inside, remove the lids, and check the temperature of the water in each can  |
|          |                  | Unpainted can Painted can '  |
|          | G.               | Express the value of the addition of flat black paint to the one can by comparing the water temperature inside the two cans; the addition of flat black paint affects collection and storage of sensible heat (circle one) |
|          |                  | Not at all Enough to notice Significantly  |
|          | H.               | Clean work area and discuss your findings with your instructor   |

## FUNDAMENTALS OF SOLAR SYSTEMS UNIT I .

1.

|          | NAME  |     | •                 |
|----------|---|-----|-------------------|
|          | TEST  |     |                   |
| Match th | e terms on the right with their correct definitions.  |     |                   |
| a.       | The ratio of solar energy absorbed by a surface compared to the total amount of solar   | 1.  | Insolation        |
|          | energy striking the surface   | 2.  | Absorptivity      |
| b.       | Glass panes or plastic sheets used to cover solar collectors  | 3.  | Sensible heat     |
| c.       | The tendency of some transparent materials,   | 4.  | Glazing           |
| -        | such as glass, to both transmit and block radiation, resulting in both direct and indirect heat gain  | 5.  | Greenhouse effect |
| . d.     | The transfer of heat from one substance   | 6.  | Direct radiation  |
|          | or region to another  | 7.  | Thermal mass      |
| e.       | Heat that can be physically felt or "sensed" or absorbed by a liquid or solid mass  | 8.  | Diffuse radiation |
| f.       | The potential heat storage capacity of a given substance or system  | 9.  | Heat transfer     |
| g.       | The total solar energy received at any given  | 10. | Re-emit           |
|          | point on the earth's surface  | 11. | Infrared rays     |
|          | Portions of the sun's radiation diffused or scattered by atmospheric particles, clouds, and pollutants; accounts for about 45% of total insplation on a bright, clear day | 12. | Btu               |
| i.       | The remainder of radiation not reflected, absorbed, or diffused that passes more or less directly to the earth's surface from the sun                                     |     |                   |
| ا        | British thermal unit; the amount of heat required to raise the temperature of one pound of water one degree Fahrenheit  | -   |                   |
| k.       | Long-wave rays in solar radiation that are characterized by their heating effect when they strike a surface on the earth  |     | 7                 |

The tendency of a material or substance to discharge infrared rays which it has absorbed;

sometimes called re-radiation

| 2.          | Arrange correct s       | in order the basic sequence of a solar system equence number in the appropriate blank.   | operation by placing the                                 |
|-------------|-------------------------|--|--|
| 0           | a.                      | Collected energy must be stored  | . •  |
|             | b.                      | Stored energy must be distributed  |  |
|             | C.                      | Available energy must be collected   | •  |
| 3.          | Match the               | e types of solar systems on the right with their corre   | ect applications.  |
|             | a.                      | A solar heating or cooling system that uses external mechanical power to move or store solar heat  | <ol> <li>Hybrid system</li> <li>Active system</li> </ol> |
| 4           | b.                      | A solar heating or cooling system that does not use external mechanical power to move or store solar heat  | 3. Passive system  |
|             | c.                      | A solar heating or cooling system which combines both active and passive systems   | •  |
| 4.          | Circle th<br>of solar g | e words which best complete the following stater ecometry and their meanings.  | ments concerning elements.                               |
|             |                         | ar altitudeThe angle of the sun's position in the sk<br>ctions, the earth)   | y with respect to (compass                               |
|             | b. Sola<br>tion         | ar azimuthThe position of the (sun, earth) with  | respect to compass direc-                                |
| <b>/</b> 5. | sy <b>ste</b> m a       | e following problem concerning rules of thumb<br>at 42°N latitude needs a collector that will collect<br>conths. What would be the best collector tilt?    | for collector tilt: A solar the most radiation during    |
|             |                         |  |  |
| 6.          | A south                 | e following problem concerning rules of thumb-<br>facing collector is not collecting enough winter<br>ollector indicates all components are in good shape? | r radiation; an inspection                               |
| 7.          | Complet                 | e the following list of statements concerning compo  | onents of a typical flat plate                           |
|             | a. Fla                  | t plate collectors typically use liquid as the   |  |
|             |                         | t plate collectors typically have<br>integrated or attached array of copper tubes  | absorber plates with                                     |
|             |                         | neath the absorber plate is an insulating material bed heat through the back of the  | that retards loss of the ab-                             |



| . Co              | omplete the following list of statements concerning how the "greenhakes a flat plate collector absorb heat.  | ouse effect"               |
|-------------------|--|----------------------------|
| a.                | In order to collect as much energy as possible, collectors are often coglazing material of glass or plastic which are highly transparent   | vered with a to incoming   |
| b.                | These covers serve as insulation over the absorber plate and keep down   |                            |
| c.                | Since glass or certain plastics are virtually opaque to the outgoir infrared radiation, the radiation is trapped inside the this phenomenon is known as the "greenhouse effect"  | ng long-wave<br>and        |
| ) abs             | olve the following problem concerning the efficiency of flat plate canning a solar system installation, it is found that collectors with a selesorber with glazing cost very little more than collectors with flat blaces with glazing; which type of collector should be chosen for the system. | ctive surface              |
|                   |  | •                          |
|                   |  | <del>.</del>               |
| . Lis<br>a.<br>b. | st two sensible heat storage mediums.  | <u> </u>                   |
| . Sel             | lect true statements concerning guidelines for sensible heat storage "X" in the appropriate blanks. a. The capacity of sensible heat storage materials is equal to the spetthe material times its volume   |                            |
| **********        | b. Liquid storage materials are most commonly used with liquid collectors  | d flat plate               |
|                   | c.` Solid storage materials are most commonly used with air flat plan  | te col <del>lect</del> ors |
|                   | d. A large volume of solid materials is required to attain the same heat storage as water because the specific heat is much high materials than for water  | amount of er for solid     |
|                   | e. With solid storage materials, an additional allowance must be more circulation of air around the materials to facilitate heat transfer; a solid-to-void ratio   | nade for the this requires |
|                   | f. A common solid-to-void ratio for solid sensible heat storage ma percent solid to 30 percent void  | terials is 70              |
| .—                | g. Solid systems frequently use storage containers made of pre-ca concrete block, pressure-preserved wood or rammed earth, and built storage tanks have flexible liners to prevent leaks   | st concrete,<br>most site- |
|                   |  | •                          |

ERIC Full Text Provided by ERIC

ξ.

|     |  | h. For liquid storage, the most appropriate storage size is 1/2 gallon of water per square foot of collector  |  |
|-----|--|---|--|
|     |  | i. Rock-bed storage should be sized to provide 50 to 100 pounds of rock per square foot of collector, and the rock size should be .75 to 1.5-inches; these sizes insure that the interior of individual rocks can be heated and a good heat flow maintained |  |
|     |  | j. Rock-bed storage bins can be constructed of wood or pre-cast concrete, but they should be properly sized, insulated, waterproofed against the intrusion of ground water, and sealed with a sealant that will hold up in the high operating temperatures  |  |
| 12. |  | ct true statements concerning insolation variables to consider in solar system ning by placing an "X" in the appropriate blanks.  |  |
|     |  | _a. Latitude Over the course of a month, latitude has the greatest single effect on insolation received at any location   |  |
|     | ` <u> </u>   | b. Cloud cover-Brings about the greatest day to-day variation in insolation at any particular locality, and is the least predictable of any of the variables  |  |
| •   |  | c. Atmospheric turbidityHaze, smoke, fog, or dust that contributes to the reduction in the transparency of the atmosphere and a reduction in insolation   |  |
|     |  | _d. Altitude-Increased altitude decreases the amount of insolation received   |  |
| ş   |  | e. ObstructionsNearby trees and tall buildings can block off the direct rays of sunlight during part of the day, and even if they do not directly block the rays, they may interfere with diffused radiation that would otherwise be received               |  |
| ,   |  | f. Orientation of the land surfaceIt is good to remember that most insolation data is for a vertical surface; planning for sloping sites requires appropriate modifications in data, especially if the slopes are south-facing                              |  |
| 13. | Dete   | ermine collector tilt for specific latitudes.   |  |
| 14. | Determine collector orientation for specific situations. |   |  |
| 15) | Den  | nonstrate the ability to:   |  |
|     | a.   | Construct and use a device to measure solar altitude and solar azimuth.   |  |
| •   | b.   | Evaluate the use of flat black paint in collecting sensible heat.   |  |
|     |  | (NOTE: If these activities have not been accomplished prior to the test, ask your   |  |

instructor when they should be completed.)

## FUNDAMENTALS OF SOLAR SYSTEMS UNIT I

#### ANSWERS TO TEST

- 1. a. 2 e. 3 i. 6 b. 4 f. 7 j. 12 c. 5 g. 1 k. 11 d. 9 h. 8 l. 10
- 2. a. 2 b. 3
  - c. 1
- 3. a. 2 b. 3
- c. 1
- 4. a. The earth
  - b. Sun
- 5. 57°
- 6. Reorienting the collector to the southeast or southwest
- 7. a. Heat transfer medium ...
  - b. Blackened copper
  - c. Collector panel
- 8. a. Solar radiation
  - b. Convective heat losses
  - c. Collector
- The collectors with selective surface absorbers should be chosen because they are the
  most efficient and the slight difference in cost will be justified by collector performance
- 10. a. Water
  - b. Solid materials such as rock, brick, or adobe
- 11. b, c, e, f, i, j
- 12. b, c, e
- 13. Evaluated to the satisfaction of the instructor
- 14. Evaluated to the satisfaction of the instructor
- 15. Performance skills evaluated to the satisfaction of the instructor

### ACTIVE SOLAR HEATING SYSTEMS UNIT II

#### UNIT OBJECTIVE

After completion of this unit, the student should be able to discuss basic solar systems used for domestic water heating and space heating, and list the functions of heat pumps in active solar heating systems. The student should also be able to solve problems concerning solar domestic water heating and solar space heating and be able to construct a working model solar water heater. This knowledge will be evidenced by correctly performing the procedures outlined in the assignment and job sheets and by scoring 85 percent on the unit test.

#### SPECIFIC OBJECTIVES

After completion of this unit, the student should be able to:

- 1. Match terms related to active solar heating systems with their correct definitions.
- 2. Complete a list of statements concerning characteristics of a thermo-syphon domestic hot water system:
- 3. Circle the words which best complete statements concerning characteristics of a pumped circulation domestic hot water system with heat exchanger.
- 4. Select true statements concerning characteristics of a pumpéd circulation domestic hot water system with freeze control.
- 5. Select true statements concerning characteristics of a pumped circulation domestic hot water system with draindown.
- 6. List two arrangements for domestic hot water storage tanks.
  - 7. Complete a list of statements concerning characteristics of dual domestic hot water tanks.
- -
- 8. Circle the words which best complete statements concerning characteristics of a single storage domestic hot water tank.
- 9. Select true statements concerning characteristics of a combined solar space and domestic hot water system.
- 10. Complete a list of statements concerning characteristics of a water collection, water storage, air distribution space heating system.
- 11. Distinguish between a series configuration and a parallel configuration in water collection, water storage, water distribution space heating systems.
- 12. Complete a list of ways radiant panels are used in water collection, water storage, water distribution space heating systems.



- 13. Select true statements concerning characteristics of an air collection, solid material storage, air distribution space heating system.
- 14. Complete a list of characteristics of water collection, water storage, heat pump distribution space heating systems.
- 15. Distinguish between an air-to-air heat pump and a water-to-air heat pump function in a solar space heating system.
- 16. Select true statements concerning steps in the operation of an air-to-air heat pump in a solar heating system.
- 17. Select true statements conterning steps in the operation of a water-to-air heat pump in a solar heating system.
- 18. Circle the words which best complete statements concerning design considerations for piping systems.
- 19. Select true statements concerning design considerations for corrosion protection.
- 20. List four other considerations for corrosion protection.
- 2 to the a problem concerning design considerations for collector cover glazing.
- 22. Complete a list of statements concerning requirements for absorber plate insulation.
- 23. Solve a problem concerning high temperature protection and its applications.
- 24. Complete a list of statements concerning rules of thumb for circulating pumps and solar system controls.
- 25. Solve problems concerning solar domestic water heating systems.
- 26. Solve problems concerning solar space heating systems.
- 27. Demonstrate the ability to construct a working model solar water heater.

## ACTIVE SOLAR HEATING SYSTEMS UNIT II

#### SUGGESTED ACTIVITIES

- I, Provide student with objective sheet.
- II. Provide student with information, assignment, and job sheets.
- III. Make transparencies.
- IV. Discuss unit and specific objectives.
- V. Discuss information and assignment sheets.
- VI. Discuss and demonstrate the procedures outlined in job sheet.
- VII.  $^{\mathcal{O}}$  Send for a copy of Solar Energy Systems to use as a teaching aid; write to:

Copper Development Association, Inc. 1011 High Ridge Road Stamford, CT 06905

(NOTE: Much of the information and many of the illustrations in this unit were taken from this publication.)

- VIII. Have a local or area architect who has designed a solar system bring the plans to class and discuss planning procedures, system selection, system installation, and system maintenance.
  - IX. Read Job Sheet #1 carefully and arrange to borrow the required chemical glassware and support equipment from a local high school or college chemistry department.
  - X. Nave a solar dealer bring a solar collector to the classroom, talk about its component structure, and demonstrate its efficiency.
- XI. Invite a solar systems dealer to bring solar components such as valves, solenoids, sensors, and dampers to class and talk about their fabrication requirements and their functions within a solar system.
- XII. Give test.

#### INSTRUCTIONAL MATERIALS

- I. Included in this unit:
  - A. Objective sheet
  - **B.** Information sheet



#### C. Transparency masters

- 1. TM 1--Pressurized Thermo-Syphon DHW System
- 2. TM 2--Pumped DHW System with Heat Exchanger
- 3. TM 3--Pressurized Pumped DHW System with Freeze Control
- 4. TM 4-Pumped Circulation DHW System with Draindown
- 5. TM 5-- Dual DHW Storage Tanks
- 6. TM 6--Single DHW Storage Tank
- 7. TM 7--Combined Solar Space Heating and DHW System
- 8. TM 8-Water Collection, Water Storage, Air Distribution Space Heating System
- TM 9--Water Collection, Water Storage, Water Distribution Space Heating System
- 10. TM 10-Water Collection, Water Storage, Solar Radiant Heating
- 11. TM 11--Air Collection, Solid Material Storage, Air Distribution Space Heating System
- 12. TM 12-Water Collection, Water Storage, Air-to Air Heat Pump Distribution Space Heating System
- 13. TM 13--Water Collection, Water Storage, Water-to-Air Heat Pump Distribution Space Heating System

#### Assignment sheets

- 1. Assignment Sheet #1-Solve Problems Concerning Solar Domestic Water Heating Systems
- 2. Assignment Sheet #2\*Solve Problems Concerning Solar Space Heating Systems
- E. Answers to assignment sheets
- F. Job Sheet #1-Construct a Working Model Solar Water Heater
- G. Test
- H. Answers to test

#### II. References:

- A. Solar Energy Systems. New York, NY 10174: Copper Development Association, Inc., 1979.
- B. Sheet Metal and Air Conditioning Contractors National Association. Fundamentals of Solar Heating. Washington, D.C. 20545: U.S. Department of Energy, 1978.



- C. Solar Energy Applications Laboratory, Colorado State University. Solar Heating and Cooling of Residential Buildings, Sizing, Installation, and Operation of Systems. Washington, D.C. 20545: U.S. Department of Energy, 1977.
- D. Solar Energy Project, Reader. Washington, D.C. 20545: U.S. Department of Energy, 1979.
- E. Solar Energy Project, Text. Washington; D.C., 20545: U.S. Department of Energy, 1979.
- F. Solar Energy Project, Earth Science Activities. Washington, D.C. 20545: U.S. Department of Energy, 1979.

## ACTIVE SOLAR HEATING SYSTEMS UNIT II

#### INFORMATION SHEET

#### Terms and definitions

ł.

- A. Aggréssive water--Highly mineralized local water supplies that have high levels of dissolved sulfates and chlorides and high PH values
- B. DHW-Domestic hot water
- C. Thermo-syphon--The circulation of water between a tank and a collector maintained by the natural convection currents that are set up when water is heated
- D. Heat exchanger--A device that absorbs heat and then releases it to complete the heat transfer process
- E. Toxic--Containing poison
- F. Nontoxic--Free of poison
- G. Loop-A pipe configuration designed to complete a liquid flow from one given point to another with interconnections among components in a system
- H. Solenoid-A valve which mechanically or electronically starts, stops, or diverts flow in a system
- I. Sensor-A device which functions as a thermostat to detect changes in temperature; its on-off functions can be set for minimum low or maximum high temperatures
- J. One-way check valve--A valve which permits flow in one direction only and prevents flow back to the source
- K. Tandem -- Working side by side or together
- L. Auxiliary storage--A standby or backup storage facility that permits storage of hot water that exceeds the capacity of the prime or system storage facility
- M. Auxiliary heat--A standby or backup gas or electric heating system programmed to automatically maintain heating load requirements when the solar system fails to meet the required load demands
- N. Heat sink-Body which is capable of accepting, storing, and releasing heat
- O. Corrosion--The eating away or wearing away of metals, especially metals in contact with chemicals
- P. Dissimilar metals--Any two metals that have different properties



- Q. Electrolysis-An electro-chemical reaction that causes deterioration when two dissimilar metals come in contact
- R. Dielectric-An electric insulator used to control electrolysis at points where dissimilar metals meet
- S. Closed system--A solar system into which no air penetrates or from which no air can be expelled
- T. Open system-A solar system into which air can penetrate or from which air can be expelled for draindown or to create a syphon effect
- U. PH-A symbol for the degree of acidity or alkalinity of a solution; PH is measured on a scale of 0, indicating highest acidity, to 14, indicating highest alkalinity
- V. Outgassing-The tendency of certain insulating materials to release elements of their original composition, especially when exposed to high temperatures
- W. Damper-A mechanical device, sometimes electronically activated, to stop or moderate flow within a system
- II. Characteristics of a thermo-syphon DHW system (Transparency 1)
  - A. Most basic of solar water heating systems
  - B. Circulation of water between tank and collector is maintained by natural convection currents set up when water is heated
  - C. Requires no heat exchanger
    - (NOTE: Because there is no heat exchanger, the same water that circulates, through the collector will later appear at the hot water tap.)
  - D. When the water in the solar collector becomes hotter than the water in the storage tank, it rises to the tank as the colder tank water drops into the collector supply line
  - E. When no water is being run at a tap, circulation will continue until tank and collector temperature are equalized
  - F. Rate of flow cannot be controlled
  - G. Difficult to provide freeze protection, and system is therefore most appropriate for regions that do not reach freezing temperatures
- III. Characteristics of a pumped circulation DHW system with heat exchanger (Transparency 2)
  - A. Collector water is pumped through a closed pipe loop incorporating a heat exchanger which is immersed in a storage tank



- B. The closed collector pipe loop must have an expansion tank and a separate \*pressure relief valve in addition to the valve on the tank
- C. Because collected heat must be transferred through a heat exchanger, the collection fluid must be hotter; this makes the system somewhat less efficient than one in which domestic water circulates directly through the collector
- D. A check valve in the collector return prevents migration of heat from tank to collector by thermo-syphon action on cold nights
- E. Because collector water and domestic water do not intermingle, an antifreeze solution can be added to the collector water for low-temperature protection

(NOTE: Check applicable codes for the use of nontoxic and toxic antifreeze solutions; single-wall heat exchangers may be required with nontoxic antifreeze, and double-wall heat exchangers may be required with toxic antifreeze to provide a double barrier between the toxic antifreeze and potable water.)

- IV. Characteristics of a pumped circulation DHW system with freeze control (Transparency 3)
  - A. System employs a pump but does not use a heat exchanger
  - B. Collector circuit is not sealed off from stored water, and antifreeze cannot be used
  - C. Freeze protection is provided by pumping water through the system with a rate of flow high enough to prevent freezing
  - D. A three-way solenoid valve is the key control element in a pumped circulation system
  - E. During normal operation, the solenoid valve allows water to circulate freely between tank and collector
  - F. During normal operation, no cold water is admitted to the system unless a hot water tap is opened in the building, in which case makeup water enters from the supply source
  - G. In freezing temperatures, the solenoid valve automatically cuts off the storage tank and diverts water from the collector into a dry well or sump, setting up a constant flow of water from the source throught the collector circuit and into the sump
- V. Characteristics of a pumped circulation DHW system with draindown (Transparency 4)
  - A. System incorporates a circulating pump for collector water, but does not employ a heat exchanger



- B. System employs a temperature sensor affixed to the bottom of the absorber plate
- C. When the sensor detects a drop to about 40°F, it initiates closing of the motorized valve in the collector supply
- D. When the motorized valve reaches a fully closed position, it trips an end switch which in turn trips the solenoids of both the dump valve and the air intake valve
- E. Water then drains freely from the collector circuit and out of the system
  - (NOTE: This drain off is usually no more than two or three gallons, but it does protect all piping exposed to freezing temperatures.)
- F. Pressurized source water is prevented from flowing to the collector by means of a motorized valve in the supply line and a one-way check valve in the return line
- G. When absorber plate temperature rises to a preset difference above storage, the motorized valve begins to open, the circulating pump restarts, and the dump valve and inlet valve close
- H. As the collector circuit refills, trapped air is relieved through the automatic vent and normal circulation of collector water is resumed
- VI. Arrangements for DHW storage tanks
  - A. Dual solar and conventional tanks
  - B. Single storage tanks
  - C. Combined solar space and DHW heating systems
- VII. Characteristics of dual DHW tanks (Transparency 5)
  - A larger tank is connected to the collector loop and stores hot water from the collector
  - B. In tandum with the larger tank is a conventional water heater with a fossilfuel burner or an electric heating element
  - \*C. The outlet pipe of the solar storage tank is connected to the cold or inlet line of the conventional heater
  - D. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap
  - E. When the solar-heated water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat



- F. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or electrode
- G. This configuration allows only the relatively cold water to circulate through the collector, and this permits the collector to function at a higher efficiency
- VIII. Characteristics of a single storage DHW tank (Transparency 6)
  - A.\* Can provide both solar and auxiliary storage in the same tank
  - B. When this system is used, a large tank should be selected
  - C. The thermostat of the auxiliary fuel input should be set to maintain a tank temperature of about 110-120°F
    - D. Because the lowest temperature of water that can be circulated back through the collector is 110°F, collector efficiency is lowered
  - IX. Characteristics of a combined solar space and DHW system (Transparency 7)
    - A. Water is heated and stored in a solar storage tank
    - B. Makeup water for hot water supply passes through a heat exchanger in the solar storage tank
    - C. If the solar storage tank temperature is high enough, cold domestic makeup water passing through will pick up sufficient heat to avoid drawing energy from the domestic water heater
    - **5**. When the temperature of the domestic water tank drops below the storage tank temperature, the domestic water is pumped through the heat exchanger, transferring whatever heat is available
    - E. When required, an auxiliary heat supply may be programmed to supplement DHW requirements

(NOTE: There are many variations of combination space and water heating systems; sometimes the heat exchanger is placed in the DHW storage tank, and it is also possible to combine a space heating system with a two-tank DHW system.)

- X. Characteristics of a water collection, water storage, air distribution space heating system (Transparency 8)
  - A. These systems have found wide acceptance because they are simple to operate and control
  - B. The circulating pump in the collector loop operates whenever collector temperature is higher than the temperature of the storage tank water by a preset amount



- C. When the pump stops, water in the collectors and pipe lines drains into the storage tank
- D. To permit the automatic draining process, the return pipe must be coupled to the tank in such a fashion that the end of the pipe is kept above the level of the stored water or the pipe must be vented by some other means
- E. When the building thermostat calls for heat, a pump circulates stored water through the heat exchanger coil in the return air duct upstream of the furnace
- F. As water is being circulated through the heat exchanger, the furnace fan begins to draw air through the heat exchanger coil and forces the warmed air into the building
- G. As long as the coil continues to maintain supply air temperature high enough, the furnace heating element remains off, but when solar supplied heat falls short of preset temperature settings, the furnace comes on to furnish supplementary heat

(NOTE: The placement of thermostats or two-stage thermostats provides several variations, in the system described above, and some of these will be discussed in a following objective.)

- XI. Differences between a series configuration and a parallel configuration in water collection, water storage, water distribution space heating systems
  - A. These systems are highly suited for fin tube and radiant panel installations
  - B. One configuration for this system is that heat can be supplied by either the solar system or the auxiliary boiler working in series
  - C. Another configuration for this system is that heat can be supplied by both the solar system and the auxiliary boiler working in *parallel*
  - D. In a series configuration, when the solar storage tank is hot enough to supply the heating load, water is pumped from the storage tank through the finned tubes and bypasses the boiler (Transparency 9)
  - E. In a series configuration, if the storage tank is not hot enough to supply the heating load completely, water is pumped through the boiler and then into the finned tubes, bypassing the storage tank

(NOTE: It is not advisable to pump water from the storage tank, through the boiler, and then through the finned tubes; this would actually use more auxiliary energy and defeat the purposes of the solar component.)

F. In a parallel configuration, if the heating requirement can be supplied by the water from the solar tank, the auxiliary boiler does not operate (Transparency 9)



- G. In a parallel configuration, when more heat is required than the solar system can supply alone, the boiler kicks in to supplement the solar heat
- H. The parallel configuration permits lower temperature water in the solar system to be used to supply a portion of the heating load and actually contributes to higher collector efficiency and more usable solar energy
- XII. Ways radiant panels are used in water collection, water storage, water distribution space heating systems (Transparency 10)
  - A. Radiant panel heating systems employ copper tubes embedded in concrete floor slabs and in wall and ceiling construction
  - B. Floor installations are the most common with copper coils embedded in concrete with one inch or more of concrete above the tubes and never less than an inch of concrete below the tubes
  - (NOTE: For slab or grade construction, insulation is imperative beneath the slab; it is also important to insure that ground water will not carry away heat.)
    - C. Ceiling and wall panels are usually embedded in plaster
  - D. Wall panel installations require heavy insulation to reduce heat loss to the ouside

(NOTE: Centering coils between rooms or floors is not recommended because it usually results in poor heat transfer and lack of room temperature control.)

- XIII. Characteristics of an air collection, solid material storage, air distribution space heating system (Transparency 11)
  - A. When heat is available for collection, but there is no heat demand in the house, the collector circulation fan begins to draw air down through the storage container
  - B. Motor operated damper number 3 is open whenever the collector fan is operating and closed at all other times
  - C. The top portion of the storage container contents will heat first, and the heat will extend downward as more energy is collected

(NOTE: Motor operated damper number 4 is normally open.)

D. When no heat is being collected, but is called for in the building, the centrifugal fan in the auxiliary heating system begins operation and signals dampers 1 and 2 to open

(NOTE: These dampers are closed unless the centrifugal fan is working.)



- E. Return air is drawn upward through the storage container, exits at maximum temperature, and is circulated through the building
- F. When the heating load cannot be supplied by the solar system, the auxiliary heating system comes on
- G. When there is a simultaneous collection of energy and demand for heat by the building, motor operated damper 4 is closed

(NOTE: Damper 4 is open unless both collection and distribution fans are operating simultaneously.)

H. Air is circulated directly from the collector to the building

(NOTE: Air-rock systems do have limitations that require special design considerations; these will be covered in a later objective.)

- XIV. Characteristics of water collection, water storage, heat pump distribution space heating systems
  - A. The electrically driven heat pump enhances the flexibility and efficiency of solar systems
  - B. A heat pump has the capability of extracting heat from a cooler source and increasing it to a higher temperature, thereby increasing the thermal gradient
  - C. A heat pump can extract useful heat from the solar storage system even when the temperature has failen below room temperature
- XV. Differences between an air-to-air heat pump and a water-to-air heat pump function in a solar space heating system
  - A. In an air-to-air heat pump, when heating is required, the heat pump extracts heat from one air source (usually the outside air), increases its temperature, and warms the room air (Transparency 12)
  - B. In a water-to-air heat pump, when heating is required, the heat pump extracts heat from the storage water, increases its temperature, and warms the room air (Transparency 13)
- XVI. Steps in the operation of an air-to-air heat pump in a solar heating system (Transparency 12)
  - A. All solar heating is done directly from storage without the aid of the heat pump, but the heat pump fan is used to circulate room air over the heat exchange coil
  - B. If heat available from solar storage is insufficient, the heat pump begins to operate, supplying additional heat to the air



C. Although this does not permit stored solar energy to be used below) the space temperature, it greatly reduces operational time of the heat pump and saves much electricity that would otherwise be used to operate the heat pump composition.

(NOTE: There are other configurations in using a heat pump with a solar system; some permit the heat pump to extract heat from water or solid storage at temperatures below the room temperature, but these systems are complex and require many automatic controls.)

XVII. Steps in the operation of a water-to-air heat pump in a solar heating system (Transparency 13)

- A. When the solar storage tank temperature is over a preset point (usually 90°F), storage is used directly for space heating with the heat pump fan circulating the room air over the solar water coil
- B. When the storage tank temperature falls below the temperature needed for heating, the control valve changes position and circulates the storage water into the heat pump
- C. When the water flow to the heat pump has been proven by a flow switch, the heat pump compressor begins to operate, extracting heat from the water and increasing its temperature; it is then used for warming room air
- D. This procedure continues until the heating load has been satisfied or storage tank temperature drops to the lower operating limits of the heat pump (usually about 60°F)
- E. Sometimes, other water supplies of appropriate temperature can be used when usable heat in the solar storage tank has been exhausted
- F. An auxiliary heat supply is usually required with a water-to-air heat pump solar system

XVIII. Design considerations for piping systems

- A. Corrosion is the biggest enemy of piping systems and other solar components
- B. It is imperative, from a corrosion standpoint that the fluid passages in the absorber plate be compatible with the materials used for piping, storage tank, pump, and valve bodies
- C. All piping should be pitched from the high point of the system to insure complete drainage when necessary
- D. In systems with drainage as freeze protection, the piping should be pitched at a minimum of 1/8 inch per 1 foot of run to insure that fluid will drain completely



E. Start up of all liquid-carrying systems should include a flushing operation to remove dirt and debris accumulated during fabrication and installation

(NOTE: Follow manufacturer's recommendations carefully when flushing systems which use a heat transfer fluid other than water.)

- XIX. Design considerations for corrosion protection
  - A. Corrosion protection has three major concerns in metal collector systems:
    - 1. Corrosion between dissimilar metals
    - 2. Use of corrosive liquids
    - 3. Presence of air in the system
  - B. When dissimilar metals are used in the presence of moisture, corrosion can occur; this is true even of copper when used with another metal
    - Example: If copper tubes are used to connect aluminum collectors, the collectors soon develop pits in the aluminum fluid tubes and leaks develop
  - C. In a solar system with a circulating fluid, it is not sufficient simply to use dielectric fittings to separate dissimilar metals and control electrolysis
    - Example: Copper ions can be carried by the fluid and deposited on other metal and cause pitting
  - D. Although it is difficult to exclude bronze valves and pump impellers from collector systems, as a general rule, it is best not to mix metals

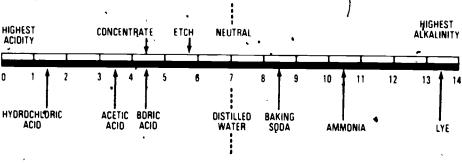




XX. Other considerations for corrosion protection

A. Check the local water supply for PH level (Figure 1)?

(NOTE: Some areas have "aggressive" waters which are highly mineralized, have a high level of dissolved sulfates and chlorides, have PH values above 7.3, high carbon dioxide content, and the presence of dissolved oxygen gas.) FIGURE 1



(Courtesy A. B. Dick)

- B. A trouble free history of copper plumbing in the locality can usually be taken as evidence that the water is not aggressive to copper, but it may be aggressive to other metals
- C. When there is a question concerning the presence of aggressive water, the water should be chemically analyzed, and a treatment engineer should be consulted to prescribe ways to make and keep the water nonaggressive
- D. When satisfreeze or special heat transfer fluids are added to the water, it increases the potential for corrosion
- E. Anti-freezes which are propylene glycol (nontoxic) or ethylene glycol (toxic) based are the two major types of anti-freeze used with water in solar collectors
- F. Propylene glycol is claimed to be nontoxic and should be used in DHW systems unless a double walled heat exchanger is employed
- G. Anti-freeze solutions usually require the addition of corrosion inhibitors and buffers for PH, and all anti-freeze solutions should be monitored and replenished as required
- XXI. Design considerations for collector cover glazing (Figure 2)
  - A. When using glass cover plates, tempered glass with ground edges should be specified and recommendations for maximum permissable spans should be carefully followed



B. When two glass plates are hermetically sealed, they must have the same physical characteristics

Example: A 3/32-inch-thick glass inner plate should not be used with a 3/16-inch-thick tempered cover plate; this would exert substantial internal pressure on the glazing

- C. Thin sheets of plastic film can be used for cover plates in certain applications and offer the advantage of light weight, low cost, and increased fracture resistance
  - D. Plastic selected should have proven long-term resistance to ultraviolet radiation breakdown
  - E. Additional cover layers reduce heat loss, but there is a point where additional glazing actually diminishes collector efficiency

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| MATERIAL                 | THICKNESS<br>(INCHES) | SOLAB ENERGY<br>NRANSMISSION<br>(%) | MAXIMUM<br>OPERATING<br>TEMP (°F) |
|--------------------------|-----------------------|-------------------------------------|-----------------------------------|
| Clear Lime               | . 1/8                 | 85 0                                | <del></del>                       |
| Float Glass              | 3⁄16<br>1.4           | 81 Q<br>78 0                        | - 40C                             |
| Water White              | ```                   | 04.0                                |                                   |
| ,                        | 18                    | 91 0                                | 400                               |
| Crystal (Low Iron) Glass | 3 16<br>1 4           | 90 5<br>, 90 0                      | 400                               |
| 100% Acpriic             | 1 8                   | 89 0                                |                                   |
| Poloriese Cast           | 3-16                  | 87 0                                | 190                               |
| Sheet                    | , 14                  | . 85 0                              | ,                                 |
| Polycarbonate            | 1.8                   | 81 0                                |                                   |
|                          | 3 16                  | 78 0                                | 270                               |
|                          | 14                    | 74 0                                |                                   |
| Tedlar Film              | 0 004                 | 93 5                                | 227                               |
| Filon 388                | 0 060                 | 82 0                                | <del></del>                       |
| (Flat) 548               | 0 030                 | 86 0                                | 220                               |
| 608                      | 0 080                 | 77 0                                |                                   |
| Teflon Film              | 0 002                 | 97 0                                | 400                               |
| Mylar Film               | 0 001                 | 95 0                                | 220                               |
| Kalwali Sunlight Regular | 0 025                 | 93 0                                | 140                               |
| *                        | 0 040                 | 86 0 .                              | 140                               |
| Lexan Film               | 0 005                 | 94 0                                | 270                               |
|                          | 0 007                 | 93 0                                |                                   |



#### XXII. Requirements for absorber plate insulation

- A. Since absorber plates frequently reach temperatures of more than 200°F, they must be insulated to maximize energy collection from the plate
- B. The back of the collector is typically insulated with a 3 to 4-inch thick fiberglass blanket.
- C. Most foamed urethane insulation currently available undergoes volumetric expansion, at temperatures over 250°F and should be used with care, if at all
- D. Other insulations have problems with the outgassing of volatile elements which can lead to corrosion and other collector problems
- E. Insulation selected should be evaluated according to application needs (Figure 3)

|                                    | INSULATION  |                  |                           |  |
|------------------------------------|-------------|------------------|---------------------------|--|
| FIGURE 3                           | FIBERGLASS  | URETHANE         | EXTRUDED POLYSTYRENE FOAM |  |
| Heat Loss                          | Good        | Excellent        | Excellent                 |  |
| Moisture<br>Resistance             | Fair        | Excellent        | Excellent                 |  |
| Volatile<br>Outg <del>assing</del> | Excellent   | Poor             | Fair                      |  |
| Temperature<br>Resistance          | Excellent   | Fair             | Poor                      |  |
| Desirability                       | Recommended | Not Recommended* | Not Recommended*          |  |

<sup>\*</sup>Not recommended for high temperature application Courtesy Copper Development Association Inc. .

#### XXIII. High temperature protection and its applications

A. Should fluid circulating through an absorber plate stop while the sun is shining, the solar collector can reach temperatures high enough to damage it; this condition is known as stagnation

(NOTE: To avoid collector damage, the collector frame, piping connections, and insulation must be able to withstand high temperatures.)

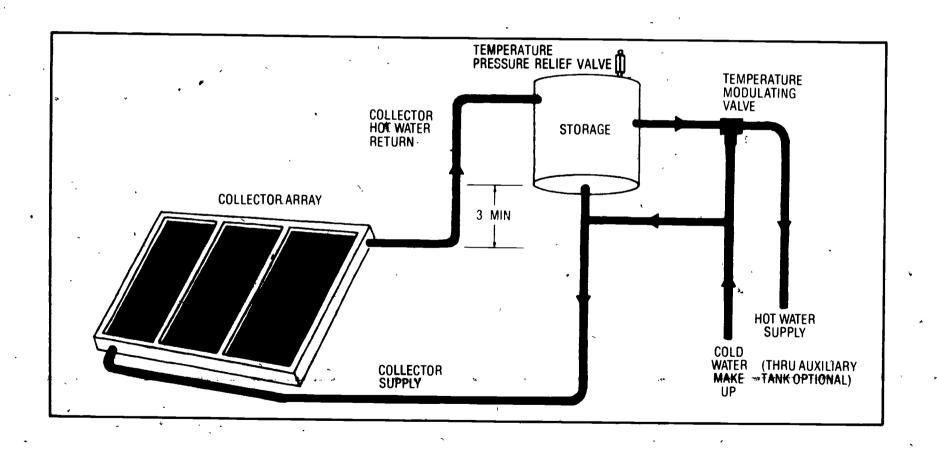
- B. When cooler fluid is pumped into a collector in a condition of stagnation, the resulting thermal shock can cause the collector to buckle and the glazing to break
- C. High temperature protection serves to solve problems of stagnation and thermal shock in several ways:
  - One method uses a temperature sensor on the back of the collector plate to actuate a cutout relay in the power supply to the circulating pump; when the collector plate reaches a preselected temperature, power to the pump is cut off preventing circulation of the collector fluid



- 2. Another method employs a timing device that prevents automatic restarting of the pump in the event of a power failure lasting more than a minute or two
- 3. Still another method employs a temperature sensor to prevent pump operation when a preset temperature differential exists between the collector plate and the circulating fluid
  - (NOTE: This is an expensive method and is seldom used in residential applications.)
- XXIV. Rules of thumb for circulating pumps and solar system controls.
  - A. Pumps ordinarily selected for residential and small solar applications should be centrifugal types with mechanical shaft seals or totally sealed units
  - B. Pumps may be close-coupled, in-line, or base-mounted
  - C. Pump should have a proper-combination of flow rate and lift characteristics for the application
    - (NOTE: Typically, a pump should provide a flow rate of one to three gallons of water per hour, per square foot of collector surface.)
  - D. In open systems, pumps must have sufficient lifting capacity to raise water from the storage tank to the top of the collector
    - (NOTE: In closed systems which have high lifting requirements and low flow quantitites, two small pumps connected in series may be a better alternative to overcome friction losses through the piping.)
  - E. In most small solar systems, the pumps will not exceed 1/4 to 1/3 horse-power and may be as small as 1/6 to 1/20 horsepower in closed systems
  - F. When centrifugal pumps are used, it is essential that they operate with a net positive suction head
    - (NOTE: This can be accomplished by connecting the pump through the storage tank wall below the water level in the tank; this means there will always be a positive head of water in the tank above the pump.)
  - G. The circulating pump in the collector loop is normally started or stopped by means of a differential temperature control which actuates the collector pump when the collector temperature is higher than the tank water temperature, and shuts the collector pump off when the collector water temperature approaches the tank temperature

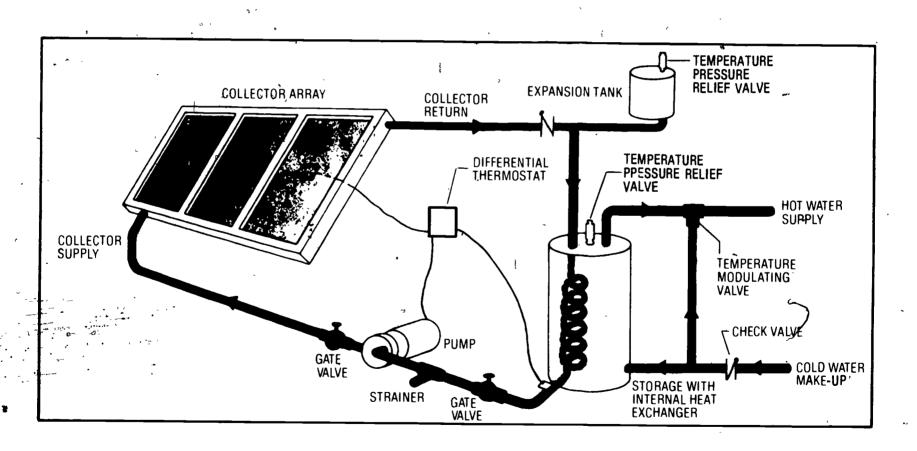


# **Pressurized Thermo-Syphon DHW System**





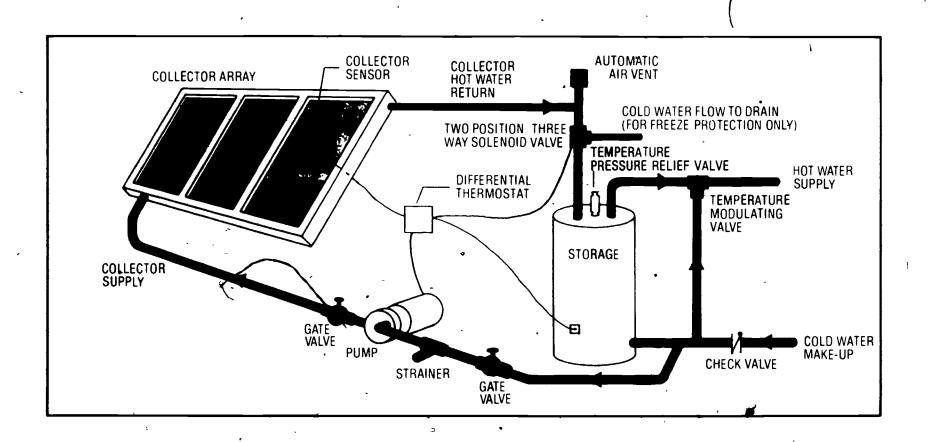
# **Pumped DHW System with Heat Exchanger**



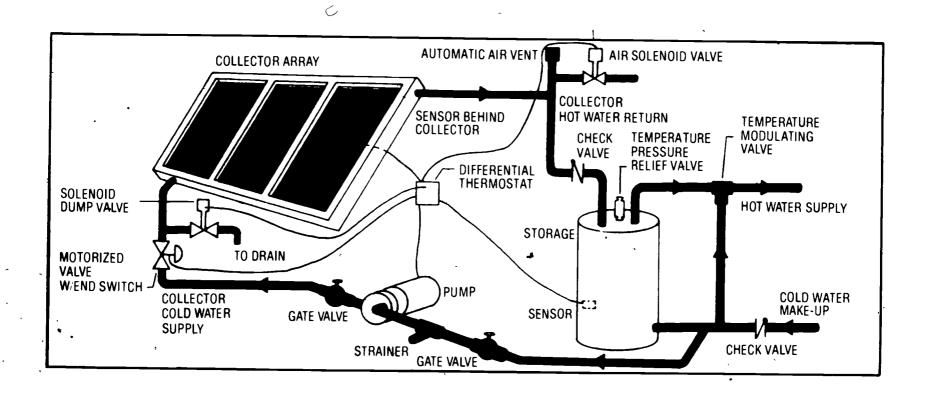




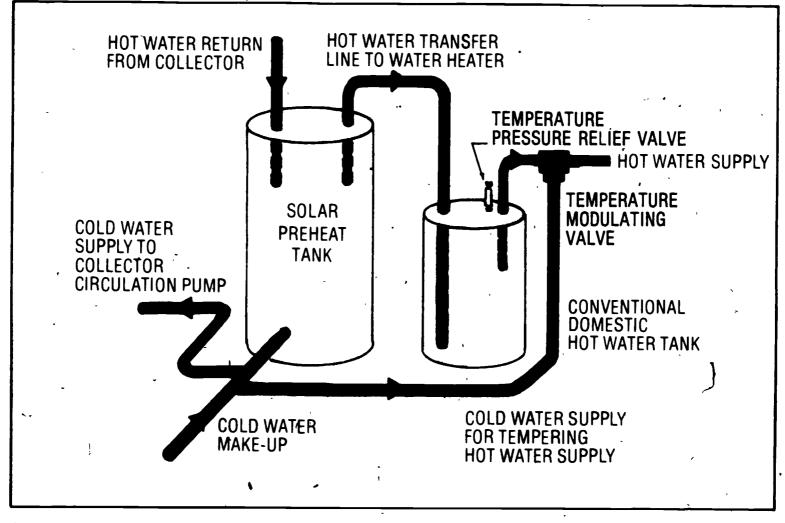
## Pressurized Pumped DHW System with Freeze Control



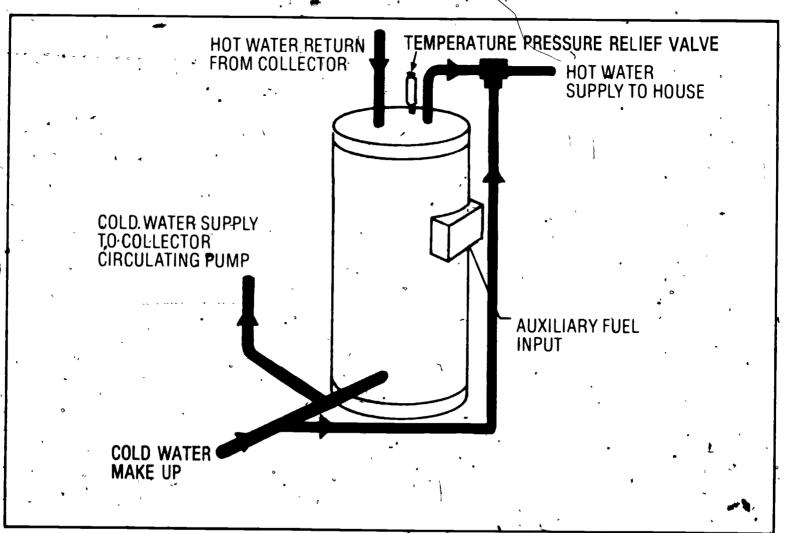
# Pumped Circulation DHW System with Draindown



## **Dual DHW Storage Tanks**



# Single DHW Storage Tank

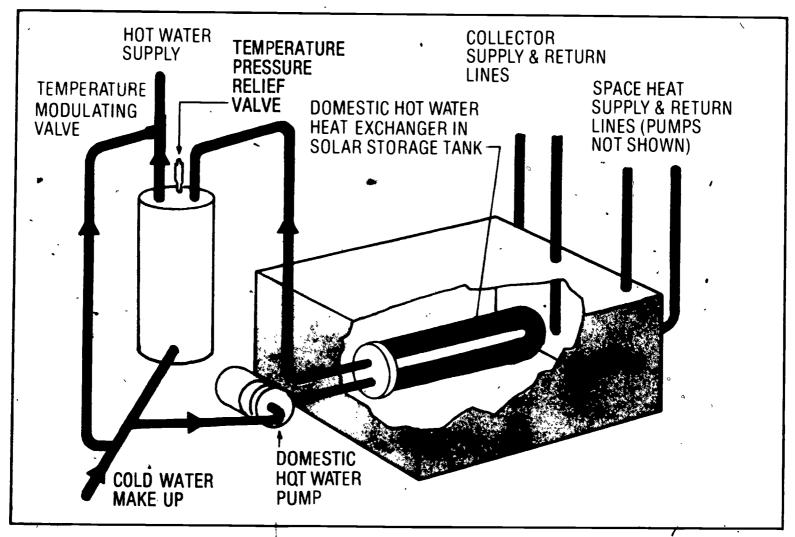


Courtesy Copper Development Association Inc.

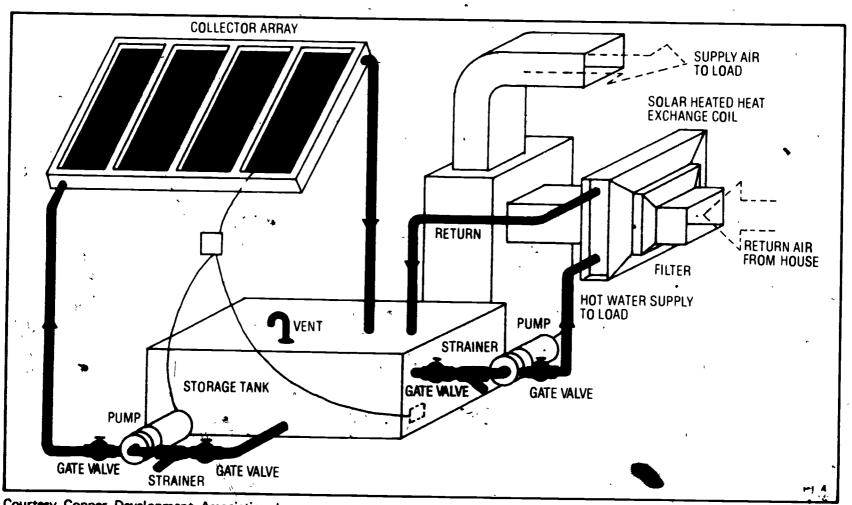
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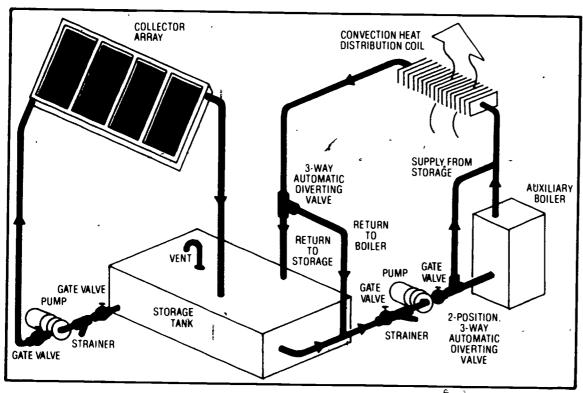
# **Combined Solar Space Heating and DHW System**



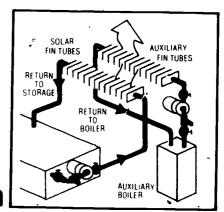
# Water Collection, Water Storage, Air Distribution Space Heating System



# Water Collection, Water Storage, Water Distribution Space Heating System

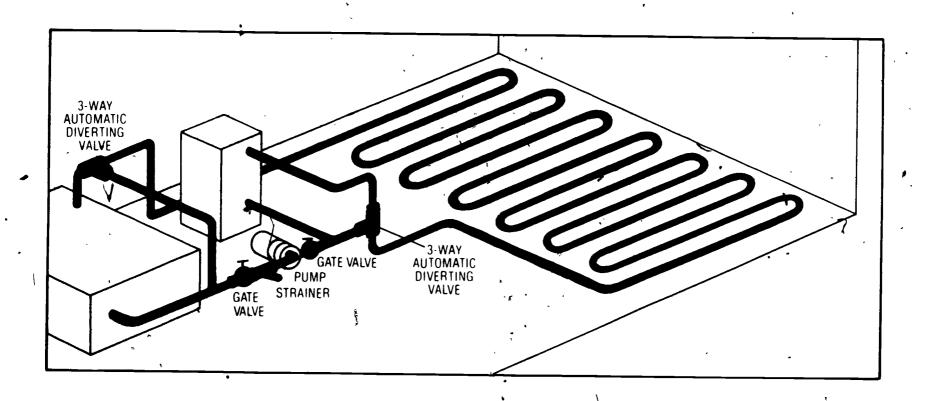


**Series Configuration** 

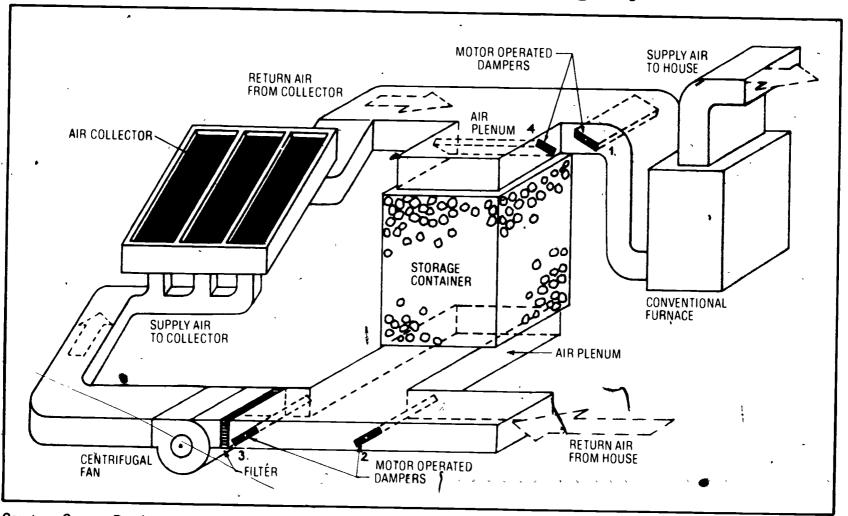


**Parallel Configuration** 

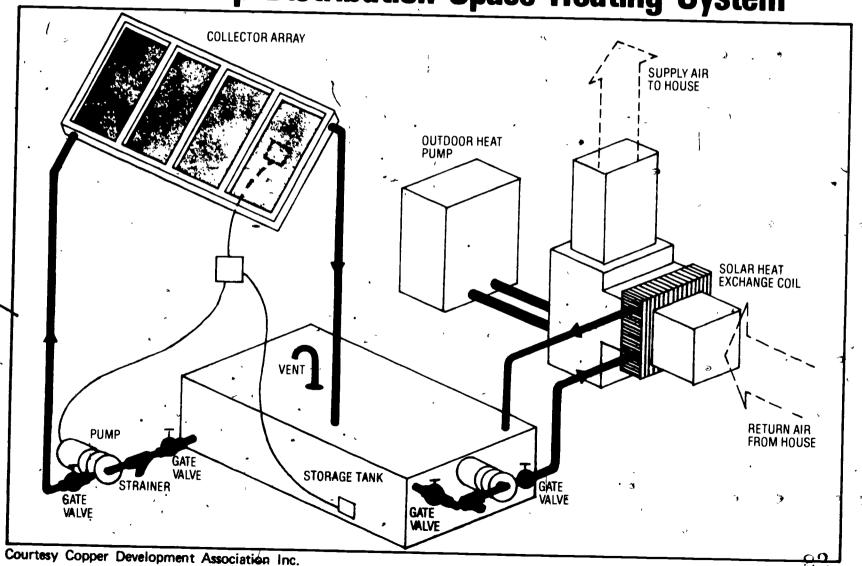
# Water Collection, Water Storage, Solar Radiant Heating



# Air Collection, Solid Material Storage, Air Distribution Space Heating System



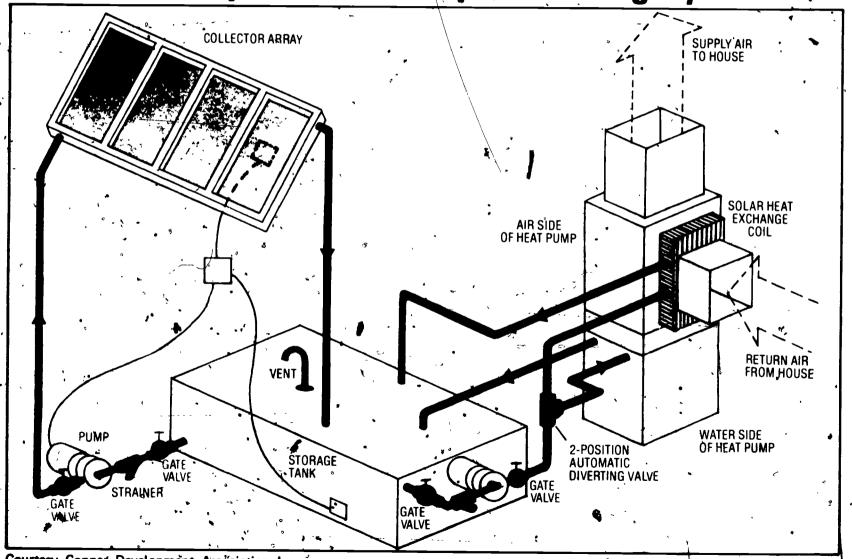
Water Collection, Water Storage, Air-to-Air Heat Pump Distribution Space Heating System



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## Water Collection, Water Storage, Water-to-Air **Heat Pump Distribution Space Heating System**



## ACTIVE SOLAR HEATING SYSTEMS UNIT II

## ASSIGNMENT SHEET #1--SOLVE PROBLEMS CONCERNING . SOLAR DOMESTIC WATER HEATING SYSTEMS

| A:   | What would be the least expensive solar domestic water heating system in a situation where hot water demands are medium, as opposed to high, and in a region where temperatures do not reach the freezing point?  Answer |
|------|--|
| В. Ţ | What can be added to collector water to provide low-temperature protection in a sola domestic hot water heating system employing pumped circulation with a heat exchanger?   |
| •    | Answer   |
| · C. | In a solar domestic hot water heating system that employs pumped circulation with freeze control, antifreeze cannot be used; how is freeze protection provided?  Answer  |
| D.   | Single storage solar domestic hot water tanks are practical because they provide bot solar and auxiliary storage in the same tank, but what precaution should be taken whe planning such a system?  Answer               |
| E.   | Certain configurations of dual solar domestic hot water tanks allow only relatively col-<br>water to circulate through the collector; does this afford higher or lower collector<br>efficiency?                          |
| *    | Answer   |
|      | ,  |



## ACTIVE SOLAR HEATING SYSTEMS UNIT II

## ASSIGNMENT SHEET #2-SOLVE PROBLEMS CONCERNING SOLAR SPACE HEATING SYSTEMS

| Α. | wide acceptance because it is simple to operate and control?   |
|----|--|
|    | Answer   |
| В. | A heat pump has the capability of extracting heat from a cooler source and increasing it to a higher temperature; how does this capability affect a water collection water storage, heat pump distribution space heating system? |
|    | Answer   |
| C. | Where are radiant panels most frequently installed when they are used in a water collection, water storage, water distribution space heating system?   |
|    | Answer   |
| D. | What happens in an air collection, solid material storage, air distribution space heating system when the heating load demands cannot be met by the solar system?  |
|    | Answer   |

# ACTIVE SOLAR HEATING SYSTEMS UNIT II

## ANSWERS TO ASSIGNMENT SHEETS

## Assignment Sheet #1

- A. A thermo-syphon system
- B. Antifreeze
- C. By pumping water through the system with a rate of flow high enough to prevent freezing
- D. A large tank should be selected
- E. Higher efficiency

## Assignment Sheet #2

- A. A water collection, water storage, air distribution system
- B. The heat pump can extract useful heat from the solar storage system even when the temperature has fallen below room temperature
- C. Slab floors
- D. The auxiliary heating system comes on

# ACTIVE SOLAR HEATING SYSTEMS UNIT II

## JOB SHEET #1-CONSTRUCT A WORKING MODEL SOLAR WATER HEATER

- I. Tools and materials
  - A. 1 shallow cardboard box
  - B. 1 sheet of glass large enough to cover the box
  - C. 20 feet of black rubber subing
  - D. 1 ring stand
  - E. 1 large clamp
  - F. 1 condensation column
  - G. 1 pinch-cock
  - H. 1 Celsius thermometer
  - 1. 1 50 millititer (ml) beaker
  - J. 1 cork stopper
  - K. 1 funnel
  - L. 1 can of flat black paint and a paintbrush
  - M. Paint thinner and a clean cloth

(NOTE: The ring stand, clamp, condensation column, pinch-cock, beaker, stopper, and funnel should be available in the chemistry department at your local high school.)

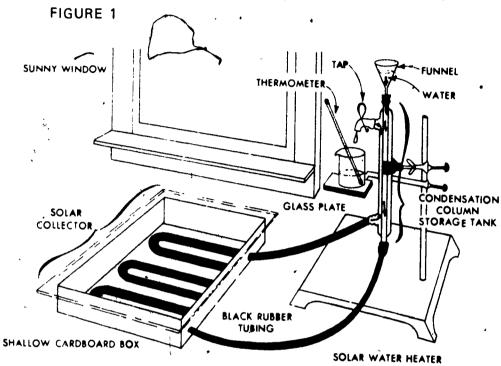
## II. Procedure

A. Assemble the apparatus for your solar water heater according to the diagram in Figure 1

## **JOB SHEET #1**

B. Fill the entire unit with water (Figure 1)

(NOTE: Be sure the tubing, combination condensation column, and storage tank are completely filled.)



Courtesy U.S. Department of Energy

- C. Drain off 50 ml of water from the tap and record the temperature on the data chart that accompanies this job sheet
- D. Pour the water back into the funnel
- E. Place your cardboard box solar collector in the sun and record the temperature of the water each minute for a period of 20 minutes

(NOTE: This means you will have to draw a water sample from the system for each check, but be sure to pour each sample back into the system.)

- Record your data on the data chart
- G. Drain the entire system
- H. Paint the cardboard box black and allow it to dry
- 1. Clean the paintbrush while you are waiting for the paint to dry
  - Repeat steps B through F with the black cardboard box solar collector

# JOB SHEET #1 DATA CHART

| UNPAINTED BOX: | INITIAL | WATER | TEMPERATURE |  |
|----------------|---------|-------|-------------|--|
|                |         |       |             |  |

| TEMP. READING   | MINUTE #                         | TEMP. READING   |
|-----------------|----------------------------------|---|
|                 | 11                               |   |
| ,               |                                  | ,   |
|                 |                                  |   |
|                 | i                                |   |
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| , ,             |                                  |   |
| EMP   REAUING   | MINUIE #                         | TEMP READING  |
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| •               | 12                               |   |
|                 | , 1                              | •   |
|                 | 12                               |   |
|                 | 12.                              |   |
|                 | 12<br>13<br>14<br>15             |   |
|                 | 12<br>13<br>14                   |   |
|                 | 12<br>13<br>14<br>15<br>16<br>17 |   |
|                 | 12<br>13<br>14<br>15<br>16       |   |
|                 |                                  | 11 12 13 14 15 16 17 18 19 20 TED BOX: INITIAL WATER TEMPERATURE TEMP. READING MINUTE # |

# JOB SHEET #1

| Κ  | Rec        | ord your d          | lata on the                  | data chart | . 3                |            | ı          |                        |              | 1        |
|----|------------|---------------------|------------------------------|------------|--------------------|------------|------------|------------------------|--------------|----------|
| L. | Drai       | n the ent           | ire system                   |            |                    |            |            |                        |              |          |
| M. | Retu       | urn tool <b>s</b> a | ınd materia                  | ls to prop | er <b>s</b> torage | area       |            |                        |              |          |
| N. | Ans        | wer the fo          | llowing que                  | stions:    |                    | ,          |            | •                      |              |          |
| 4  | 1.         | Why sho             | uld a <i>black</i>           | rubber tul | be be use          | d in this  | activity?  |                        |              |          |
|    | 2.         | How did             | painting t                   | he collect | or box t           | olack aff  | ect the te | mperature              | of the       | water?   |
|    |            |                     |                              |            | • ,                |            |            |                        |              | 1        |
|    |            |                     | <b>_</b>                     |            |                    | •          | •          |                        |              | <u> </u> |
|    | <b>3</b> . | •                   | rt of the s                  | •          | uld be ti          | ne same    | as the co  | ld water               | supply       | pipe in  |
|    | ,*         |                     | •                            | •          | •                  |            | ٠,         | ,                      |              |          |
|    | 4.         |                     | aratus you'v<br>also be call |            |                    |            | peen terme | d <sup>ń</sup> a solar | water h      | neater"  |
| •  | ,<br>5.    | Èxplain             | your an <b>sw</b> e          | r to quest | tion 4             | ` <u>'</u> | <b>4</b> . | t                      | ,            |          |
| -  | •          | ,                   | 2                            |            |                    | , ,        | •          | _                      |              |          |
| •  | 6.         |                     | least two to                 | • •        |                    | do to in   | nprove the | efficience             | <del></del>  | ne solai |
|    | •          | <del>,</del>        | ,                            | *          | · · ·              |            |            |                        | <del>.</del> |          |
|    | ^          | •                   |                              | <u></u>    | •                  | ,          | ,,         | ,                      | •            | ) **     |

## ACTIVE SOLAR HEATING SYSTEMS UNIT II

NAME

| •  | TEȘT  | •           | ,                      |
|--|---|-------------|------------------------|
| Match th                                     | e terms on the right with their correct definitions.  |             |                        |
| a.   | Highly mineralized local water supplies that have high levels of dissolved sulfates   | 1.          | Auxiliary heat         |
|  | and chlorides and high PH values  | 2.          | Corrosion              |
| b.   | Domestic hot water  | 3.          | РН                     |
| c:   | The circulation of water between a tank and a collector maintained by the natural   | 4.          | Nontoxic               |
|  | convection currents that are set up where water is heated   | 5.          | Tandem                 |
| d.   | A device that absorbs heat and then releases it   | 6.          | Aggressive water       |
|  | to complete the heat transfer process   | 7.          | Heat exchanger         |
|  | Containing poison   | 8.          | Damper                 |
|  | Free of poison  | <b>_ 9.</b> | Open system            |
| g.   | A pipe configuration designed to complete a figure flow from one given point to another   | 10.         | DHW :                  |
|  | with interconnections among components in a system  | 11.         | Toxic                  |
| h.   | A valve which mechanically or electronically starts, stops, or diverts flow in a system   | 12.         | One-way check<br>valve |
| i.   | A device which functions as a thermostat to detect changes in temperature; its on-off functions can be set for minimum low or maximum high temperatures                         | 13.         | Sensor                 |
| j.   | A valve which permits flow in one direction only and prevents flow back to the source   |             |                        |
| <u>.                                    </u> | Working side by side or together  | , .         | n                      |
| <u></u>                                      | A standby or backup storage facility that permits storage of hot water that exceeds the capacity of the prime or system storage facility-                                       | \$          | •                      |
| m.   | A standby or backup gas or electric heating system programmed to automatically maintain heating load requirements when the solar system fails to meet the required load demands | ;<br>3      | ·                      |
|  |   | ~           |                        |

1.

|      | n,     | Body which is capable of accepting, storing, and releasing heat  | 14.             | Outgassing                             | •          |
|------|--------|--|-----------------|--|------------|
|      | 0.     | The eating away or wearing away of metals,   | 15.             | Thermo-sypl                            | non        |
|      |        | especially metals in contact with chemicals  | 16.             | Loop .                                 |            |
|      | _p.    | Any two metals that have different properties  | 17.             | Closed sypho                           | on         |
| `    | q.     | An electro-chemical reaction that causes deterioration when two dissimilar metals  | 18.             | Solenoid                               | -          |
| •    |        | come in contact  | 19.             | Electrolysis                           | , ,        |
|      | r.     | An electric insulator used to control electrolysis at points where dissimilar metals meet  | 20.             | Auxiliary<br>storage                   | <b>~</b> ' |
| -    | s.     | A solar system into which no air penetrates or from which no air can be expelled   | 21.             | Heat sink                              | •.         |
| •    | t.     | A solar system into which air can penetrate  | 22:             | Dielectric,                            | •          |
|      |        | or from which air can be expelled for drain-<br>down or to create a syphon effect  | <b>2</b> 3.     | Di <b>ss</b> imilar<br>met <b>a</b> ls |            |
|      | u.     | A symbol for the degree of acidity or alkalini-  |                 | 1                                      |            |
|      |        | ty of a solution; PH is measured on a scale of 0, indicating highest acidity, to 14, indicating highest alkalinity                           | -               | ••                                     | <u>.</u>   |
| -    | v.     | The tendency of certain insulating materials to release elements of their original composition, especially when exposed to high temperatures | يبو             |  | -          |
|      | w.     | A mechanical device, sometimes electronically activated, to stop or moderate flow within arsystem  | ,               | F X                                    | • .        |
| ⊾Con | nglete | the following list of statements concerning ch   | aracto          | ♥<br>eristics `of a                    | ء - thermo |
|      |        | HW system.   |                 |  |            |
| a)   | Mos    | t basic of heating   | g syst          | ems '                                  |            |
| b.   |        | ulation of water between tank and collector is maj<br>currents set up when water is heated   | in <b>ta</b> in | ed by natural                          | cońvec-    |
| C.   | Req    | uires no   |                 |  | • "        |
| d.   |        | n the water in the solar collector becomes hotter the it rises to the tank as the colder tank water drop                                     |                 |  |            |
| e.   | Whe    | n no water is being run at a tap; circulation wil  | ll con          | itin <b>ue</b> u <b>ntil t</b>         | ank and    |
| f.   | Rate   | e of flow be control   | olled           | ,                                      |            |
| g.   |        | icult to provide freeze protection, and system is t  | heref           | ore most app                           | ropriate   |

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- 3. Circle the words which best complete the following statements concerning characteristics of a pumped circulation domestic hot water system with heat exchanger.
  - a. (Domestic, Collector) water is pumped through a closed pipe loop incorporating a heat exchanger which is immersed in a storage tank
  - b. The closed collector pipe loop must have a/an (expansion, storage) tank and a separate pressure relief valve in addition to the valve on the tank
  - c. Because collected heat must be transferred through a heat exchanger, the collection fluid must be (hotter, cooler); this makes the system somewhat less efficient than one in which domestic water circulates directly through the collector
  - d. A (relief, check) valve in the collector return prevents migration of heat from tank to collector by thermo-syphon action on cold nights
  - e. Because collector water and domestic water do not intermingle, an antifreeze solution can be added to the (domestic, collector) water for low-temperature protection

| 7.              | hot wat                | er system with freeze control by placing an "X" in the appropriate blanks.   |
|-----------------|------------------------|--|
|                 | a.                     | System employs a heat exchanger but does not use a heat pump   |
| ,               | b                      | Collector circuit is not sealed off from stored water, and antifreeze cannot be used   |
|                 | c.                     | Freeze protection is provided by pumping water through the system with a rate of flow high enough to prevent freezing  |
|                 | d.                     | A two-way solenoid valve is the key control element in a pumped circulation system   |
|                 | e.                     | During normal operation, the solenoid valve allows water to circulate freely between tank and collector  |
|                 | f.                     | During normal operation, cold water is admitted to the system unless a hot water tap is opened in the building, in which case makeup water enters from the supply source   |
|                 | g.                     | In freezing temperatures, the solenoid valve automatically opens in the storage tank and diverts water from the collector into a dry well or sump, setting up a constant flow of water from the source through the collector circuit and into the sump |
| 5. <sup>^</sup> | Select tr<br>hot water | ue statements concerning characteristics of a pumped circulation domestic system with draindown by placing an "X" in the appropriate blanks.   |
|                 | a.                     | System incorporates a circulating pump for collector water, but does not employ a heat exchanger   |
|                 | <u>.</u> b.            | System employs a temperature sensor affixed to the bottom of the circulating pump  |
|                 |                        |  |

| e. Water then drains freely from the collector circuit and out of the system  f. Pressurized source water is prevented from flowing to the collector by means of a motorized valve in the supply line and a one-way check valve in the return line  g. When the absorber plate temperature rises to a preset difference abow storage, the motorized valve begins to open, the circulating pump restarts and the dump valve and inlet valve open  h. As the collector circuit refills, trapped air is relieved through the automatic vent and normal circulation of collector water is resumed  6. List two arrangements for domestic hot water storage tanks.  a.  b.  7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an  c. The  |    |      | c. When the sensor detects a drop to about 40°F, it initiates closing of the motorized valve in the collector supply  |
|---|----|------|---|
| f. Pressurized source water is prevented from flowing to the collector by means of a motorized valve in the supply line and a one-way check valve in the return line  g. When the absorber plate temperature rises to a preset difference abow storage, the motorized valve begins to open, the circulating pump restarts and the dump valve and inlet valve open  h. As the collector circuit refills, trapped air is relieved through the automatic vent and normal circulation of collector water is resumed  6. List two arrangements for domestic hot water storage tanks.  a.  b.  complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an  c. The  of the solar storage tank is connected to the conventional water heater with a fossil-fuel burner or an  c. The  connected to the cold or inlet line of the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the  water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank to trip and energize the conventional water heater burner or  g. This configuration allows only the relatively cold water to circulate through the |    |      | d. When the motorized valve reaches a fully closed position, it trips an end switch which in turn trips the solenoids of only the dump valve and not the air intake valve                     |
| means of a motorized valve in the supply line and a one-way check valve in the return line  g. When the absorber plate temperature rises to a preset difference abow storage, the motorized valve begins to open, the circulating pump restarts and the dump valve and inlet valve open  h. As the collector circuit refills, trapped air is relieved through the automatic vent and normal circulation of collector water is resumed  6. List two arrangements for domestic hot water storage tanks.  a.  b.  7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an  c. The  of the solar storage tank is connected to the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the  water is warm enough, it will move through the conventional tank and without requiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or  This configuration allows only the relatively cold water to circulate through the   |    |      | e. Water then drains freely from the collector circuit and out of the system  |
| storage, the motorized valve begins to open, the circulating pump restarts and the dump valve and inlet valve open  h. As the collector circuit refills, trapped air is relieved through the automatic vent and normal circulation of collector water is resumed  6. List two arrangements for domestic hot water storage tanks.  a.  b.  7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an  c. The   |    |      | f. Pressurized source water is prevented from flowing to the collector by means of a motorized valve in the supply line and a one-way check valve in the return line                          |
| 6. List two arrangements for domestic hot water storage tanks.  a.  b.  7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the b. In tandem with the larger tank is a conventional water heater with a fossil-fuel burner or an  c. The of the solar storage tank is connected to the cold or inlet line of the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without reguiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or   |    |      | g. When the absorber plate temperature rises to a preset difference above storage, the motorized valve begins to open, the circulating pump restarts, and the dump valve and inlet valve open |
| b. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an  b. In tandem with the larger tank is a conventional water heater with a fossil-fuel burner or an  c. The of the solar storage tank is connected to the cold or inlet line of the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or   |    |      | h. As the collector circuit refills, trapped air is relieved through the automatic vent and normal circulation of collector water is resumed  |
| 7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the b. In tandem with the larger tank is a conventional water heater with a fossil-fuel burner or an  c. The of the solar storage tank is connected to the cold or inlet line of the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or   | 6. | List | t two arrangements for domestic hot water storage tanks.  |
| 7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an  b. In tandem with the larger tank is a conventional water heater with a fossil-fuel burner or an  c. The of the solar storage tank is connected to the cold or inlet line of the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or   |    | a.   |   |
| 7. Complete the following list of statements concerning characteristics of dual domestic hot water tanks.  a. A larger tank is connected to the collector loop and stores hot water from the burner or an   |    | b.   |   |
| c. The of the solar storage tank is connected to the cold or inlet line of the conventional heater  d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or  |    |      | A larger tank is connected to the collector loop and stores hot water from the  |
| d. Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap  e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or  |    | b.   | In tandem with the larger tank is a conventional water heater with a fossil-fuel burner or an   |
| e. When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat  f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or   |    | C.   | The of the solar storage tank is connected to the cold or inlet line of the conventional heater   |
| f. Should the conventional tank water drop below a preset temperature, it will cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or   |    | d.   | Any demand for hot water causes the source water pressure to force water through the solar storage tank, through the conventional tank, and out to a hot water tap                            |
| cause the thermostat in the conventional tank to trip and energize the conventional water heater burner or  This configuration allows only the relatively cold water to circulate through the   |    | e.   | When the water is warm enough, it will move through the conventional tank without affecting the thermostat in the conventional tank and without requiring additional heat                     |
| g. This configuration allows only the relatively cold water to circulate through the collector, and this permits the collector to function at   |    | f. ` | cause the thermostat in the conventional tank to trip and energize the conven-  |
| ,   | ,  | g.   | This configuration allows only the relatively cold water to circulate through the collector, and this permits the collector to function at  |

| 8.           | Circle the words which best complete the following statements concerning characteristics of a single storage domestic hot water tank.  |
|--------------|--|
| . 3          | a. ☐Can⊱Cannot) provide both≅solar and auxiliary storage in the same tank  |
| `\ 3         | b. When this system is used, a (small, large) tank should be selected  |
| ,            | The thermostat of the auxiliary fuel input should be set to maintain a tank temperature of about (100-110°F, 110-120°F)  |
| •            | d. Because the lowest temperature of water that can be circulated back through the collector is 110°F, collector efficiency is (increased, lowered)  |
| <b>*9</b> .  | Select true statements concerning characteristics of a combined solar space and domestic hot water system by placing an "X" in the appropriate blanks.                                       |
|              | a. Water is heated and stored in a solar storage tank  |
|              | b. Makeup water for hot water supply passes through a heat exchanger in the solar storage tank   |
| ্<br>অ       | c. If the solar storage tank temperature is high enough, cold domestic makeup water passing through will pick up sufficient heat to avoid drawing energy from the domestic water heater      |
|              | d. When the temperature of the domestic water tank goes above the storage tank temperature, the domestic water is pumped through the heat exchanger, transferring whatever heat is available |
|              | e. An auxiliary heat supply cannot be programmed to supplement DHW requirements  |
| 1 <b>Ŏ</b> . | Complete the following list of statements concerning characteristics of a water collection, water storage, air distribution space heating system.  |
| •            | a. These systems have found wide acceptance because they are   |
|              | b. The circulating pump in the collector loop operates whenever collector temperature is than the temperature of the storage tank water by a preset amount                                   |
| - <b>એ</b>   | c. When the pump stops, water in the collectors and pipe lines drains into the   |
| ا ا          | d. To permit the automatic draining process, the return pipe must be coupled to the tank in such a fashion that the end of the pipe is kept  |
|              | of the stored water or the pipe must be vented by some   |
|              | e. When the building thermostat calls for heat, a pump circulates stored water through the heat exchanger coil in the return air duct upstream of the  |
| ٠,,          | ```  |

|      |               |                  | • •  |
|------|---------------|------------------|--|
|      | f.            | , ura            | water is being circulated through the heat exchanger, the furnace fan begins to wair through the heat exchanger coil and forces the warmed air into the lding  |
|      | g.            | iuii             | long as the coil continues to maintain supply air temperature high enough, the hace heating element remains off, but when s short of preset temperature settings, the furnace comes on to furnish sup- |
|      |               | pler             | mentary heat   |
| Ť1.  | tio           | ıı, wa           | sh between a series configuration and a parallel configuration in water collecter storage, water distribution space heating systems by placing an "X" next to iptions of a series configuration.       |
| -    | L             | a.               | Highly suited for fin tube and radiant panel installations   |
|      |               | b.               | One configuration for this system is that heat can be supplied by either the solar system or the auxiliary boiler  |
|      |               | c.               | Another configuration for this system is that heat can be supplied by both the solar system and the auxiliary boiler   |
|      | ,             | d.               | When the solar storage tank is hot enough to supply the heating load, water is pumped from the storage tank through the finned tubes and bypasses the boiler   |
|      | <br>ر         | e.               | If the storage tank is not hot enough to supply the heating load completely, water is pumped through the boiler and then into the finned tubes, bypassing the storage tank                             |
|      |               | f.               | If the heating requirement can be supplied by the water from the solar tank, the auxiliary boiler does not operate   |
|      |               | g.               | When more heat is required than the solar system can supply, alone, the boiler kicks in to supplement the solar heat   |
|      | <del></del> - | h.               | Permits lower temperature water in the solar system to be used to supply a portion of the heating load and actually contributes to higher collector efficiency and more usable solar energy            |
| 12., | Con<br>stor   | nplete<br>age, w | the following list of ways radiant panels are used in water collection, water vater distribution space heating systems.  |
| ,    | a.            | Radi<br>slabs    | ant panel heating systems employ copper tubes embedded in concrete floor and in wall and ceiling construction  |
| **•  | b             | with             | or more of concrete above the tubes and rest than an inch of concrete below the tubes  |
| •    | 'C. ,         | Ceilir           | ng and wall panels are usually embedded in   |
|      | d.            | Wall<br>heat     | panel installations require to reduce loss to the outside  |

97.



| 13  | storage, air distribution space heating system.   |
|-----|---|
| ,   | a. When heat is available for collection, but there is no heat demand in the house, the collector circulation fan begins to draw air down through the storage container                 |
|     | b. Motor operated damper number 3 is closed whenever the collector fan is operating and open at all other times   |
|     | c. The bottom portion of the storage container contents will heat first, and the heat will extend upward as more energy is collected  |
| ,   | d. When no heat is being collected, but is called for in the building, the centrif-<br>ugal fan in the auxiliary heating system begins operation and signals dampers<br>1 and 2 to open |
| •   | e. Return air is drawn upward through the storage, exits at maximum tempera-<br>ture, and is circulated through the building  |
|     | f. When the heating load cannot be supplied by the solar system, the auxiliary heating system comes on  |
|     | g. When there is a simultaneous collection of energy and demand for heat by a building, motor operated damper 4 is open   |
|     | h. Air is circulated directly from the collector to the building  |
| 14. | Complete the following list of characteristics of water collection, water storage, heat pump distribution space heating systems.  |
|     | a. The electrically driven heat pump enhances the flexibility and efficiency of   |
|     | b. A heat pump has the capability of extracting heat from a cooler source and increasing it to a higher temperature, thereby increasing the   |
|     | c. A heat pump can extract useful heat from the solar storage system even—when the temperature has room_temperature   |
| 15. | Distinguish between an air to-air heat pump and a water-to-air heat pump function in a solar space heating system by placing an "X" next to the function of an air-to-air heat pump.    |
|     | a. When heating is required, the heat pump extracts heat from the storage water, increases its temperature, and warms the room air  |
|     | b. When heating is required, the heat pump extracts heat from one air source (usually the outside air), increases its temperature, and warms the room air                               |
| 16. | Select true statements concerning steps in the operation of an air-to-air heat pump in a solar heating system by placing an "X" in the appropriate blanks.                              |
| 1   | a. All solar heating is done directly from storage without the aid of the heat pump, but the heat pump fan is used to circulate room air over the heat exchange coil                    |
|     |   |



|              | <u>·</u> b.              | If heat available from solar storage is insufficient, the heat pump begins to operate, supplying additional heat to the air  |
|--------------|--------------------------|--|
|              | c.                       | Although this does not permit stored solar energy to be used below the space temperature, it greatly reduces operational time of the heat pump and saves much electricity that would otherwise be used to operate the heat pump compressor |
| <b>-</b> 17. | Select tru<br>a solar he | ue statements concerning steps in the operation of a water-to-air heat pump in ating system by placing an "X" in the appropriate blanks.   |
| ,            | a.                       | When the solar storage tank temperature falls below a preset point (usually 90°F), storage is used directly for space heating with the heat pump fan circulating the room air over the solar water coil                                    |
|              | ,b.                      | When the storage tank temperature is over the temperature needed for heating, the control valve changes position and circulates the storage water into the heat pump   |
|              | c.                       | When the water flow to the heat pump has been proven by a flow switch, the heat pump compressor begins to operate, extracting heat from the water and increasing its temperature; it is then used for warming room air                     |
|              | d.                       | This procedure continues until the heating load has been satisfied or storage tank temperature drops to the lower operating limits of the heat pump (usually about 60°F)   |
| •            | e.                       | Sometimes, other water supplies of appropriate temperature can be used when usable water in the solar storage tank has been exhausted  |
|              | f.                       | An auxiliary heat supply is usually required with a water-to-air heat pump solar system  |
| 18.          |                          | e words which best complete the following statements concerning design ations for piping systems.  |
| <i>:</i>     |                          | rrosion, Freezing) is the biggest enemy of piping systems and other solar apponents  |
|              | lect<br>tanl             | s imperative, from a corrosion standpoint, that the fluid passages in the (color, absorber plate) be compatible with the materials used for piping, storage c, pump, and valve bodies  |
|              |                          | (pumps, piping) should be pitched from the high point of the system to the complete drainage when necessary  |
|              | at a                     | systems with drainage as freeze protection, the piping should be pitched minimum of (1/2, 1/8) inch per 1 foot of run to insure that fluid will drain apletely   |
|              | rem                      | t up of all liquid-carrying systems should include a flushing operation to ove (water and air, dirt and debris) accumulated during fabrication and allation  |



| 19.                    | Select<br>by p                               | et true statements concerning design considerations for corrosion protection lacing an "X" in the appropriate blanks.   |
|------------------------|--|---|
| -                      |  | a. Corrosion protection has three major concerns in metal collector systems:  |
|                        | •  | 1) Corrosion between dissimilar metals  |
|                        |  | 2) Use of corrosive liquids   |
|                        | \  | 3)^ Presence of air in the system   |
|                        | <del></del>                                  | b. When dissimilar metals are used in the presence of moisture, corrosion can occur; this is true even of copper when used with another metal   |
|                        |  | _c. In a solar system with a circulating fluid, it is sufficient simply to use dielectric fittings to separate dissimilar metals and control electrolysis   |
|                        |  | _d. Although it is difficult to exclude copper valves and pump impellers from collector systems, as a general rule, it is best to mix metals  |
| 20.                    | List   | four other considerations for corrosion protection.   |
| ,                      | а.   |   |
|                        |  | <u> </u>  |
|                        | b.   |   |
|                        |  |   |
|                        | c. , •                                       |   |
|                        | ,  | · · · · · · · · · · · · · · · · · · ·   |
|                        | d.   | · · · · · · · · · · · · · · · · · · ·   |
|                        | ,  |   |
| <b>21</b> <sub>.</sub> | glazır                                       | the following problem concerning design considerations for collector covering: Additional layers of cover glazing reduce heat loss in a collector; why not keep ig glazing to make the collector even more efficient? |
|                        | <u>.                                    </u> |   |
|                        |  |   |
| 22.                    | Comp<br>insula                               | plete the following list of statements concerning requirements for absorber plate ation.  |
|                        | 1  | Since absorber plates frequently reach temperatures of more than 200°F, they must be insulated to from the plate  |
|                        | b  | The back of the collector is typically insulated with athick fiberglass blanket   |



| ٠   | C.           | Most insulation currently available undergoes volumetric expansion at temperatures of 250°F and should be used with care, if at all   |
|-----|--------------|---|
|     | d.           | Other insulations have problems with the outgassing of volatile elements which can lead to corrosion and  |
|     | e.           | Insulation selected should be evaluated according to application needs .  |
| 23. | tior         | we the following problem concerning high temperature protection and its applicans: When cooler fluid is pumped into a collector in a condition of stagnation, what ally happens?  |
|     |              |   |
| 24. |              | nplete the following list of statements concerning rules of thumb for circulating aps and solar system controls.  |
|     | a.           | Pumps ordinarily selected for residential and small solar applications should be centrifugal types with mechanical shaft seals or   |
|     | b.           | Pumps may be close-coupled, in-line, or   |
|     | `. <b>c.</b> | Pump should have a proper combination of and lift characteristics for the application   |
|     | d. `         | In, pumps must have sufficient lifting capacity to raise water from the storage tank to the top of the collector  |
|     | e.           | In most small solar systems, the pumps will not exceed 1/4 to 1/3 horsepower and may be as small as 1/6 to 1/20 horsepower in   |
|     | f.           | When centrifugal pumps are used, it is essential that they operate with a net positive suction head   |
| ~   | , g.         | The in the collector loop is normally started or stopped by means of a differential temperature control which actuates the collector pump when the collector temperature is higher than the tank water temperature, and shuts the collector pump off when the collector water temperature approaches the tank temperature |
| 25. | Solv         | e problems concerning solar domestic water heating systems.   |
| 26. | Solv         | e problems concerning solar space heating systems.  |
| 27. | Dem          | constrate the ability to construct a working model solar water heater.  |
|     | (NO<br>instr | TE: If these activities have not been accomplished prior to the test, ask your uctor when they should be completed.)  |



## ACTIVE SOLAR HEATING SYSTEMS UNIT II

## **ANSWERS TO TEST**

- 16 17 m. 10 18 21 9 b. h. n. t. 13 2 23 3 15 0. u. C. 12 14 d. j. p. 19 8 11 k. 5 e. q. 20 22
- 2. a. Solar water
  - c. Heat exchanger
  - e. Equalized
  - f. Cannot
- 3. a. Collector
  - b. Expansion
  - c. Hotter d. Check
  - d. Check e. Collector
- 4. b, c, e
- 5. a, c, e, f, h
- 6. Any two of the following:
  - a. Dual solar and conventional tanks
  - b. Single storage tanks
  - c. Combined solar space and DHW heating systems
- 7. a. Collector e. Solar-heated b. Electric heating element f. Electrode c. Outlet pipe g. A higher efficiency
- 8. a. Can
  - b. Large
  - c. 110-120°F
  - d. Lowered
- 9. a, b, c
- 10. a. Simple to operate and control
  b. Higher
  c. Storage tank
  d. Above the level
  e. Furnace
  g. Solar supplied heat
- 11. a, b, d, e
- 12. b. One inch
  - c. Plaster
  - d. Heavy insulation
- 13. a, d, e, f, h

- 14. a. 'Solar systems'
  - b. Thermal gradient
  - c. Fallen below
- 15. b
- 16. a, b, c
- 17. c, d, f
- 18. a. Corrosion
  - b. Absorber plate
  - c. Piping
  - d. 1/8
  - e. Dirt and debris
- 19. a, b
- 20. Any four of the following:
  - a. Check the local water supply for PH level
  - b. A trouble free history of copper plumbing in the locality can usually be taken as evidence that the water is not aggressive to copper, but it may be aggressive to other metals
  - c. When there is a question concerning the presence of aggressive water, the water should be chemically analyzed, and a treatment engineer should be consulted to prescribe ways to make and keep the water nonaggressive
  - d. When antifreeze or special heat transfer fluids are added to the water, it increases the potential for corrosion
  - e. Anti-freezes which are propylene glycol (nontoxic) or ethylene glycol (toxic) based are the two major types of anti-freeze used with water in solar collectors
  - f. Propylene glycol is claimed to be nontoxic and should be used in DHW systems unless a double walled heat exchanger is employed
  - g. Anti-freeze solutions usually require the addition of corrosion inhibitors and buffers for PH, and all anti-freeze solutions should be monitored and replenished as required
- 21. There is a point where additional glazing actually diminishes collector efficiency
- 22. a. Maximize energy collection
  - b. 3 to 4-inch
  - c. Foamed urethane
  - d. Other collectable problems
- 23. This usually results in thermal shock which can cause the collector to buckle and the glazing to break
- 24. a. Totally sealed units

d. Open systems

b. Base-mounted

e. Closed systems

Circulating pump

- c. Flow rate
- 25. Evaluated to the satisfaction of the instructor
- 26. Evaluated to the satisfaction of the instructor
- 27. Performance skills evaluated to the satisfaction of the instructor

## LOAD CALCULATIONS AND SOLAR COOLING UNIT III

## **UNIT OBJECTIVE**

After completion of this unit, the student should be able to solve a problem concerning considerations for establishing heat requirements for solar water heating, discuss the concept of degree days, list the procedure for sizing a solar collector, and discuss basic concepts of solar cooling with absorption systems. The student should also be able to complete a sunchart worksheet for a specific solar application and size a solar collector. This knowledge will be evidenced by correctly performing the procedures outlined in the assignment sheets and by scoring 85 percent on the unit test.

## SPECIFIC OBJECTIVES

After completion of this unit, the student should be able to:

- 1. Match terms related to load calculations and solar cooling with their correct definitions.
- 2. Solve a problem concerning considerations for establishing heat requirements for solar water heating.
- 3. Solve a problem concerning the concept of degree days and its formula.
- 4. Solve a problem concerning the concept of the degree day adjustment factor and its applications.
- 5. Solve a problem concerning the sun chart worksheet and its applications.
- 6. Complete a list of statements concerning the procedure for collector sizing.
- 7. Select true statements concerning rules of thumb for solar refrigeration systems.
- 8. Complete a list of statements concerning basic concepts of solar cooling with absorption systems.
- 9. Match types of lithium-bromide-water units with their characteristics.
- 10. Select true statements concerning operating principles of an absorption air conditioner.
- 11. Select true statements concerning system flow in a water chiller application.
- 12. Solve a problem concerning evaporative cooling with rock-bed storage.
- 13. Complete a sun-chart worksheet for a specific solar application.
- 14. Size a solar collector for a combination DHW and space heating solar system.



# LOAD CALCULATIONS AND SOLAR COOLING UNIT III

## SUGGESTED ACTIVITIES

- I. Provide student with objective sheet.
- II. Provide student with information and assignment sheets.
- III. Make transparencies.
- IV. Discuss unit and specific objectives.
- V. Discuss information and assignment sheets.
- VI. Review basic elements of heating and cooling load calculations.

(NOTE: This information is available in Manual J, Load Calculation for Residential Winter and Summer Air Conditioning; check with a local air conditioning contractor to obtain a copy, or it may be ordered from The Air-Conditioning Contractors of America, 1228 17th St. N. W., Washington, D.C. 20036; the ASHRAE Handbook of Fundamentals is another source for information on load calculations, or the materials in Unit VI, "Residential Heat Loss and Heat Gain," Air Conditioning and Refrigeration, Book III, as published by the Mid-America Vocational Curriculum Consortium, will serve the purpose well.)

- VII. Invite a representative from a local gas or electric utility to talk to the class concerning calculations for heating and cooling loads; most utilities use computerized load calculations, and it would be especially effective if the utility representative could present a computerized load calculation that would provide the students with additional information and assistance with the assignment sheets in this unit.
- VIII. Read the assignment sheets carefully, and select a model home that students can use to adequately calculate heating loads for a typical solar application in your specific locale.
  - IX. Prepare a chart of solar information pertinent to your area; it should include latitude, degree day information, design temperature for both heating and cooling, a solar insolation chart, and prevailing winter and summer winds.
  - Locate a business or residence in your area that is using a solar cooling system, and invite the person most familiar with the system to talk to the class about its design, performance, and maintenance.
- XI. Give test.



## INSTRUCTIONAL MATERIALS

- I. Included in this unit:
  - A. Objective sheet
  - B. Information sheet
  - C. Transparency masters
    - 1. TM 1-Absorption Air Conditioner
    - 2. TM 2-Flow Schematic of a Water Chiller Operation
    - 3. TM 3--Evaporative Cooling with Rock-Bed Storage
  - D. Assignment sheets
    - 1. Assignment Sheet #1--Complete a Sun-Chart Worksheet for a Specific Solar Application
    - 2. Assignment Sheet #2--Size a Solar Collector for a Combination DHW and Space Heating Solar System
  - E. Test /
  - F. Answers to test
- II. References:
  - A. Solar Energy Systems. New York, NY 10174: Copper Development Association, Inc., 1979.
  - B. Solar Energy Applications Laboratory, Colorado State University. Solar Heating and Cooling of Residential Buildings, Sizing, Installation and Operation of Systems. Washington, D.C. 20402: U.S. Department of Commerce, 1977.
  - C. Solar Energy Project, Text. Washington, D.C. 20545: U.S. Department of Energy, 1979.
  - D. Solar Energy Project, Reader. Washington, D.C. 20545: U.S. Department of Energy, 1979.

## LOAD CALCULATIONS AND SOLAR COOLING UNIT III

## INFORMATION SHEET

## I. Terms and definitions

- A. Btu-British thermal unit; the amount of heat required to raise the temperature of one pound of water one degree Fahrenheit
- B. Btuh-British thermal units per hour; unit used to express hourly heat flow
- C. Dry-bulb temperature-: The air temperature as measured by an ordinary thermometer
- D. Wet-bulb temperature. The air temperature as measured by a thermometer whose bulb is covered with a wet cloth or wet wick and moved in air that has a velocity of one thousand feet per minute
- E. Heat loss-The amount of heat lost through all building surfaces, walls, floors, doors, and windows exposed to outdoors or to adjoining spaces with different temperatures
- F. Heat gain-The amount of heat gained through all building surfaces, walls, floors, doors, and windows exposed to outdoors or from adjoining spaces with different temperatures
- G. Load-The total heat loss and heat gain of a structure expressed in Btuh; this calculation is used to size heating and cooling equipment
- H. Ventilation--Controlled air brought into a structure
- I. Infiltration-Uncontrolled air that leaks into a structure
- J. Humidity-The amount of water vapor or moisture that is present in the atmosphere or any material
- K. Relative humidity. The percentage of moisture in the air compared to the total amount of moisture the air could hold at the same temperature and barometric pressure
- L. Psychometrics-The science of measuring and changing the properties of air
- M. Hydronics-The science of heating and cooling with liquids
- N. Nomogram--A chart which can be used with a straightedge to determine the square footage requirements of a collector
- O. Refrigerant-A substance used in refrigerating mechanisms to absorb heat in the evaporator
- P. Absorbent-A liquid which combines chemically with a refrigerant and causes heat to be released in the process of combination



- Q. R-value-The rating given to a material's ability to resist heat transfer
- R. Cfm--Cubic feet per minute
- S. Ton of refrigeration-A refrigerating effect equal to 12,000 Btuh
- T. Chiller-The component in an absorption cooling unit which absorbs heat from the circulating water supply
- II. Considerations for establishing heat requirements for solar water heating
  - A. Hot water consumption is the major factor influencing annual heat requirements
  - B. The amount of heat required to produce hot water depends on
    - 1. Number of gallons of hot water consumed daily
    - 2. Inlet temperature of the cold water supply
    - 3. Desired discharge temperature at the fixtures
  - C. Deep wells produce water at a relatively constant temperature, but water from shallow wells, lakes, rivers, and reservoirs, varies with changing air temperature throughout the year (Figure 1)

## FIGURE 1

|             |          | 1   | F  | M  | A  | M  | J   | J  | A    | S  | 0  | N  | <u>D</u> |
|-------------|----------|-----|----|----|----|----|-----|----|------|----|----|----|----------|
| Albuquerque | w        | 62  | 62 | 62 | 62 | 62 | 62  | 62 | 62   | 62 | 62 | 62 | 62       |
| Boston      | Re       | 32  | 36 | 39 | 52 | 58 | 71  | 74 | 67 ° | 60 | 58 | 48 | 45       |
| Chicago     | L        | ,32 | 32 | 34 | 42 | 51 | 57  | 65 | 67   | 62 | 57 | 45 | 35       |
| Denver      | Ri       | 39  | 40 | 43 | 49 | 55 | 60  | 63 | 64   | 63 | 56 | 45 | 37       |
| Fort Worth  | L        | 46  | 49 | 57 | 70 | 75 | 81  | 79 | 83   | 81 | 72 | 56 | 46       |
| Los Angeles | Rı       | 50  | 50 | 54 | 55 | 63 | 70  | 73 | 73   | 72 | 68 | 57 | 52       |
| Las Vegas   | L.W      | 57  | 64 | 68 | 71 | 77 | 85  | 87 | 86   | 78 | 70 | 65 | 57       |
| Miami       | W        | 70  | 70 | 70 | 70 | 70 | 70  | 70 | 70   | 70 | 70 | 70 | 70       |
| Nashville   | Ri       | 48  | 46 | 53 | 63 | 66 | 69  | 71 | 75   | 75 | 71 | 58 | 53       |
| New York    | Re       | 36  | 35 | 36 | 39 | 47 | 54  | 58 | 60   | 61 | 57 | 46 | 45       |
| Phoênix *   | Ri, Re.W | 48  | 48 | 50 | 52 | 57 | 59  | 63 | 75   | 79 | 69 | 59 | 54       |
| Saft Lake C | W,C      | 35  | 37 | 38 | 41 | 43 | 47  | 53 | 52   | 46 | 43 | 38 | 37       |
| Séattle     | Ri :     | 43  | 42 | 46 | 51 | 56 | 61  | 65 | 66   | 65 | 58 | 52 | 44       |
| Washington  | , PN     | 42  | 42 | 52 | 56 | 63 | 67, | 67 | 78   | 79 | 68 | 55 | 46       |

Source Data From Handbook of Air Conditioning System Design p 5-41 through 5-46 McGraw Hill Book Company New York (1965) Abbreviations C—Creek L—Lake Re-Reservoir Ri-River W—Well

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D. The formula for determining Btu requirements for hot water is: Desired discharge temperature minus inlet temperature of cold water supply times 8.33 (it takes 8.33 Btu to raise one gallon of water 1°F) times the number of gallons of hot water consumed

(NOTE: The chart in Figure 2 shows how the above formula would work in determining hot water requirements for a family of four in Nashville, Tennessee; the desired discharge temperature is 135°F and the water consumption is estimated to be 91 gallons per day.)

## FIGURE 2

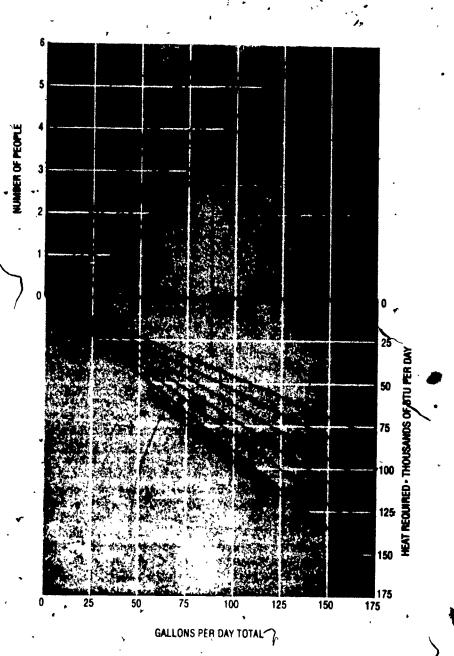
Example: family of Four-Nectivitie, Terraseese High-Consumption— 91 Gallons/Day

| MONTH      | COLD<br>WATER<br>TEMP. | MEAT MEQUIPMENTS (ATUANY) |
|------------|------------------------|---------------------------|
| January    | 46                     | 67,500                    |
| February   | 46                     | 67,500                    |
| March -    | 53                     | 62,200                    |
| April      | 63                     | 54,600                    |
| May        | 66                     | 52,300                    |
| June       | 69                     | 50,000                    |
| July       | 71 .                   | 48,500                    |
| August     | 75                     | 45,500                    |
| September  | 75 •                   | 45,500                    |
| October    | 71                     | 48,500                    |
| November - | 58 ~                   | 58,400                    |
| December . | <b>53</b> ,            | , <b>62,200</b> .         |
|            |                        |                           |

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E. Typically, a family of four consumes between 60 to 90 gallons of hot water daily, but the hot water consumption requirements can be arrived at for any latitude by interpolating between the cold water supply temperatures shown in Figure 1, the formula for arriving at Btu.requirements given in item D, and by using the chart in Figure 3 to achieve a number of persons/gallons requirements figure

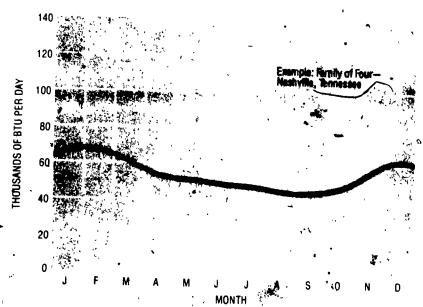
FIGURE 3



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F. Calculations obtained by using the chart in Figure 3 can be checked by plotting a graph of the information; the graph should curve smoothly, and any sharp deviation in any month is a clue that an error exists (Figure 4)

(NOTE: The following graph reflects information previously noted for a family of four in Nashville, Tennessee.) • FIGURE 4



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III. The concept of degree days and its formula

- A. Instead of using peak heating demands to determine heating requirements, the concept of degree days is used to determine average requirements.
- B. A degree day is a standard used to measure the heating season's mean temperature
- C. The number of degree days in a calendar day is determined by the following formula: Subtract the day's mean temperature from 65°F

Example: If the mean temperature on a given day is 50°F, subtract 50°F from 65°F, and this yields 15 degree days for that specific calendar day

D. By adding the number of degree days for each day of the month, the average monthly conditions can be identified, and the average yearly conditions can be identified

(NOTE: Degree days charts for many locations in America and Canada are available from many sources; examples will be given later in this unit.)

E. In general, a solar system should be considered for a residence only when the space heating demand has been limited to approximately 8 Btu per square foot per degree day or less

Example: Consider a home in Nashville, Tennessee, which loses 30,000 Btu per hour, while the outdoor temperature is 17°F; if this temperature exists for a 24-hour period, the building demand is 30,000 x 24 which is 720,000 Btu; since the design point temperature is 17°F (48 degree days per day), the house requires a net heat input of 15,000 Btu per degree day as shown below:

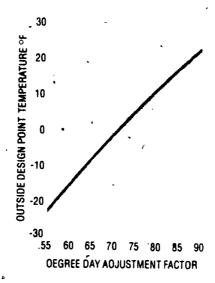
30,000 Btu/hr x 24 hrs (65°F degree day base - Btu/DD 17°F design point temp)

Assuming that the home's floor area is 2,000 square feet, the required heat input is 7.5 Btu per square foot per degree day; since this is less than the requirements of 8 Btu per square foot per degree day, this house is a good candidate for solar heating

- F. Homes that exceed the minimum 8 Btu per square foot per degree day are not well suited for solar applications and the money would be better spent on insulation to reduce energy demands
- IV. The concept of the the degree day adjustment factor and its applications
  - A. Because structures absorb radiant heat through windows and other components, this actually lowers the building's heating requirements, but are not included in peak load calculations

B. This adjustment is made by using a degree day adjustment factor as presented in the following chart (Figure 5)

## FIGURE 5



The outside design point temperature is based on hourly average temperatures for each hour of a total year. The average hourly temperatures will be above the design point temperature 97½ percent of the year.

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C. Using the degree day adjustment factor is as simple as finding the outside design point temperature and tracing a line across the chart until it intersects the proper adjustment factor, which will always be less than 1.0; then, the average heat requirement calculated by standard measurement is multiplied by the degree day adjustment factor.

D. The heat load calculations for each month should be completed to include the degree day adjustment factor and prepared in a chart such as the one shown in Figure 6

| F | ısı | IRF | G |
|---|-----|-----|---|

| Example: Nashville, Tenness |           |  |  |  |  |
|-----------------------------|-----------|--|--|--|--|
| Month                       | (BTU/Day) |  |  |  |  |
| Jacuary                     | 322,500   |  |  |  |  |
| February                    | 296,700   |  |  |  |  |
| March                       | 213,000   |  |  |  |  |
| April                       | 81,270    |  |  |  |  |
| May                         | ₹16,650   |  |  |  |  |
| June *                      | 0         |  |  |  |  |
| July                        | 0         |  |  |  |  |
| August                      | 0         |  |  |  |  |
| September                   | 12,900    |  |  |  |  |
| October                     | 65.750    |  |  |  |  |
| November                    | 212,850   |  |  |  |  |
| December                    | 304.600   |  |  |  |  |



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E. Add all the heating load requirements to the hot water load requirements to obtain the total heating requirements for the home

### V. The sun-chart worksheet and its applications

A. The sun-chart worksheet is a simplified approach that permits rapid evaluation of heat loads and collector areas

(NOTE: The sun-chart worksheet was developed by the Copper 'Develop-' ment Association, Inc., and when properly used, generates results 'equal to or slightly more conservative than results achieved by computer analysis; obviously, calculations cannot be guaranteed by the CDA, but when used properly, the sun-chart worksheet can be an effective planning tool.)

- B. The simplification of calculations is accomplished by making the following assumptions about solar system characteristics:
  - 1. The collector orientation is within 15 degrees of due south; applications that vary significantly from this should be calculated after adjustment factors from an orientation chart
  - 2. Collectors with circulating liquids are used to carry collected energy to storage or load
  - 3. Water storage capacity ranges from 1 1/2 to 2 gallons per square foot of collector array
- C... The designer begins by entering the first five column's (A through E) available data concerning the application (Figure 7)



- D. The designer then performs six mathematical operations using these basic data and enters the results in columns F through L (Figure 7)
- E. A final multiplication yields data for the "Result" column on the far right; the average daily heat produced during each of the 12 months by one square foot of collector at a given tilt angle, operating at a specific temperature, and installed in a particular locality (Figure 7)

## FIGURE 7

| JOB<br>LUCATION<br>LATITUDE | LOLLECTOR TYPE<br>COLLECTOR THT<br>APPLICATION    |   |   |   |  |                    |  |         |  |          |  |                          |  |
|-----------------------------|---|---|---|---|--|--------------------|--|---------|--|----------|--|--------------------------|--|
|                             |   | •   |   |   | ,  |                    |  | , ,     | <u> </u>   |          |  | н, 1                     |  |
| •                           | HEAT JAIN<br>FAIT R<br>FAIT R<br>HABLE d<br>RIME, | OLLECTUR<br>HEAT SS<br>FALTUR<br>ABIT B<br>URMELS | AVEHAUE<br>DAYTIME<br>A.M.<br>TEMPERA<br>T. RE. I | HUR ZONTA:<br>S) AR<br>ENERGY<br>FROM<br>TABLES<br>APPENDIX B | I OCCEUTOR<br>T. FACTUR<br>FREWTARCE<br>APPEND T | INCIDENT<br>ENERGY | ABLE A<br>ME<br>EMPERA<br>ALE<br>LOI ELLUH | CO. MA. | F7-  |          | FLE<br>ESCHET<br>EN MUSEUM                       | FOTAL<br>FRERILE<br>EL E |  |
| JANUARY                     |   |   |   |   |  |                    |  |         |  |          | <del>                                     </del> |                          |  |
| FEBRUARY                    |   |   |   |   |  |                    |  |         | <del>                                     </del> | <u> </u> | 1  |                          |  |
| MARCH                       |   |   |   |   |  |                    |  |         |  |          | <del>                                     </del> | -                        |  |
| APRIL -                     |   |   |   |   | 7/   | •                  |  |         |  |          |  |                          |  |
| MAY                         |   |   |   |   |  |                    |  |         |  |          | <del>                                     </del> |                          |  |
| JUNE                        |   |   | -   |   |  |                    |  | _       |  |          |  |                          |  |
| JULY                        |   |   |   |   |  |                    |  |         |  |          | +  |                          |  |
| AUGUST                      |   |   |   |   |  |                    |  |         |  |          |  |                          |  |
| SEPTEMBER                   | $\neg \neg$                                       |   |   | $\neg \uparrow$   |  | <del>- ,  </del>   |  |         | ,  |          | <del>                                     </del> | •                        |  |
| OCTOBER                     |   |   |   |   |  |                    |  |         |  |          | <del>│                                    </del> |                          |  |
| NOVEMBER                    | •   |   |   | 1   |  |                    |  |         |  |          | <del>                                     </del> |                          |  |
| DECEMBER                    |   |   | $\neg \neg$                                       |   |  | -+                 |  |         |  |          | -  |                          |  |

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F. Information from the worksheet is then used to properly size the solar collector

(NOTE: Step by step use of the CDA sun-chart worksheet is presented in Assignment Sheet #1.)

- VI. Procedure for collector sizing -
  - A. Once the rate of energy output from the collector has been established, the designer can proceed to find the collector area needed for a specific application
  - B. It is normally not economically practicable to size solar systems to handle 100 percent of the heating requirements
  - C. Gollectors for DHW systems are usually sized to handle 70 to 80 percent of annual heating requirements
  - D. Collectors for combination DHW and space heating systems are usually sized to handle 60 to 70 percent of annual heating requirements





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- E. As a rule of thumb, the correct percentages for sizing a collector can be established by:
  - 1. Sizing a collector for a DHW system so that it supplies 100% of the heat requirement for the month of May
  - 2. Sizing a collector for a combination system so that it supplies 100% of the heat requirement for the month of March

(NOTE: The procedure for collector sizing is covered step by step in Assignment Sheet #2.)

- VII. Rules of thumb for solar refrigeration systems
  - A. Since refrigeration systems affect cooling by removing heat from the air as it comes in contact with a cold, refrigerated surface, conventional vapor-compressor cooling systems using electric motors are adaptable to systems using solar energy
  - B. Absorption systems are not adaptable to systems using solar energy
  - C. For economic reasons, the absorption systems appear to be the most useable in solar systems
  - D. Absorption systems currently available include:
    - 1. Lithium-bromide-water units
    - 2. Water-ammonia absorption units
  - E. Lithium-bromide-water units are more commercially available than other types of units
- VIII. Basic concepts of solar cooling with absorption systems
  - A. Absorption systems are similar in principle to an ordinary, electrically operated vapor-compression air conditioner
  - B. Instead of a refrigerant like Freon in a conventional air conditioner, inorganic refrigerants, such as water and ammonia, are used in an absorption machine together with an absorbent
  - C. An absorbent is a liquid which combines chemically with the refrigerant and releases heat from the fluid mixture in the combination process
  - D. In a lithium-bromide-water unit, water is the refrigerant and the lithium-bromide is the absorbent
  - E. In an ammonia-water unit, ammonia is the refrigerant and water is the absorbent

(NOTE: These units are normally used only for commercial applications.)



- IX. Types of lithium-bromide-water units and their characteristics
  - A. Air chiller-Cools air which contacts the cooling coils
  - B. Water chiller-Cools water which contacts the cooling coils
- X. Operating principles of an absorption air conditioner (Transparency 1)
  - A. The cycle begins when water in the liquid mixture in the generator is boiled off and superheated with solar energy at a temperature between 170 and 210°F
  - B. The superheated water vapor passes from the generator to the condenser where it is cooled to about 100°F by the cooling water from an outdoor cooling tower
  - C. The vapor condenses to a liquid and is then revaporized through an expánsion valve which cools the vapor-liquid mixture to a temperature of 40°F in the evaporator, coils
  - D. The heat in the room air or water which is brought in contact with the evaporator is removed by the cooled refrigerant in the evaporator
  - E. The refrigerant then passes to the absorber where it recombines with the concentrated lithium-bromide solution from the generator at a temperature of about 100°F
  - F. In this recombination process, heat is released, and the heat is removed by the cooling water from the cooling tower
  - G. The dilute solution of lithium-bromide and water in the absorber flows by gravity, or is pumped back to the generator, and the cycle is repeated
  - H. Some lithium-bromide water systems use a recouperator as a heat exchanger to make the system thermodynamically more efficient
- XI. System flow in a water chiller application (Transparency 2)
  - A. The absorption chiller should be situated close to the hot water storage tank to minimize heat loss from the pipelines connected to the tank
  - B. Hot water from the top of the storage tank is pumped through the generator by pump (P-2) and returned to the bottom of the tank; note that the piping connection goes through the auxiliary boiler
  - C. When the temperature in the storage tank is insufficient to operate the absorption chiller, the auxiliary boiler is used to provide heat to the generator
  - D. When the auxiliary boiler is used, the three-way valve at the bottom of the auxiliary boiler circulates the return water only through the auxiliary boiler so that auxiliary energy is not used to heat the solar storage tank

- E. Pump size and head depend on the flow rate and pressure loss through the system and also the size and length of piping
- F. A wet cooling tower is needed with the absorption chiller to discharge the heat from the condenser and the absorber to the atmosphere

(NOTE: Some smaller systems employ air to discharge heat from the condenser.)

- G. The size of the cooling tower depends on the size of the absorption machine and the wet-bulb temperature of the ambient air
- H. A pump (P-3) is needed to circulate the cooling water from the tower through the absorber and condenser of the absorption machine
- I. Chilled water from the evaporator is circulated to the fan-coil unit to cool the air in the rooms

(NOTE: Operation of water ammonia absorption units are similar to the lithium-bromide-water units except that operating temperatures are higher and a separator is inserted between the generator and condenser, but water-ammonia units are not readily available and are not treated in this unit.)

XII. Evaporative cooling with rock-bed storage (Transparency 3)

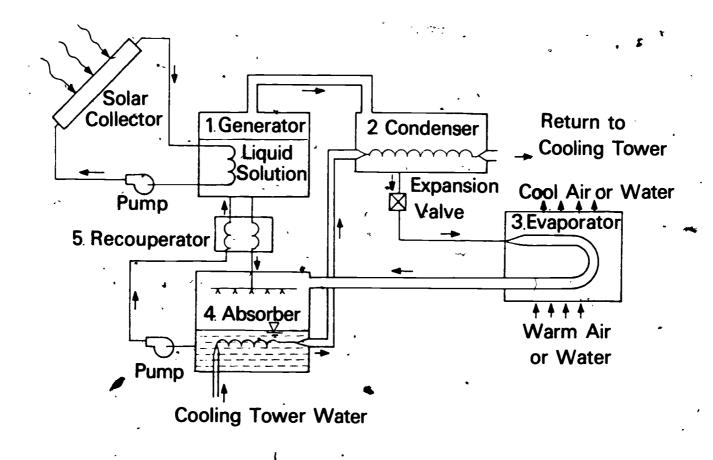
(NOTE: Strictly speaking, evaporative cooling is not a solar system, but rock-bed storage of an air-heating solar system for storing cool air in the summer can be accomplished with the following procedure)

- A. Night air is evaporatively cooled and circulated through the rock-bed to cool down the pebbles in the storage unit
- B. During the day, warm air from the building can be cooled by passing the air through the cool peoble bed
- C. When a solar heating system with rock bed storage is considered for cooling, it is advantageous to install the maximum storage volume consistent with heating system design
- D. Evaporative cooling with rock-bed storage is best restricted to arid and semi-arid regions with cool nights and low wet-bulb temperatures

(NOTE: In marginal conditions, evaporative cooling through rock-bed storage might function, but it would produce an extremely uncomfortable humidity of more than 70 percent.)



# **Absorption Air Conditioner**

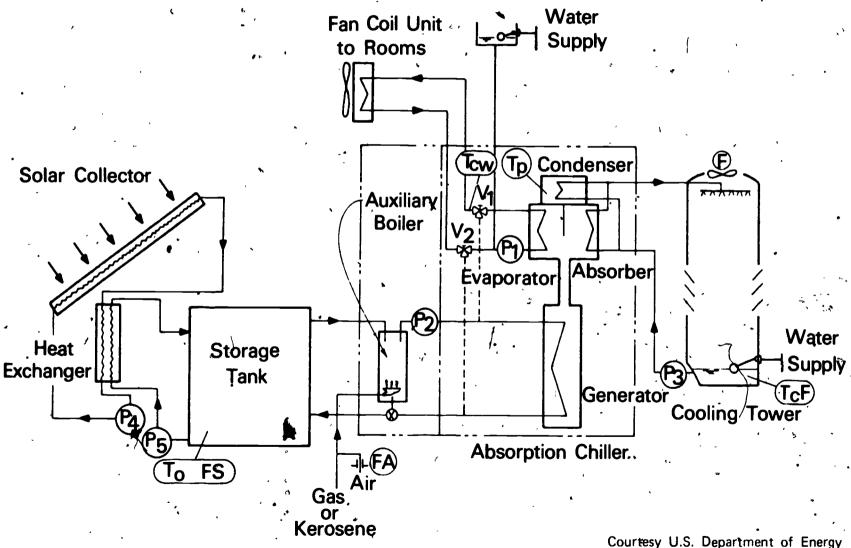


(NOTE: This type of unit is designed for commercial use only.)

Courtesy U.S. Department of Energy

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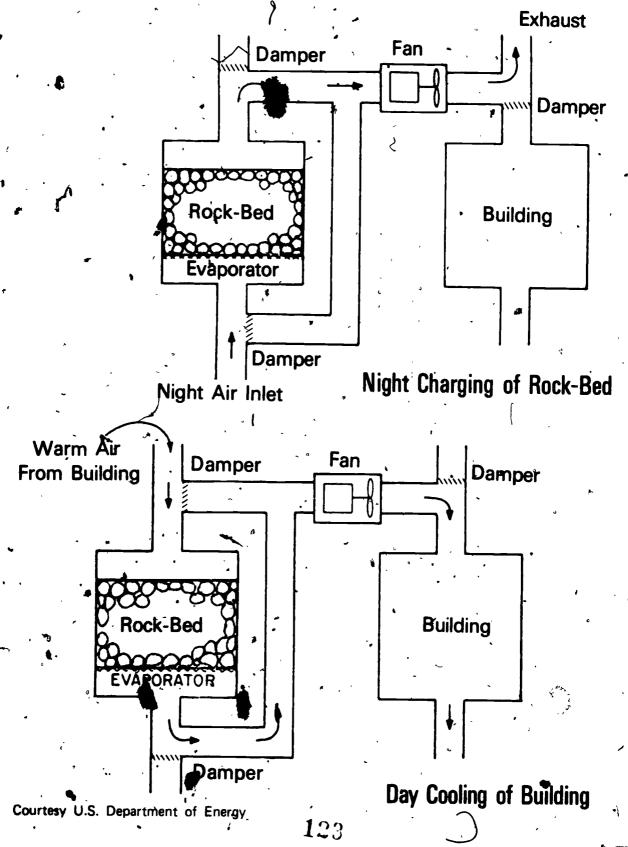
# Flow Schematic of a Water Chiller Operation



Courtesy U.S. Departmen

(NOTE: This operation is for commercial use only.)

# **Evaporative Cooling with Rock-Bed Storage**



ERIC

## LOAD CALCULATIONS AND SOLAR COOLING

# ASSIGNMENT SHEET #1-COMPLETE A SUN-CHART WORKSHEET FOR A SPECIFIC SOLAR APPLICATION.

Directions: Proceed carefully through the following example of how the CDA sun-chart worksheet should be filled out column by column; these examples are from a CDA sunchart worksheet prepared for a setar application in Nashville, Tennessee, but all materials presented can be adapted to fit latitude, type of collector, and other pertinent factors necessary to produce an accurate "Results" column. Refer to the completed CDA sunchart worksheet as you move through the example. The reference will assist you in understanding each step and its particular significance in the process.

## DATA INPUT (Columns A through E)

Column A:

Enter the collector heat gain factor from the chart in Figure 1; this chart is a general guideline, but heat gain factors are supplied by manufacturers of collectors; note that in the completed worksheet, the collector has 2 plates and a copper absorber with selective surface

FIGURE 1

| COLLECTOR<br>DESCRIPTION                                     | Heat Gala<br>Pactor | Heat Loos<br>Factor |   |
|--|---------------------|---------------------|---|
| 1 Cover Plate<br>Copper Abserber<br>with Flat Black Surface  | .78                 | 1.35                |   |
| 2 Cover Plates<br>Copper Absorber<br>with Flat Black Surface | .72                 | 90                  |   |
| 1 Cover Plate Copper Absorber Selective Surface              | 76                  | . 85                | 1 |
| 2 Cover Plates<br>Copper Absorber                            |                     |                     |   |
| Selective Surface  | ر 70.               | <del>65 -</del>     |   |

Courtesy Copper Development Association Inc.

Column B:

Enter the collector heat loss factor from the chart in Figure 1; note what is entered on the completed worksheet and remember this information for collectors not listed on the chart in Figure 1 is available from the collector manufacturer

Column C:

Enter the daytime average air temperature for the locale; this may be obtained from available charts or from a local or regional weather station; in the case of the completed worksheet, the daytime average temperature for Nashville. Tennessee during the month of January is 46°F and for the month of July is 87°F

Column D: Enter the amount of horizontal solar energy received by a horigontal surface on an average day in each month; this information is available in insolation tables which are included as examples in this activity; enter the number preceding the slash in the insolation chart; note that in the completed worksheet, the January figure is 601 and the July figure is 2033; the entry after the slash is a diffuse percent used interpolating information needed in

Enter the collector tilt factor; from the completed worksheet, you can see the entry of 1.44 is the January tilt factor for the Nashville latitude of 36°. This requires interpolation, but here's how it works: In January, Nashville has a % diffuse factor of 65%. If a collector tilt of 51° (latitude plus 15°) is desired, we must interpolate between both the positions of latitude and the tables for % diffuse. First, interpolate for latitude on each of the two applicable % diffuse charts (60% and 80%). On the 60% chart, we interpolate between the January factor for a collector tilt of latitude +15°, for 32° latitude (1.37) and for 40° latitude (1.60). Since the latitude of the site (36°) is halfway between them, the result is 1.485, or call it 1.49. Similarly, for the 80% chart, the result is 1.28. Since the % diffuse for Nashville in January is 65%, an interpolation between 1.49 and 1.28 yields a tilt factor of 1.4375, call it 1.44, and that is the tilt factor that should be entered across from January in column E

### COMPUTATION SECTION (Columns Athrough L)

Column E 🕟

Column F: This entry is obtained by multiplying the quantities from columns D and E; on the completed worksheet, the January figure would be 865.44, call it 865

Column G:

Enter here the assumed collector input temperature as obtained from the following chart in Figure 2; for Nashville for an application that combines space heating and DHW, that figure is 100°; be careful with this part of the procedure because this chart was prepared specifically for Nashville; other locales will probably have different collector input temperatures from month to month

|   |                                       |                  | ۰   |
|---|---------------------------------------|------------------|---|
| + | Comb<br>Space H<br>and Dor<br>Water H | eating<br>nestic | Domestic Water<br>Heating Only (Add to<br>Cold Water Supply<br>Temperature) |
|   | January                               | 100°             | CWS + 20°   |
|   | February                              | 115°             | CWS + 35°   |
| ì | March                                 | 140°             | CWS + 60°   |
|   | April                                 | . 155°           | <b>GMS</b> + 75°  |
|   | May                                   | 165°             | CWS + 85°   |
|   | June                                  | 175*             | CWS + 95°   |
|   | July                                  | /180             | CWS +100°   |
|   | August                                | \$ 180°          | CWS-+100*   |
|   | September 1                           | 175*             | CWS + 95°   |
|   | October                               | 150°             | CWS + 70°   |
| ~ | November                              | 130°             | CWS + 50° .   |
|   | December                              | 105*             | CWS + 30°   |
|   | _                                     | _                |   |

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Column H:

FIGURE 2

Enter here the temperature difference between the collector inlet and the daytime average air temperature; in other words, subtract Column C from

Column G; in the case of the completed worksheet, the figure is 54

Column J:

This entry is obtained by dividing Column B by column A and multiplying the result by 2 times the quantity from column H; in the completed worksheet, the figure is 100

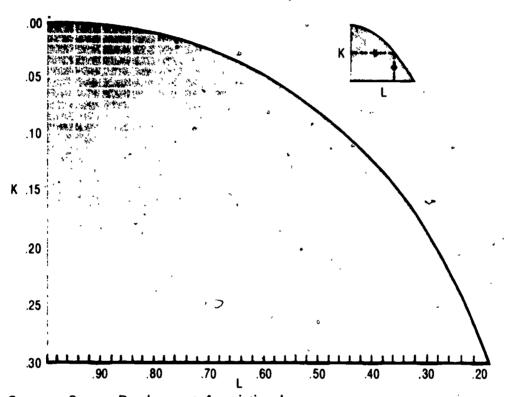
Column K:

This entry is obtained by dividing the result from Column J by the quantity from Column F; in the completed worksheet, the figure is .12; the figure in the completed worksheet is a little over 100, but call it 100



Column L: This entry is obtained by referring to the Collectable Energy Graph in Figure 3, finding the quantity obtained in Column K, then following the K axis across the graph until it intersects the curved L axis; the completed worksheet shows .42

#### FIGURE 3



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Result Column:

This entry is obtained by multiplying the values from Columns F and L; this is the amount of heat collected in Btu per square foot per day, an average day in a particular month; on the completed worksheet, the figure for January is 363.30, but call it 363; once the rate of output from the collector has been determined, the designer can proceed to find the collector area needed for a specific application

Assignment: Using the blank CDA sun-chart worksheet provided with this activity, complete the worksheet with information provided by your instructor; this information should include specific latitude, average daytime temperature, heat gain factor and heat loss factor for a given collector, necessary collector inlet temperatures, and whatever materials are necessary to complete the assignment; you may refer as needed to the sample exercise which you have just completed; when you have finished the worksheet, and just for fun, write a brief note explaining why the columns in the worksheet jump from "H" to "J" and omit the "I." Good luck.



## COMPLETED CDA SUN-CHART WORKSHEET

| JOB CDA Sol<br>LOCATION N<br>LATITUDE 36 | ashville, Ten  | nessee   | COL   | LECTOR TILT   | E Double Gla<br>51° (Latitud<br>pace and Wat           | le + 15°)                     | tive Surface                                       | _                    |                  | •    | ٩  |   |
|--|--|--|---|---|--|-------------------------------|--|----------------------|------------------|------|--|---|
|  | ^  | В  | С   | D .   | E  | F                             | G  | н                    | J '              | К    | L  | RESULT  |
| ,  | COLLECTOR<br>HEAT GAIN<br>FACTOR<br>(TABLE 8)<br>OR MFG S<br>LIT | COLLECTOR<br>HEAT LOSS<br>FACTOR ~<br>(TABLE 8)<br>OR MFG S<br>LIT | AVERAGE<br>DAYTIME<br>AIR<br>TEMPERA-<br>TURE F | HORIZONTAL<br>SOLAR<br>ENERGY<br>(FROM<br>TABLES)<br>APPENOIX B | COLLECTOR<br>TILT FACTOR<br>(FROM TABLE)<br>APPENDIX C | INCIDENT<br>ENERGY<br>F D x E | COLLECTOR<br>INLET<br>TEMPERA<br>TURE<br>(TABLE 9) | COLUMN G<br>COLUMN C | B <sub>x2H</sub> | K F  | L IS<br>FOUND FROM<br>FIGURE 41<br>USING K | TOTAL<br>ENERGY<br>COLLECTED<br>FXL<br>BTU SO<br>FT OAY |
| JANUARY                                  | 70   | 65   | 46  | 601   | 1 44 °   | 865                           | 100  | 54                   | 100              | 12   | 42   | 363   |
| FE8RUARY                                 | 70   | 65   | 48  | 882   | 1 30   | 1147                          | 115  | 67                   | 124              | 11   | 44   | 505   |
| MÅRCH                                    | 70   | · 65   | 57  | 11,88   | 1 09   | 1295                          | . 140  | 83                   | 154              | 12   | 42   | 544   |
| APRIL                                    | 70   | 65   | 67  | 1638  | 88   | 1441                          | 155  | 88                   | 163              | 11   | 44   | 634   |
| MAY                                      | 70   | 65   | 76  | 1911  | 63,  | 1204                          | , 165  | 89                   | 165              | 14   | 37   | 445   |
| JUNE ,                                   | 70   | 65   | <b>*</b> 84                                     | 2081  | <b>,</b> 61  | 1269                          | 175  | . 91 .               | 169              | 13   | 39   | 495   |
| JULY                                     | 70   | 65   | 87  | 2033  | 62   | 1260                          | 180  | 93                   | 173              | 14   | 37   | 466   |
| AUGUST                                   | 70   | 65   | 86  | 1845  | 89   | 1642                          | 180  | 94                   | 175              | 11   | 44   | 722   |
| SEPTEM8ER                                | 70   | 65   | 81  | 1561  | 1 10   | 1717                          | 175  | 94                   | 175              | 10   | 46   | 790   |
| остовієя                                 | 70   | 65   | 69  | 1199  | 1 42   | 1703-                         | 150  | 81                   | 150              | 09   | 48*  | 817   |
| NOVEMBER                                 | 70   | 65   | 55  | 808   | 1 57   | 1269                          | 130  | 75                   | 139              | 11   | 44   | 558   |
| DECEMBER                                 | 70 b   | 65 .   | 47  | 605   | 1 63   | 986                           | 105  | - 58                 | 108              | 11 , | 44   | . 434   |

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# AVERAGE MONTHLY AND YEARLY DEGREE DAYS FOR CITIES IN THE UNITED STATES AND CANADA. a.b.c.(BASE 65)

#### HOW DEGREE DAYS ARE MEASURED

A degree of tay is a standard measure used by healing engineers to measure the healing season is accidences. This combine of degree days in a calendar day is determined by subtracting the day's mean importance from 65. If the riigh on a given day was 60 and the low was 40 the mean temperature that day would be 50. Subtracted from 65, this would give 15 degree days for that calendar day.

| UNITE | D ST | ATES |
|-------|------|------|
|       |      | ~~   |

|        | <b></b>   |   |   |  |  | OHITE  | DSTA  | IES   |  |   |   |  |  |   |  |
|--------|---|---|---|--|--|--|---|---|--|---|---|--|--|---|--|
| State  | Station   | Avg<br>Winter<br>Temp F   | July                                    | Aug  | Sept   | Oct  | Nov   | Dec   | Jan  | Feb   | Mar   | Apr  | May  | June  | Yearly<br>Total  |
| Aia    | Birmingham A<br>Huntsville A<br>Mobile A<br>Montgomery A  | 54 2<br>51 3<br>59 9<br>55 4  | 0 0 0                                   | 0<br>0<br>0  | 6<br>12<br>0<br>0  | 93<br>127<br>22<br>68  | 363<br>426<br>213<br>330  | 555<br>663<br>357<br>527  | 592<br>694<br>415<br>543   | 462<br>557<br>300<br>417  | 363<br>434<br>211<br>318  | 108<br>138<br>42<br>90   | 9<br>19<br>0<br>0  | 0 0 0   | 2551<br>3070<br>1560<br>2291   |
| Alaska | Arichotage A<br>hairbanks A<br>uundau A<br>Nome A   | 230<br>67<br>321<br>131   | 245<br>171<br>301<br>481                | 291<br>332<br>338<br>496   | 516<br>642<br>483<br>693   | 930<br>1203<br>725<br>1094   | 1284<br>1833<br>921<br>1455   | 1572<br>2254<br>1135<br>1820  | 1631<br>2359<br>1237<br>1879   | 4316<br>1901<br>1070<br>1666  | 12 <b>9</b> 3<br>17 <b>3</b> 9<br>1073<br>1770  | 879<br>1068<br>810<br>1314   | 592<br>555<br>601<br>930   | 315<br>222<br>381<br>573  | 10 <b>86</b> 4<br>1427 <b>9</b><br>9075<br>14171   |
| Ariz   | Flagstaff A Phoenix A Tucson A Winslow A Yuma A   | 35 6<br>58 5<br>58 1<br>43 0<br>64 2  | 46<br>0<br>0<br>0                       | 68<br>0<br>0<br>0  | 201<br>0<br>0<br>6<br>0  | 558<br>22<br>25<br>245<br>0  | 867<br>234<br>231<br>711<br>108   | 1073<br>415<br>406<br>1008<br>264   | 1169<br>474<br>471<br>1054<br>307  | 991<br>328<br>344<br>770<br>190   | 91 67<br>217<br>242<br>601<br>90  | 651<br>75<br>75<br>291<br>15   | 437<br>0<br>6<br>96<br>0   | 2 1 <b>80</b><br>0<br>0<br>0  | 7152<br>1765<br>1800<br>4782<br>974  |
| Ark    | Fort Smith A<br>Little Rock A<br>Texarkana A  | 50 3<br>50 5<br>54 2  | 0<br>0<br>ນ                             | 0<br>0<br>0  | 12<br>9<br>0   | 127<br>127<br>78   | 450<br>465<br>345   | 704<br>716<br>561   | 781<br>756<br>626  | 596<br>577<br>468   | 456<br>434<br>350   | 144<br>126<br>105  | 22<br>9<br>0   | 0   | 3292<br>3219<br>2533   |
| Calif  | Bakersheid A Bishop Bite Canyon A Burbank Eureka C Fresno Long Beach A Los Angeles Los Angeles A Los Angeles C Oakland A Sacrament A Sacrament A Sacrament C Sandberg San Francis San Francis San Francis Santa Marix A | 55 4<br>46 0<br>42 2<br>58 6<br>49 9<br>53 3<br>57 8<br>57 4<br>60 3<br>41 2<br>53 8<br>53 8<br>53 8<br>54 8<br>6 8<br>59 5<br>53 8<br>55 8<br>55 8<br>55 8<br>55 8<br>55 8<br>56 8<br>57 8<br>57 4<br>68 8<br>58 8<br>58 8<br>58 8<br>58 8<br>58 8<br>58 8<br>58 8 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0   | 0<br>0<br>37<br>257<br>0<br>257<br>0<br>28<br>0<br>34<br>50<br>0<br>0<br>0<br>0<br>78<br>174<br>93 | 0<br>48<br>108<br>258<br>0<br>9<br>42<br>6<br>123<br>45<br>0<br>0<br>30<br>21<br>60<br>102 | 37<br>260<br>347<br>43<br>329<br>84<br>47<br>78<br>31<br>406<br>127<br>53<br>62<br>202<br>43<br>118<br>146 | 282<br>576<br>594<br>177<br>414<br>354<br>171<br>180<br>132<br>696<br>309<br>318<br>321<br>480<br>135<br>480<br>135<br>231<br>270 | 502<br>797<br>781<br>301<br>499<br>577<br>316<br>291<br>229<br>902<br>481<br>555<br>546<br>533<br>691<br>236<br>462<br>388<br>391 | 546<br>874<br>896<br>366<br>546<br>605<br>397<br>372<br>310<br>983<br>527<br>605<br>583<br>778<br>298<br>508<br>443<br>459 | 364<br>680<br>795<br>277<br>470<br>426<br>311<br>302<br>230<br>784<br>400<br>428<br>414<br>392<br>661<br>235<br>395<br>336<br>370 | 267<br>5555<br>806<br>239<br>505<br>335<br>264<br>202<br>738<br>353<br>341<br>332<br>310<br>620<br>214<br>363<br>319<br>363 | 105<br>306<br>597<br>138<br>162<br>171<br>219<br>123<br>525<br>168<br>173<br>426<br>135<br>279<br>279<br>282 | 19<br>143<br>412<br>81<br>372<br>62<br>93<br>158<br>88<br>347<br>180<br>47<br>76<br>264<br>90<br>214<br>239<br>233 | 0<br>36<br>195<br>18<br>285<br>8<br>24<br>81<br>159<br>90<br>0<br>0<br>0<br>57<br>42<br>126<br>180<br>165 | 2122<br>4275<br>5596<br>1846<br>4643<br>2811<br>1803<br>2061<br>1348<br>5722<br>2870<br>2515<br>2502<br>2419<br>4209<br>1458<br>3015<br>3001<br>2867 |
| Colo   | Alamosa A<br>Colorado Springs A<br>Denver A<br>Denver C<br>Gran filinction A<br>Pueblo A  | 29 7<br>37 3<br>37 6<br>40 8<br>39 3<br>40 4  | 65<br>9<br>6<br>U<br>0                  | 99<br>25<br>9<br>0<br>0  | 279<br>132<br>117<br>90<br>30<br>54  | 639<br>456<br>428<br>366<br>313<br>326   | 1065<br>825<br>819<br>714<br>786<br>750   | 1420<br>1032<br>1035<br>905<br>1113<br>986  | 1476<br>1128<br>1132<br>1004<br>1209<br>1085   | 1162<br>936<br>938<br>951<br>907<br>871   | 1020<br>693<br>687<br>800<br>729<br>772   | 696<br>582<br>558<br>492<br>387<br>429   | 440<br>319<br>268<br>254<br>146<br>174   | 168<br>64<br>66<br>48<br>21<br>15   | 8529<br>6423<br>6283<br>5524<br>5641<br>5462   |
| Conn   | Bridgept d A<br>Hardord A<br>New Haver A  | 39 9<br>37 3<br>39 0  | 000                                     | 0<br>12<br>12  | 66<br>11 <b>7</b><br>87  | 307<br>394<br>347  | 615<br>714<br>648   | 986<br>1101<br>1011   | 1079<br>1190<br>1097   | 966<br>1042<br>991  | 853<br>908<br>871   | 510<br>519<br>543  | 208<br>205<br>245  | 27<br>33<br>45  | 5617<br>6235<br>5897   |
| Del    | Wilmington A  | 42 5  | υ                                       | 0  | 51   | 270  | 588   | 927   | 980  | 874   | 735   | 387  | 112  | 8   | 4930   |
| DC     | Aushington A  | 45 7.   | 0 ,                                     | ú  | 33   | 217  | 519   | 834   | 871  | 79  | 626   | 268  | 74   | 0   | 4224   |
| Fia    | At arachicilia C<br>Ouytona Beach A<br>Frind Myers A<br>Jakinson Julie A<br>Key West A<br>Lakin and C<br>Mami A<br>Mami A<br>Mami A<br>Man Beach C<br>Originato A<br>Prinsia 1 A<br>Tampai A<br>West Paim Bellinia A    | 61 2<br>64 5<br>68 6<br>61 9<br>73 1<br>66 7<br>71 1<br>72 5<br>65 7<br>60 1<br>66 4<br>68 4  | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000  | 00000000000000   | 16<br>0<br>0<br>12<br>0<br>0<br>0<br>0<br>19<br>28   | 153<br>75<br>24<br>144<br>-0<br>57<br>0<br>72<br>195<br>198<br>60   | 319<br>211<br>109<br>310<br>28<br>164<br>65<br>40<br>198<br>353<br>360<br>171<br>65   | 347<br>248<br>146<br>332<br>40<br>195<br>74<br>56<br>220<br>400<br>375<br>202<br>87  | 260<br>100<br>101<br>246<br>31<br>146<br>56<br>36<br>165<br>277<br>286<br>148   | 140<br>62<br>174<br>9<br>99<br>19<br>105<br>103<br>202<br>102<br>31   | 33<br>15<br>0<br>21<br>0<br>0<br>0<br>0<br>6<br>36<br>36<br>0  | 000000000000   | 000000000000  | 1308<br>679<br>442<br>1239<br>108<br>661<br>214<br>141<br>766<br>1463<br>1485<br>683<br>253  |

Reprinted from ASHRAE 1973 Systems Handbook Chapter 43 Energy Estimating Method

a Dat 11 condent of this present area, on the after of the United States Weather Bureau Mchhily North present in the containing and the ating Degree Days 1960, are for this present and 1991 of the fine fusive. These data also include information from the 1969 Brinsound for this publication, where available.

Dara for a ipum statili si Allandi ity statilni i ji are buth given where available

Data for Canadian cries where computed by the Climatology Division. Depart ment of Transport from normal monthly mean temperatures and/the monthly values of healing degree days data were obtained using the National Research Council computer and a method devised by H.C.S. Thorn of the United States We ather Bureau. The healing degree days are based on the period from 1931 to 1960.



# AVERAGE MONTHLY AND YEARLY DEGREE DAYS, CONTINUED

| State     | Station  | Avg<br>Winter<br>Temp °F                                     | July                                      | Aug  | Sept  | Oct  | Nov  | Dec  | Jan   | Feb  | Mar  | Apr  | Мау  | June  | Yearty<br>Total  |
|-----------|--|--|---|--|---|--|--|--|---|--|--|--|--|---|--|
| Ga.       | Athens A<br>Atlanta A<br>Augusta A<br>Columbus A<br>Macon<br>Rome A<br>Savannah<br>Thomasville C                       | 51 7<br>54 5<br>54 8<br>56 2<br>48 8                         | 0,00000                                   | 0<br>0<br>0<br>0<br>0                        | 12<br>18<br>0<br>0<br>0<br>24<br>0                  | 115<br>124<br>78<br>87<br>71<br>161<br>47<br>25      | 405<br>417<br>333<br>333<br>297<br>474<br>246<br>198   | 632<br>648<br>552<br>543<br>502<br>701<br>437<br>366         | 642<br>636<br>549<br>552<br>505<br>710<br>437<br>394        | 529<br>518<br>445<br>434<br>403<br>577<br>353<br>305         | 431<br>428<br>350<br>338<br>295<br>469<br>254<br>208       | 141<br>147-<br>90<br>96<br>63<br>177<br>45<br>33     | 22<br>25<br>0<br>0<br>0<br>34<br>0                   | 0<br>0<br>0<br>0                                | 2929<br>2961<br>2397<br>2383<br>2136<br>3326<br>1819<br>1529 |
| Hawas     | Libue A<br>Honolulu A<br>Hilo A  | 742  | g,  | 0 0  | 0 0   | 0 0  | 0  | 0 0  | 0   | 0  | 0 0  | 0 0  | 0  | 0 0   | 0  |
| Ideho     | Boise A<br>Lewiston A<br>Pocatello A   | 39 7<br>41 0<br>34 8   | 0<br>0<br>0                               | 0  | 132<br>123<br>172                                   | 415<br>403<br>493                                    | 792<br>756<br>900                                      | 1017<br>933<br>1166  | 1113<br>1063<br>1324  | 854<br>815<br>1058   | 722<br>694<br>905  | 438<br>426<br>555                                    | 245<br>239<br>319                                    | 81<br>90<br>141                                 | 5809<br>5542<br>7033   |
| <b>12</b> | Cairo C<br>Chicago (O Hare ) A<br>Chicago (Midway) A<br>Chicago<br>Moline A<br>Peoria A<br>Rockford A<br>Springfield A | 47 8<br>35 8<br>37 5<br>38 8<br>36 4<br>36 1<br>34 8<br>40 6 | 0<br>0<br>0<br>0<br>0<br>0<br>6           | 0<br>12<br>0<br>0<br>9<br>6                  | 36<br>117<br>81<br>68<br>99<br>87<br>114<br>72      | 164<br>381<br>326<br>279<br>335<br>326<br>400<br>291 | 513<br>807<br>753<br>705 ><br>774<br>759<br>837<br>696 | 791<br>1166<br>1113<br>1051<br>1181<br>1113<br>1221<br>1023  | 856<br>1265<br>1209<br>1150<br>1314<br>1218<br>1333<br>1135 | 680<br>1086<br>1044<br>1000<br>1100<br>1025<br>1137<br>935   | 539<br>939<br>890<br>868<br>918<br>849<br>961<br>769       | 195<br>534<br>480<br>489<br>450<br>426<br>516<br>354 | 47<br>260<br>211<br>226<br>189<br>183<br>236<br>136  | 0<br>72%<br>48<br>46<br>39<br>33<br>60          | 3821<br>6639<br>6155<br>5882<br>6408<br>6025<br>6830<br>5429 |
| ind .     | Evansville A Fort Wayne A Indianapolis A South Bend A  | 45 0<br>37 3<br>30 6<br>36 6                                 | 0<br>0<br>0                               | 0<br>9<br>0<br>6                             | 66<br>105<br>90<br>111                              | 220<br>378<br>316<br>372                             | 606<br>783<br>723<br>777                               | 896<br>1135<br>1051<br>1125                                  | 955<br>1178<br>1113<br>1221                                 | 767<br>1028<br>949<br>1070                                   | 620<br>890<br>809<br>933                                   | 237<br>471<br>432<br>525                             | 68<br>189<br>177<br>239                              | 0<br>39<br>39<br>60                             | 4435<br>6205<br>5699<br>6439                                 |
| lowa '    | Burlington A Des Moines A Dubuque A Sioux City A Waterloo A  | 37 6<br>35 5<br>32 7<br>34 0<br>32 6                         | 0<br>0<br>12<br>0<br>12                   | 0<br>6<br>31<br>9                            | 93<br>961<br>156<br>108<br>138                      | 322<br>363<br>450<br>369<br>428                      | 768<br>828<br>906<br>867<br>909                        | 1135<br>1225<br>1287<br>1240<br>1296                         | 1259<br>1370<br>1420<br>1435<br>1460                        | 1042<br>1137<br>1204<br>1198<br>1221                         | 859<br>915<br>1026<br>989<br>1023                          | 426<br>438<br>546<br>483<br>531                      | 177<br>180<br>260<br>214<br>219                      | 33<br>30<br>78<br>39<br>54                      | 6114<br>6588<br>7376<br>6951<br>7320                         |
| Kans      | Concordia A Dodge City A Goodland A Topeka A Wichita A   | 40 4<br>42 5<br>37 8<br>41 7<br>44 2                         | 0<br>0<br>0<br>0                          | 0<br>6<br>0                                  | 57<br>33<br>81<br>57<br>33                          | 276<br>251<br>381<br>270<br>229                      | 705<br>666<br>810<br>672<br>618                        | 1023<br>939<br>1073<br>980<br>905                            | 1163<br>1051<br>1166<br>1122<br>1023                        | 935<br>840<br>955<br>893<br>804                              | 781<br>719<br>884<br>722<br>645                            | 372<br>354<br>507<br>330<br>270                      | 14<br>12<br>236<br>124<br>87                         | 1 <b>6</b><br>9<br>42<br>12<br>6                | 54791<br>49 <b>86</b><br>6141<br>5182<br>4620                |
| Ку        | Covington A<br>Lexington A<br>Louisville A   | 41 4<br>43 8<br>44 0   | 0<br>0<br>0                               | 0 0  | 75<br>54<br>54                                      | 291<br>239<br>248                                    | 669<br>609<br>609                                      | 983<br>902<br>890  | 1035<br>946<br>930  | 893<br>818<br>818  | 756<br>685<br>682  | 390<br>325<br>315                                    | 149<br>105<br>105                                    | 24<br>0<br>9                                    | 5265<br>4683<br>4660   |
| La-       | Alexandria A Baton Rotige A Lake Charles A New Orleans A New Orleans C Shreveport A                                    | 57.5<br>58.8<br>60.5<br>61.0<br>81.8<br>56.2                 | ,<br>000000                               | 000000                                       | 300000  | 56<br>31<br>19<br>19<br>12<br>47                     | 273<br>216<br>210<br>192<br>165<br>297                 | 431<br>369<br>341<br>322<br>291<br>477                       | 471<br>409<br>381<br>363<br>344<br>552                      | 361<br>294<br>274<br>258<br>241<br>426                       | 260<br>208<br>195<br>192<br>177<br>304                     | 69<br>33<br>39<br>39<br>24<br>81                     | 0<br>0<br>0<br>0<br>0                                | 0 0 0   | 1921<br>1560<br>1459<br>1385<br>1254<br>2184                 |
| Me        | Caribou A<br>Portland A  | 24 4<br>33 0   | 78<br>12                                  | 115<br>4 53                                  | 336<br>195  | 582<br>508   | 1044<br>807  | 1535<br>1215   | 1690<br>1339  | 1470<br>1182   | 130 <b>8</b><br>1042 -                                     | 858 °<br>675   | 46 <b>8</b><br>372                                   | 183<br>111                                      | 9767<br>7511   |
| Md        | Battimore A<br>Battimore C<br>Frederich A  | 43 7<br>46 2<br>42 0   | , 0                                       | 0<br>0<br>0                                  | 48<br>27<br>66                                      | 264<br>189<br>307                                    | 585<br>486<br>624                                      | 905<br>806<br>955  | 936<br>859<br>995   | 820<br>762<br>876  | 679<br>629<br>741  | 327<br>288<br>384                                    | 90<br>65<br>127                                      | 0<br>0<br>12                                    | 4654<br>4111<br>5087   |
| Mass      | Boston A Nantucket A Pittsfield A Worcester A  | 40 0<br>40 2<br>32 6<br>34 7                                 | 0<br>12<br>25<br>6                        | 9<br>22<br>59<br>34                          | 60<br>93<br>219<br>147                              | 316<br>332<br>524<br>450                             | 603<br>573<br>831<br>774                               | 983<br>896<br>1231<br>1172                                   | 1088<br>992<br>1339<br>1271                                 | 972<br>941<br>1196<br>1123                                   | 846<br>896<br>1063<br><del>9</del> 98                      | 513<br>621<br>660<br>612                             | 208<br>384<br>326<br>304                             | 36<br>129<br>105<br>78                          | 5634<br>5891<br>7578<br>6969                                 |
| Mich      | Alpena A Detroit (City) A Detroit (Wayne) A Detroit (Willow  | 29 7<br>37 2<br>37 1   | 68<br>0<br>0                              | 105<br>0<br>0                                | 273<br>87 ¢<br>96                                   | 580<br>360<br>353                                    | 912<br>738<br>738                                      | 1268<br>1088<br>1088   | 1404<br>1181<br>1194  | 1299<br>1058<br>1061   | 1218<br>936<br>933   | 777<br>522<br>534                                    | 446<br>220<br>239                                    | 156<br>42<br>57                                 | 8506<br>6232<br>6293   |
|           | Run) A Escanaba C Fint A Grand Rapids Lansing A Marquette C Muskegon A Sault Ste Marge                                 | 37 2<br>29 6<br>33 1<br>34 9<br>34 6<br>30 2<br>36 0<br>27 7 | 0<br>59<br>16<br>9<br>6<br>59<br>12<br>96 | 0<br>87<br>40<br>28<br>22<br>81<br>28<br>105 | 90<br>243<br>159<br>135<br>138<br>240<br>120<br>279 | 357<br>539<br>465<br>434<br>431<br>527<br>400<br>580 | 750<br>924<br>843<br>804<br>813<br>936<br>762<br>951   | 1104<br>1293<br>1212<br>1147<br>1163<br>1268<br>1088<br>1367 | 1190<br>1445<br>1330<br>1259<br>1262<br>1411<br>1209        | 1053<br>1296<br>1198<br>1134<br>1142<br>1268<br>1100<br>1380 | 921<br>1203<br>1066<br>1011<br>1011<br>1187<br>995<br>1277 | 519<br>777<br>639<br>579<br>579<br>771<br>594<br>810 | 229<br>456<br>319<br>279<br>273<br>468<br>310<br>477 | 45<br>159<br>90<br>75<br>69<br>177<br>78<br>201 | 6258<br>8481<br>7377<br>6894<br>6909<br>8393<br>6696<br>9048 |
| Minn      | Duluth A<br>Minneapolis A_<br>Rochester A  | 23 4<br>20 3<br>28 6   | 71<br>22<br>25                            | 109<br>31<br>34                              | 330<br>189<br>186                                   | 632<br>_505_<br>_474                                 | 1131<br>1014<br>1005                                   | 1581<br>1454<br>1438   | 1745<br>1631<br>1593  | 1518<br>1380<br>1366   | 1355<br>1166<br>1150                                       | 840<br>621<br>630                                    | 490<br>288<br>301                                    | 198<br>81_<br>93                                | 10000<br>8382<br>8295  |
| Miss      | Jackson A<br>Meridian A<br>Vicksburg C   | 55 7<br>55 4<br>56 9   | 0 0                                       | 0  | 0<br>0<br>0   | 65<br>81<br>53                                       | 315<br>339<br>279                                      | 502<br>518<br>462  | 546<br>543<br>512   | 414<br>417<br>384  | 310<br>310<br>282  | 87<br>81<br>69                                       | Ð<br>0<br>0  | 0 0   | 2239<br>2289<br>2041   |
| Mo        | Columbia A<br>Kansas City A<br>St Joseph A<br>St Louis A   | 423<br>439<br>403<br>431                                     | 0 0                                       | 0<br>0<br>6                                  | 54<br>39<br>60<br>60                                | 251<br>220<br>285<br>251                             | 651<br>612<br>708<br>627                               | 967<br>905<br>1039<br>936                                    | 1076<br>1032<br>1172<br>1026                                | 874<br>818<br>949<br>848                                     | 716<br>682<br>769<br>704                                   | 324<br>294<br>348<br>312                             | 121<br>109<br>133<br>121                             | 12<br>0<br>15<br>15                             | 5046<br>4711<br>5484<br>4900                                 |

## AVERAGE-MONTHLY AND YEARLY DEGREE DAYS, CONTINUED

| State      | Station   |  | July                                       | Aug  | Sept   | Oct  | Nov  | Dec  | Jan   | Feb   | Mar  | Apr  | May   | June   | Yearly<br>Total  |
|------------|---|--|--|--|--|--|--|--|---|---|--|--|---|--|--|
|            | St Louis C<br>Springfield A   | 44 8<br>44 5   | υ<br>0                                     | 0  | 36<br>45   | 202<br>223   | 576<br>600   | 884<br>877   | 977<br>973  | 801<br>781  | -651<br>660  | 270<br>291   | 87<br>105   | o`<br>6  | 4484<br>4900   |
| Mont       | Billings A Glasgew A Great Fail's A Havre A Havre C Helena A Katispell A Miles City A Missoula A                          | 34 5<br>26 4<br>32 8<br>28 1<br>29 8<br>31 1<br>31 4<br>31 2<br>31 5         | 6<br>31<br>78<br>78<br>19<br>31<br>50<br>6 | 15 /<br>47<br>53<br>53<br>3*<br>59<br>99<br>6'<br>74 | 186<br>270<br>258<br>306<br>252<br>294<br>321/<br>174<br>303 | 487<br>608<br>543<br>595<br>539<br>601<br>654<br>502<br>65T        | 89°<br>1104<br>921<br>1065<br>1014<br>1002<br>1020<br>972<br>1035  | 1135<br>1466<br>1169<br>1367<br>1321<br>1265<br>1240<br>1296<br>1287 | 1296<br>1711 -<br>1349<br>1584<br>1528<br>1438<br>1401<br>1504<br>1420      | 1100<br>1439<br>1154<br>1364<br>1305<br>1170<br>1134<br>1252<br>1120    | 970<br>1187<br>1063<br>1181<br>1116<br>1042<br>1029<br>1057<br>970 | 570<br>648-<br>642<br>657<br>612<br>651<br>639<br>579<br>621       | 385<br>335<br>384<br>338<br>304<br>381<br>397<br>276<br>391       | 102<br>150<br>186<br>162<br>135<br>195<br>207<br>99<br>219 | 7049<br>8996<br>7750<br>8700<br>8182<br>8129<br>8191<br>7723<br>8125         |
| Neb        | Grand Island A Lincoln C Norfolk A North Platte A Scottsbluth A Valentine A   | 36 0<br>38 8<br>34 0<br>35 5<br>35 6<br>35 9<br>32 6                         | 9000                                       | 6<br>6<br>0<br>6<br>12<br>0                          | 108<br>75<br>111<br>123<br>105<br>138<br>165                 | 381<br>301<br>397<br>440<br>357<br>459<br>493                      | 834<br>726<br>873<br>885<br>828<br>876<br>942                      | 1172<br>1066<br>1234<br>1166<br>1175<br>1128<br>1237                 | 1314 <sup>2</sup><br>1237<br>1414<br>1271<br>1355<br>1231<br>1395           | 1089<br>1016<br>1179<br>1039<br>1126<br>1008<br>1176                    | 908<br>834<br>983<br>930<br>939<br>921<br>1045                     | 462<br>402<br>498<br>519<br>465<br>552<br>579                      | 211<br>171<br>(933<br>248<br>208<br>285<br>285<br>288             | 45<br>30<br>48<br>57<br>42<br>75<br>84                     | 6530<br>5864<br>6979<br>6684<br>6612<br>6673<br>7425                         |
| Nev .      | Elko A<br>Ely A<br>Las Vegas A<br>Reno A<br>Winnemucca A  | 34 0<br>33 1<br>53 5<br>39 3<br>36 7   | 9<br>28<br>0<br>43<br>0                    | 34<br>43<br>0<br>87<br>34                            | 225<br>234<br>0<br>204<br>210                                | 561<br>592<br>78<br>490<br>536                                     | 924<br>939<br>387<br>801<br>876                                    | 1197<br>1184<br>617<br>1026 <del>9</del>                             | 1314<br>1308 /<br>688<br>1073<br>1172                                       | 1036<br>1075<br>487<br>823<br>916                                       | 911<br>977<br>335<br>729<br>837                                    | 621<br>672<br>111<br>510<br>573                                    | 409<br>456<br>6<br>357<br>363                                     | t92<br>225<br>0<br>189<br>153                              | 7433<br>7733<br>2709<br>6332<br>6761   |
| NH         | Concord A Mt Washington Obsv  | 33 0<br>15 2   | 6<br>493                                   | 50<br>536  | 177<br>720   | 505<br>1057  | 822<br>1341  | 1240 ,<br>1742   | 1358<br>1820  | 1184 1<br>1663  | 1032   | 636<br>1260  | 298<br>930  | 75<br>603  | 7383<br>13817  |
| NJ         | Atlantic City A Newark A Trenton C  | 43 2<br>42 8<br>42 4   | 0  | 0 -  | 39<br>30<br>57   | 251<br>248<br>264  | 549<br>573<br>576  | 880<br>921<br>924  | 936<br>983<br>989   | 848<br>876<br>885   | 741<br>729<br>753  | 420<br>381<br>399  | 133<br>118<br>121   | 15<br>0<br>12  | 4812<br>4589<br>4980   |
| N M        | Albuquerque A<br>Clayton A<br>Raton A<br>Rosweii A<br>Silver Çity A   | 45 0<br>42 0<br>38 1<br>47 5<br>48 0   | 0 0 9 0                                    | 0<br>6<br>28<br>0                                    | 12<br>66<br>126<br>18  | 229<br>310<br>431<br>202<br>183                                    | 642<br>699<br>825<br>573<br>525                                    | 868<br>899<br>1048<br>806<br>729                                     | 930<br>986<br>1116<br>840<br>791 •  | 703<br>812<br>904<br>641<br>605   | 595<br>747<br>834<br>481<br>518                                    | 288<br>429<br>543<br>201<br>261                                    | 81<br>183<br>301<br>31<br>87                                      | 0<br>21<br>63<br>0   | 4348<br>5458<br>6228<br>3793<br>3705   |
| NY         | Albany A Albany C Binghamton A Binghamton C Bulfako A   | 34 6<br>37 2<br>33 9<br>36 6<br>34 5   | 0<br>0<br>22<br>0                          | 19<br>9<br>65<br>28<br>37                            | 138<br>102<br>201<br>141<br>~141                             | 440<br>375<br>471<br>406<br>440                                    | 777<br>699<br>810<br>-732<br>-777                                  | 1194<br>1104<br>1184<br>110*<br>1156                                 | 1311<br>1218<br>1207<br>1190<br>1256  | 1156<br>1072<br>11 54<br>1081<br>1145                                   | 992<br>908<br>1045<br>949<br>1039                                  | 564<br>498<br>645<br>543<br>645                                    | 239<br>186<br>313<br>229<br>329                                   | 45<br>30<br>99<br>45<br>78                                 | 6875<br>6201<br>7286<br>6451<br>7062   |
|            | New York (Cent<br>Park)<br>New York (La   | 42.8   | 0 .  | 0  | 30   | 233  | 540  | 902  | 986   | 885   | 760  | 408  | 118   | 9  | 4871   |
|            | Guardiai A<br>New York<br>Kennnedyi A<br>Rochester A<br>Schennedady C<br>Syracuse A                                       | 43 1<br>41 4<br>35 4<br>35 4<br>35 2   | 0<br>9<br>0<br>0                           | 0<br>31<br>22<br>28                                  | 36<br>126<br>123<br>132                                      | 248<br>415<br>422<br>415   | 528<br>564<br>747<br>756<br>744                                    | 933<br>1125<br>1159<br>1153  | 973<br>1029<br>1234<br>1283<br>1271   | 935<br>1123<br>1131<br>1140   | 750<br>815<br>1014<br>970<br>1004                                  | 414<br>480<br>597<br>543<br>570                                    | 124<br>167<br>279<br>211<br>248                                   | 6<br>12<br>48<br>30<br>45                                  | 4811<br>5219<br>6748<br>6650<br>6756   |
| NC         | Asheville C<br>Cape Hatteras<br>Charlotte A<br>Greensboro A<br>Raleigh A<br>Wimington A<br>Winston Salem A                | 46 7<br>53 3<br>50 4<br>47 5<br>49 4<br>54 6<br>48 4                         | 0 0 0 0 0 0                                | 0<br>0<br>0<br>0<br>0                                | 48<br>0<br>6<br>33<br>21<br>0<br>21                          | 215<br>78<br>124<br>192<br>164<br>74<br>171                        | 555<br>273<br>438<br>513<br>450<br>291<br>483                      | 775<br>521<br>691<br>778<br>716<br>521<br>747                        | 784<br>580<br>691<br>784<br>725<br>546<br>753                               | 683<br>518<br>582<br>672<br>616<br>462<br>652                           | 592<br>440<br>481<br>552<br>487<br>357<br>524                      | 273<br>177<br>156<br>234<br>180<br>96<br>207                       | 87<br>25<br>22<br>47<br>34<br>0<br>37                             | 0<br>0<br>0<br>0<br>0                                      | 4042<br>2612<br>3191<br>3805<br>3393<br>2347<br>3595                         |
| <b>N</b> D | Bismarck A<br>Deviis Lake C<br>Fargo A<br>Williston A   | 26 6<br>22 4<br>24 8<br>25 2   | 34<br>46<br>28                             | 28<br>53<br>37<br>43                                 | 222<br>273<br>219<br>261                                     | 577<br>642<br>574<br>601   | 10 <b>8</b> 3<br>1191<br>1107<br>1122                              | 1463<br>1634<br>1569<br>1513   | 1708 *<br>1872<br>1789<br>1758  | 1442<br>1579<br>1520<br>1473  | 1203<br>1345<br>1262<br>1262                                       | 645<br>753<br>690<br>681   | 329<br>381<br>332<br>357  | 117<br>138<br>99<br>141                                    | 6851<br>9901<br>9226<br>9243   |
| Ohio       | Akron Canton A Cocionnati G Cleveland A Columbus C Columbus C Oayt in A Main theid A S induster C Toli do A You gistown A | 38 1<br>45 1<br>37 2<br>39 7<br>41 5<br>39 8<br>36 9<br>39 1<br>36 4<br>36 8 | 0 0 0 0 0 6                                | 9 ***<br>25<br>6<br>0<br>6<br>22<br>8<br>16<br>19    | 96<br>39<br>105<br>84<br>57<br>78<br>114<br>66<br>117<br>120 | 381<br>208<br>384<br>347<br>285<br>310<br>397<br>313<br>406<br>412 | 726<br>558<br>738<br>714<br>651<br>696<br>768<br>684<br>792<br>771 | 10.0<br>.862<br>1088<br>1039<br>977<br>1045<br>1110<br>1032<br>1138  | 1138<br>915<br>1159<br>1088<br>1032<br>1097<br>1169<br>1107<br>1200<br>1169 | 1016<br>790<br>1047<br>949<br>902<br>955<br>1042<br>991<br>1056<br>1047 | 871<br>642<br>918<br>809<br>760<br>809<br>924<br>868<br>924<br>921 | 489<br>294<br>552<br>426<br>396<br>429<br>543<br>495<br>543<br>540 | 202<br>96<br>260<br>171<br>136<br>167<br>245<br>198<br>242<br>248 | 39<br>66<br>66<br>27<br>15<br>30<br>60<br>36<br>60         | 6037<br>4410<br>6351<br>5660<br>5211<br>5622<br>6403<br>5796<br>6494<br>6417 |
| Ohla       | Okiahoma City A<br>Tulsa A  | 48.3<br>47.7   | <u>0</u>                                   | - 0  | 15<br>18   | 164<br>158   | 498<br>522   | 766<br>787   | 86 <u>8</u><br>893  | 664<br>683  | 527<br>539   | 189<br>213   | _34<br>_47  | <u>0</u> -   | 3725<br>3860   |
| Ore        | Astoria A<br>Burns C<br>Eligenii A<br>Mischam A<br>Medford A<br>Pendleton A<br>Portland A<br>Portland C                   | 45 6<br>35 9<br>45 6<br>34 2<br>43 2<br>42 6<br>45 6<br>47 4                 | 146<br>12<br>34<br>84<br>0<br>0<br>25      | 130*<br>37<br>34<br>124<br>0<br>0<br>28              | 210<br>210<br>129<br>288<br>78<br>111<br>114<br>*5           | 375<br>515<br>366<br>580<br>372<br>350<br>335<br>267               | 561<br>86<br>585<br>918<br>678<br>711<br>597                       | 679<br>1113<br>719 -<br>1041<br>871<br>884<br>735<br>679             | 753<br>1246<br>803<br>1209<br>918<br>101<br>825<br>769                      | 622<br>988<br>627<br>1005<br>647<br>773<br>644<br>594                   | 636<br>856<br>589<br>983<br>642<br>61*<br>586<br>536               | 480<br>570,<br>426<br>26<br>432<br>396<br>396<br>351               | 363<br>366<br>279<br>527<br>242<br>205<br>245<br>198              | 231<br>177<br>135<br>339<br>78<br>63<br>105<br>78          | 5186<br>6957<br>4726<br>7874<br>5008<br>5127<br>4635<br>4109                 |



132.

# AVERAGE MONTHLY AND YEARLY DEGREE DAYS, CONTINUED

|          | T  | Avg  | -T                                      |   | -1                                      |  | <del>y</del>   |  | ·   | *   |  |   |   |  |   |   |
|----------|--|--|---|---|---|--|--|--|---|---|--|---|---|--|---|---|
| State    | Station  | Winte  |   | Aug                                     | Ser                                     | N 00   | 1 Nov  | De   | □ Ja:   | n Fe  | b Mar  | Ap  | Ma  | y Jui  | ne Yearly<br>Total  |   |
|          | Roseburg<br>Salem  | A 45 4   |   | 16<br>31                                |   |  |  |  |   |   |  |   |   |  |   |   |
| Pa       | Pittsburgh<br>Pittsburgh<br>Reading<br>Scranton  | A 389<br>A 368<br>A 412<br>A 418<br>C 445<br>A 384<br>C 422<br>C 424<br>A 372<br>A 385   | 000000000000000000000000000000000000000 | 0<br>25<br>0<br>0<br>0<br>9<br>0<br>0   | 102                                     | 2 391<br>298<br>297<br>205<br>375<br>291<br>257  | 714<br>648<br>626<br>513<br>726<br>615<br>597<br>762   | 106<br>993<br>963<br>1063<br>1063<br>1063<br>1104  | 3 116<br>2 104<br>5 101<br>6 92<br>3 111<br>9 98<br>1 100   | 6 100<br>9 108<br>5 90<br>6 88<br>4 82<br>9 100<br>3 88<br>1 88<br>102  | 02 849<br>973 766<br>19 747<br>3 191<br>2 874<br>5 763<br>5 735<br>8 893 | 471<br>3 585<br>3 396<br>3 392<br>351<br>4 480<br>3 390<br>3 372<br>4 98  | 167<br>288<br>124<br>118<br>93<br>195<br>124<br>105 | 3 66<br>46<br>46<br>31<br>11<br>12<br>12<br>13 | 4 5810<br>0 6451<br>2 5251<br>0 5144<br>0 4486<br>9 5987<br>2 5053<br>0 4945<br>8 6254  |   |
| RI       |  | à 40 1<br>A 38 8   | 0                                       | 16<br>16                                | 78<br>96                                | 307<br>372   | 594<br>660   | 902  | 102   | 95  | 5 877  | 612   | 344   | . 99   | 5804  |   |
| sc       | Charleston Columbia Florence Greenville  | 56 4<br>57 9<br>54 0<br>54 5   | 0 0 0                                   | 0000                                    | 0000                                    | 59<br>34<br>84<br>78   | 282<br>210<br>345<br>315   | 471<br>425<br>577<br>552   | 48<br>44;<br>570  | 7 389<br>3 36<br>3 479  | 9 291<br>7 273<br>0 357  | 534<br>54<br>42<br>81<br>84   | 236<br>0<br>0<br>0                                  | 0  | 5954<br>2033<br>1794<br>2484  | 1 |
| so       | Huron  | 28 8<br>33 4   | 9                                       | 12                                      | 165                                     | 121<br>508   | 1014   | . 1432   | 1628  | , ,   | - 1  | 132   | 19  | 0  | ,   | Ì |
| Tenn     | Sioux Fails  | 30 6   | 22<br>19                                | -12<br>25                               | 165<br>168                              | 481<br>462   | 897<br>972   | 1172   | 1333<br>1544  | 1145  | 1051   | 615<br>573  | 326<br>270  | 126<br>78                                      | 7345  |   |
|          | Bristol Chartenooga Knoxville Memphis Memphis Nashville A  | 503<br>492<br>505<br>516<br>489  | 0<br>0<br>0<br>0<br>0                   | 000000                                  | 51<br>18<br>30<br>18<br>12<br>30<br>39  | 236<br>143<br>171<br>130<br>102<br>158<br>192  | 573<br>468<br>489<br>447<br>396<br>495<br>531  | 828<br>698<br>725<br>698<br>648<br>732<br>772  | 828<br>722<br>732<br>729<br>710<br>778<br>778   | 577<br>613<br>585   | 453<br>493<br>456<br>434<br>512  | 261<br>198<br>198<br>147<br>129<br>189  | 68<br>25<br>43<br>22<br>16<br>40                    | 000000000000000000000000000000000000000        | 3254<br>3494<br>3232<br>3015<br>3578  |   |
| Tex      | Ablene Amarillo Amarillo Auslin Brownsville Corpus Christi Oallag El Plaso Afort Worth Galveston Galveston Houston Houston Houston Lubbock Midland Aport Arthur San Angelo San Antonio Victoria Waco A Wichila Falls A | 53 9<br>47 0<br>59 1<br>67 7<br>64 6<br>55 3<br>52 9<br>55 1<br>62 0<br>66 0<br>68 0<br>48 8<br>60 5<br>60 1<br>62 7<br>75 7 2<br>55 3 0 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 99<br>205<br>31<br>0<br>0<br>62<br>84<br>65<br>6<br>0<br>0<br>174.<br>87<br>22<br>68<br>31<br>68<br>31<br>43<br>99 | 366<br>570<br>225<br>66<br>120<br>321<br>414<br>147<br>138<br>165<br>105<br>513<br>381<br>204<br>150<br>270<br>381 | 586<br>797<br>388<br>149<br>220<br>524<br>648<br>536<br>276<br>277<br>288<br>217<br>744<br>592<br>329<br>536<br>363<br>270<br>456<br>632 | 642<br>877<br>468<br>205<br>201<br>601<br>685<br>614<br>360<br>350<br>384<br>363<br>267<br>428<br>341<br>516<br>698 | 470<br>664<br>325<br>106<br>174<br>440<br>445<br>263<br>258<br>258<br>134<br>613<br>466<br>274<br>413<br>286<br>230<br>30<br>30<br>30<br>31<br>31<br>31<br>31<br>31 | 347<br>546<br>223<br>74<br>109<br>319<br>319<br>319<br>189               | 228<br>114<br>252<br>51<br>0<br>90<br>105<br>99<br>93<br>33<br>30<br>0<br>201<br>90<br>39<br>66<br>69<br>21<br>51 | 56<br>000000000000000000000000000000000000          | 000000000000000000000000000000000000000        | 3617<br>2624<br>3985<br>3985<br>600<br>914<br>2363<br>2700<br>2405<br>1274<br>1236<br>1276<br>797<br>3578<br>2591<br>1147<br>2255<br>1546<br>1173<br>2030<br>2832 |   |
| Utah     | Milford A Salf Lake-City A Wendover A  | 36 5<br>38 4<br>39 1   | 0<br>0<br>0                             | 0                                       | 99<br>81<br>48                          | 443<br>419<br>372  | 867<br>849<br>827  | . 1141<br>1082<br>1091   | 1252<br>1172<br>1178  | 988<br>910<br>902   | 922<br>763<br>729  | 419<br>408  | 279<br>233<br>171                                   | 8 <sup>7</sup><br>84<br>51                     | 649.7<br>6052<br>57.78  |   |
| VI<br>Va | Burlington A Cape Henry C  | 29 4<br>50 0   | 28                                      | 65 °                                    | 207                                     | 539  | 891  | 1349   | 1513  | 1 133   | 1,340,7  | 714   | 35.3  | 90   | 8269  |   |
|          | Lynchburg A<br>Nortolk A<br>Richmond A<br>Roanoke A  | 46 0<br>49 2<br>47 3<br>46 1   | 0000                                    | 0                                       | 0<br>51<br>0<br>36<br>51                | 223°<br>136<br>214<br>229  | 360<br>540<br>, 408<br>495<br>549  | 645<br>822<br>698<br>784<br>825  | 694<br>849<br>38<br>815<br>834  | 633<br>131<br>655<br>703<br>722   | 533<br>116<br>614  | 246<br>267<br>216<br>219<br>261   | 53<br>*8<br>37<br>53                                | 0000   | 3279<br>4166<br>3421<br>3865<br>4150  |   |
| Wash     | Olympia A Seattle Tacoma Seattle C Spokane A Walla Walla C Yakima A  | 44 2<br>44 2<br>46 9<br>36 5<br>43 8<br>39 1   | 68<br>56<br>50<br>9<br>0<br>Q           | , 1°<br>62<br>47<br>25<br>0             | 198<br>162<br>129<br>168<br>87<br>144   | 422<br>391<br>329<br>493<br>310<br>450   | 636<br>633<br>543<br>879<br>681<br>828   | 753<br>*50<br>657<br>*082<br>813<br>1039   | 834<br>828<br>738<br>1231<br>986<br>1163  | 676<br>678<br>599<br>980<br>745<br>868  | 645<br>65*<br>577<br>834<br>589  | 450<br>474<br>396<br>531<br>342<br>435  | 30"<br>242<br>288<br>1""                            | 159<br>159<br>117<br>135<br>45                 | 5236<br>5145<br>4424<br>6655<br>4805  |   |
| Ì        | Charleston A Elkins A Huntington A Parkersburg C   | 44 8<br>40 1<br>45 0<br>43 5   | 0 ,                                     | 0<br>25<br>0                            | 63<br>135<br>63<br>60                   | 254<br>400<br>251<br>164   | 591<br>129<br>585<br>606   | 865<br>992<br>856<br>905   | 880<br>1008<br>880<br>942   | 770<br>896<br>764<br>826  | 648<br>791<br>648<br>649   | 300<br>411<br>244<br>300  | 46<br>198<br>99                                     | 69<br>48<br>12t<br>12t                         | 5941<br>1476<br>5671<br>4446<br>4734  |   |
|          | Green Bay A<br>La Crosse A<br>Madison A<br>Milwaukee A   | 30 3<br>31 5<br>30 9<br>32 6   | 28<br>12<br>25<br>43                    | 50<br>19<br>40<br>47                    | 174<br>153<br>1 1<br>174                | 484<br>437<br>174<br>171   | 924<br>921<br>930<br>976   | 1333<br>1339<br>1330<br>1252   | 1494<br>1504<br>1473<br>1476  | 1313<br>12<br>1274<br>1194  | 1111<br>10 0<br>1113<br>1051   | 534<br>534<br>518<br>517  | 335<br>245<br>310                                   | 144<br>64<br>102                               | 8029<br>1589<br>1863<br>635   |   |
|          | Gasper A<br>Cheyenne A<br>Lander A<br>Sheridan A   | 33 4<br>34 2<br>31 4<br>32 5   | 6<br>28<br>6<br>25                      | 16<br>3"<br>19<br>31                    | 192<br>219<br>204<br>219                | ,14<br>549<br>555<br>539   | 912<br>909<br>1020<br>948  | 1163<br>1085<br>1299<br>1290   | 1290<br>1212<br>1417<br>1311  | 1084<br>1042<br>111<br>111  | 1 1 27<br>272 pc<br>21 1 7<br>311 14                                     | n ,<br>1114<br>114  | 481<br>158<br>181                                   | 129  | 7410<br>7351<br>Я.<br>76н   |   |

## AVERAGE MONTHLY AND YEARLY DEGREE DAYS, CONTINUED

|       |                                  |                       |          |          |              | C          | ANADA      | <u> </u> |              |        |              |              |            |          |                 |
|-------|----------------------------------|-----------------------|----------|----------|--------------|------------|------------|----------|--------------|--------|--------------|--------------|------------|----------|-----------------|
| Prov  | Station                          | Avg<br>Winter<br>Temp | July     | Aug      | Sept         | Oct        | Nov        | Dec      | Jan          | Feb    | Mar          | Apr          | May        | June     | Yearly<br>Total |
| Alta  | Banff (                          |                       | 220      | 295      | 498          | 797        | 1185       | 1485     | 1624         | 1364   | 1237         | 855          | 589        | 402      | 10551           |
|       | Calgar,                          | Al I                  | 109      | 186      | 402          | 719        | 1110       | 1389     | 1575         | 1379   | 1268         | 798          | 477        | 291      | 9703            |
|       |                                  | <b>4</b> ]            | 74       | 1801     | 411          | 738        | 1215       | 1603     | 1810         | 1520   | 1330         | 765          | 400        | 222      | 10268           |
|       | Fethbridge •                     | <b>`</b>              | 56       | 11,2     | 318          | 611        | 1011       | 1277     | 1497         | 1291   | 1159         | 696          | 403        | 213.     | . 8644          |
| вс    |                                  | • [                   | 22       | 40       | 189          | 546        | 894        | 1138     | 1314         | 1057   | 818          | 462          | 217        | 102      | 8799            |
|       |                                  | <b>^</b>              | 236      | 251      | 444          | 747        | 1110       | 1420     | 1612         | 1319   | 1122 .       | 747          | 468        | 279      | 9755            |
|       | Frequition (4                    |                       | إيرو     | 246      | 339          | 539        | 708        | 868      | 936          | 808    | 812          | 648          | 493        | 357      | 7029            |
|       |                                  | •                     | 81       | 87       | 219          | 456        | 657        | 787      | 862          | 723    | 876          | 501          | 310        | 156      | 5515            |
| •     |                                  | •                     | 1.36     | 140      | 225          | 462        | 663        | 775      | 840          | 718    | 891          | 504          | 341        | 204      | 5699            |
|       | : Victoria (                     |                       | 172      | 184      | - 243        | 426        | 607        | 723      | 805          | 668    | 660          | 487          | 354        | 250      | 5578            |
| Man   |                                  | <b>.</b>              | 4.       | 90       | 357          | 747        | 1290       | 1792     | 2034         | 1737   | 1478         | 837          | 431        | 188      | 11036           |
|       |                                  | N 1   1               | 360      | 375      | 651          | 1082       | 1620       | 2248     | 2558         | 2277   | 2130         | 1568         | 1153       | 675      | 18728           |
|       | The Pas (                        |                       | 59       | 127      | 429          | 831        | 1440       | 1981     | 2232         | 1853   | 1624         | 969          | 500        | 228      | 12281           |
|       | Winnipeg                         | <b>`</b>              | 38       | 71       | 322          | , 683      | 1251       | 1757     | 2008         | 1719   | 1465         | 813          | 404        | 147      | 10679           |
| N B   |                                  |                       | 78       | 68       | 234          | 592        | 915        | 1392     | 1541         | 1379   | 1172         | 753          | 406        | 141      | 8671            |
|       | Moneton (                        |                       | 62       | 105      | 276 ~        | 611        | 891        | 1342     | 1482         | 1336   | 1194         | 789          | 468        | 171      | 8727            |
| •     | St John (                        | -                     | 109      | 102      | 246          | 527        | 807        | 1194     | 1370         | 1229   | 1097         | 756          | 490        | 248      | 8218            |
| Nod   |                                  | • 1 1                 | 260      | 187      | 294          | 564        | 750        | 1001     | 1159         | 1085   | 1091         | 878          | 707        | 483      | 8440            |
|       | Corner Brook (                   | :                     | 102 4    | 133      | 324          | 642        | 873        | 1194     | 1358         | 1283   | 1212         | 885          | 639        | 333      | 8978            |
|       |                                  | <b>4</b>              | 121      | 152      | 330          | 670        | 909        | 1231     | 1370         | 1266 - | J243         | 838          | 657        | 366      | 8254            |
|       |                                  | <b>* 1</b>            | 130      | 205      | 444          | 843        | 1227       | 1745     | 1947         | 1688   | 1494         | 1074         | 341        | 348      | 11887           |
|       | St Johns                         | <b>`</b>   <u></u> ;  | 186      | 180      | 342          | 651        | 831        | 1113     | 1262         | 1170   | 1187         | 827          | 710        | 432      | 8991            |
| NWT   |                                  | AVAILABLE             | 273      | 459      | <b>,8</b> 07 | 1414       | 2064       | 2530     | 2632         | 2336   | 2282         | 1674         | 1063       | 483      | 18017           |
|       | Fort Norman (                    | `  3                  | 164      | 341      | 666          | 1234       | 1959       | 2474     | 2592         | 2209   | 2058         | 1386         | 732        | 294      | 16109           |
|       | Restitution Island (             | :   ₹                 | 843      | 831      | 900          | 1113       | 1311       | 1724     | 2021         | 1850   | 1817         | 1488         | 1181       | 942      | 16021           |
| N S   | Halifax (                        | :•   ≛                | 58       | 51       | 180          | 457        | 710        | 1074     | 1213         | 1122   | 1030         | 742          | 487        | 237      | 7361            |
|       | Sydney                           | Ş                     | 62       | 71       | 219          | 518        | 765        | 1113     | 1262         | 1206   | 1150         |              | 567        | 276      | 8048            |
|       | Yarmouth /                       | ·   Z                 | 102      | 115      | 225          | 471        | 696        | 1029     | 1156         | 1065   | 1004         | 726          | 493        | 258      | 7340            |
| Ont   | Couhrane (                       | :     .               | 96       | 180      | 405          | 760        | 1233       | 1778     | 1978         | 1701   | 1528         | 963          | 570        | 222      | 11412           |
| -     | Fort William ,                   | <b>4</b>     "        | 90       | 133      | 366          | 694        | 1140       | 1597     | 1792         | 1557   | 1380         | 876          | 543        | 237      | 10405           |
|       |                                  |                       | 74       | 171      | 405          | 756        | 1245       | 1807     | 2037         | 1735   | 1562         | 878          | 580        | 222      | 11572           |
|       |                                  |                       | 16       | 59       | 177          | 505        | 855        | 1234     | 1342         | 1226   | 1101         | 663          | 322        | 66       | 7586            |
|       |                                  | • I                   | 12       | 43       | 159          | 477        | 837        | 1206     | 1305         | 1198   | 1066         | 648          | 332        | 66       | 7348            |
|       | North Bay (                      |                       | 37       | 90       | 267          | 600        | 990        | 1507     | 1680         | 1463   | 1277         | 780<br>708   | 400<br>341 | 120      | 9218<br>8735    |
|       | Ortawa (<br>Toronto (            |                       | 25       | 18       | 22 <b>2</b>  | 567<br>439 | 936<br>760 | 1449     | 1624         | 1441   | 1013         | 618          | 296        | 90<br>82 | 6827            |
|       |                                  | '                     | 1 '      | 1        |              | 1          | 1          |          |              | -      |              | -            | 1,         |          | _               |
| PEI   | L harloffetowr (<br>Summerside ( |                       | 40<br>47 | 53<br>84 | 198<br>216   | 518<br>546 | 804<br>840 | 1215     | 1380         | 1274   | 1169<br>1206 | 813<br>841   | 496<br>518 | 204      | 8164<br>8488    |
|       | Summerside (                     |                       | *,       | ,        | 210          | 340        | 040        | 1240     | 1430         | 1291   | 1200         |              | 3.5        | 1 * "    |                 |
| (Jue  |                                  | .                     | 102      | 136      | 327          | 682        | 1074       | 1859     | 1879         | 1818   | 1407         | 891          | 521        | 231      | 10528           |
|       |                                  | <u> </u>              | 9        | 43<br>28 | 165          | 521<br>496 | 882        | 1392     | 1566<br>1510 | 1381   | 1175<br>1138 | - 684<br>857 | 316<br>288 | 69<br>54 | 8203<br>7899    |
|       |                                  |                       | 16<br>56 | 84       | 165<br>273   | 636        | 864<br>996 | 1516     | 1665         | 1477   | 1296         | 818          | 428        | 126      | 8372            |
|       | Queber (                         |                       | 40       | 68       | 243          | 592        | 972        | 1473     | 1612         | 1418   | 1228         | 780          | 400        | 111      | 8937            |
| Casta | Prince Albert                    |                       | 81       | 136      | 414          | 797        | 1368       | 1872     | 2108         | 1763   | 1559         | 867          | 446        | 219      | 11630           |
| Sasks |                                  |                       | 78       | 93       | 360          | 741        | 1284       | 1711     | 1965         | 1687   | 1473         | 804          | 409        | 201      | 10806           |
|       | Saskatoon (                      |                       | 56       | 87       | 372          | 750        | 1302       | 1758     | 2006         | 1689   | 1463         | 798          | 403        | 186      | 10870           |
| ΥĪ    |                                  | .     '               | 164      | 326      | 645          | 1197       | 1875       | 2415     | 2561         | 2150   | 1838         | 1006         | 570        | 258      | 15067           |
| ¥ 1   |                                  | : 1                   | 208      | 366      | 648          | 1135       | 1794       | 2325     | 2427         | 1992   | 1665         | 1020         | 590        | 294      | 14454           |
|       | Mayo Landing (                   | -   <b>T</b>          | 200      | 300      | 040          | 11133      | 1 / 3-4    | 12323    | 272          | 1792   | 1003         | 1,020        | 1 350      | 1        | 1,773           |

The data to these normals were from the full ten year period 1951, 1960 and steet to the standard resimal period 1931, 1960.

# INSOLATION AND PERCENT DIFFUSE TABLES BTU per sq. ft. per day/% DIFFUSE

| <del></del>             | _           |                  | _                 |                    | <del></del> |                    | T ~-               | -                   |                                     |                            |                                    |                            |                  |
|-------------------------|-------------|------------------|-------------------|--------------------|-------------|--------------------|--------------------|---------------------|-------------------------------------|----------------------------|------------------------------------|----------------------------|------------------|
| City                    | Lat         | Jen              | Feb               | Mar                | Apr         | Mey                | Junes              | July                | Aug                                 | Sept                       | Oct                                | Nov                        | Dec              |
| ALABAMA                 | +           | ╂─╌              | 1                 | -                  | ┼           | +                  | <del> `</del>      | <del> </del>        | <del> </del>                        | -                          | <del> </del>                       | <del></del>                | ┼                |
| Birmingham              | 36.6        | 706/53           | 967/48            | 1295/45            | 1672/40     | 1855/40            | 1917/40            | 1809/42             | 1722/40                             | 1454/41                    | 1210/39                            | 868/46                     | 661/5            |
| Mobile                  | 30.7*       | 820/40           | 1099/45           | 1406/41            | 1721/39     | 1871/38            | 1867/41            | 1714/45             | 1640/44                             | 1449/44                    | 1298/38                            | 955/44                     | 759/4            |
| Montgomery<br>ALASKA    | <b>353.</b> | 751/51           | 1013/47           | 1339/44            | 1728/39     | 1896/38            | 1971/38            | 1839/41             | 1744/40                             | 1467/42                    | 1261/38                            | 915/44                     | 719/4            |
| Annetta                 | 88.0        | 232/60           | 424/53            | 870/42             | 1342/41     | 1811/45            | 1815/48            |                     | . 25 7 50                           |                            |                                    |                            |                  |
| Bethel                  | 60.8        | 136/41           | 413/33            | 1040/18            | 1640/22     | 1682/40            | 1655/48            | 1615/47.            | 1257/ <b>5</b> 0<br>936/ <b>6</b> 0 | 951/47<br>734/53           | 450/68                             | 217/62                     | 151/5            |
| Fairbanks               | 648.        | 70/23            | 280/36            | 859/20             | 1419/20     | 1758/36            | 1943/39            | 1637/45             | 1338/41                             | 678/S1                     | 431/48<br>317/48                   | 100/48                     | 85/4-<br>22/3    |
| Matanuska -             | 91.8*       | 118/42           | 339/42            | 802/28             | 1312/37     | 1607/42            | 1703/48            | 1508/48             | 1158/50                             | 730/53                     | 369/51                             | 140/51                     | 55/5             |
| ARIZONA                 |             |                  |                   | _                  | 1           |                    |                    |                     |                                     | 1.000                      |                                    | 1                          |                  |
| Page                    | 38.8*       | 1106/18          | 1408/18           | 1939/13            | 2278/18     | 2562/18            | 2606/18            | 2507/20             | 2197/23                             | 1902/21                    | .1482/21                           | 1143/20                    | 896/2            |
| Phoenix                 | 33.4*       | 1020/31          | 1374/27           | 1813/22            | 2353/15     | 2674/13            | 2738/14            | 2485/21             | 2291/21                             | 2014/20                    | 1575/21                            | 1150/27                    | 032/3            |
| Tucson                  | 321         | 1098/29          | 1431/25           | 1776/23            | 2274/18     | 2628/15<br>2670/13 | 2761/14            | 2308/27             | 2090/28                             | 1955/21                    | 1542/21                            | 1139/24                    | 926/30           |
| Winslow                 | 38.0        | 984/30           | 1326/27           | 1779/22            | 2282/10     | 2593/18            | 2728/14<br>2709/15 | 2340/25             | 2181/25<br>2139/25                  | 1978/22                    | 1601/22                            | 1207/25                    | 995/3<br>894/3   |
| Yuma                    | 32.7*       | 1095/20          | 1442/24           | 1010/10            | 2411/14     | 2726/12            | 2012/12            | 2451/22             | 2327/20                             | 2050/18                    | 1622/20                            | 1214/24                    | 999/2            |
| ARKANSAS                |             | 1 .              |                   |                    |             | ,                  |                    | 1 40                | 2027.20                             | 203011                     | 102220                             | 121424                     | ****             |
| Fort Smith              | 36.3        | 743/47           | 998/45            | 1311/42            | .1615/41    | 1811/38,           | 2088/34            | 2084/34             | 1879/34                             | 1504/39                    | 1200/38                            | 851/42                     | 682/47           |
| Little Rock             | 34.7*       | 731/40           | 1002/45           | 1312/42            | 1610/42     | 1928/36            | 2105/34            | 2031/36             | 1860/36                             | 1517/38                    | 1228/37                            | 847/44                     | 073/4            |
| CALIFORNIA              |             |                  |                   |                    |             |                    |                    | 1                   | İ                                   |                            |                                    | 1                          |                  |
| Arcata<br>Bakarsfield   | 41.0°       | 528/53<br>766/45 | 793/48<br>1101/38 | 1132/48<br>1594/30 | 1586/40     | 1841/40            | 1980/38            | 1807/42             | 1578/44                             | 1341/41                    | 935/45                             | 593/51                     | 460/54           |
| Daggett                 | 34.9        | 957/32           | 1279/29           | 1772/23            | 2093/24     | 2508/18<br>2590/18 | 2748/14            | 2681/14             | 2419/18                             | 1991/18                    | 1457/24                            | 841/37                     | 977/47           |
| Davis                   | 38.5        | 583/63           | 944/42            | 1482/31            | 1947/28     | 2345/23            | 2588/21            | 2602/18<br>2544/18  | 2381/18 2252/21                     | 2007/18                    | 1515/22                            | 1084/28                    | 075/31           |
| El Toro                 | 33.7        | 947/36           | 1235/33           | 1609/31            | 1928/31     | 2068/33            | 2193/31            | 2344/18             | 2154/25                             | 1836/22<br>1736/30         | 1283/28                            | 796/63                     | 548/61           |
| Fresno                  | 36.8*       | 645/61           | 999/42            | 1524/31            | 1965/28     | 2308/25            | 2529/21            | 2524/20             | 2274/21                             | 1871/22                    | 1356/32                            | 1026/34                    | 969/37<br>549/56 |
| Inyokern                | 36.8        | 1150/18          | 1545/13           | 2131/6             | 2584/6      | 2903/6             | 3062/4             | 2890/6              | 2721/8                              | 2389/2                     | 1784/6                             | 1349/8                     | 1087/1           |
| Long Beach              | 33.8        | 927/37           | 1214/34           | 1609/31            | 1936/30     | 2063/33            | 2139/33            | 2200/27             | 2096/26                             | 1099/31                    | 1325/33                            | 1003/36                    | 848/36           |
| Los Angeles             | 23.9        | 925/97           | 1213/34           | 1618/30            | 1950/30     | 2058/33            | 2118/33            | 2306/27             | 2078/28                             | 1680/32                    | 1316/33                            | 1003/36                    | 848/3            |
| Mt Shaata               | 41.3*       | 500/40           | 857/44            | 1250/40            | 1755/33     | 2185/29            | 2435/24            | 2576/18             | 2212/21                             | 1734/24                    | 1154/31                            | 650/46                     | 505/40           |
| Needles<br>Oakland      | 34.8*       | 984/30<br>707/48 | 1353/25           | 1824/20            | 2316/10     | 2650/14            | 2790/13            | 2540/18             | 2276/21                             | 2013/18                    | 1537/21                            | 1123/25                    | * 813/30         |
| Pasadena                | 34.1*       | 825/36           | 1017/40           | 1456/33<br>1018/29 | 1921/29     | 2210/28<br>2097/32 | 2348/27            | 2321/27             | 2052/28                             | 1700/29                    | 1211/33                            | 822/46                     | 646/4            |
| Point Mugu              | 34.1        | 926/34           | 1220/33           | 1634/29            | 1976/32     | 2016/34            | 2138/33            | 2337/25             | 2208/23                             | 1777/28                    | 1349/31                            | 900/34                     | 870/30           |
| Riverside               | 23.9.       | 1014/30          | 1353/27           | 1762/24            | 1994/29     | 2297/25            | 2053/36<br>2507/22 | 2117/32             | 1934/33                             | 1807/36                    | 1295/34                            | 1005/34                    | 856/37           |
| Sacramento              | 38.5        | 506/63           | 939/44            | 1457/33            | 2002/25     | 2433/21            | 2682/18            | 2481/21<br>-2687/14 | 2278/21<br>2367/18                  | 1972/21                    | 1500/24                            | 1176/24<br>781/41          | 995/27<br>538/6  |
| San Diego               | 32.7*       | 975/36           | 1265/33           | 1831/81            | 1835/31     | 2001/36            | 2061/36            | 2185/30             | 2056/20                             | 1718/32                    | 1373/32                            | 1082/33                    | 903/36           |
| San Francisco           | 37.8*       | 707/45           | 1008/40           | 1454/33            | 1919/29     | 2224/28            | 2375/27            | 2390/24             | 2115/25                             | 1741/27                    | 1225/33                            | 821/40                     | 642/44           |
| San Jose                | 37.3°       | 663/48           | 980/42            | 1301/41            | 1787/34     | 2115/31            | 2207/31            | 2247/20             | 1979/31                             | 1001/20                    | 1149/38                            | 956/46                     | 630/47           |
| Sente Marie             | 34.9        | 853/40           | 1140/37           | 1581/32            | 1920/32     | 2139/32            | 2347/27            | 2340/25~            | 2105/27                             | 1729/30                    | 1353/30                            | 973/36                     | 803/24           |
| Sunnyvala<br>COLORADO   | 37.4°       | 737/44           | 1036/30           | 1485/32            | 1943/29     | 2275/ <b>27</b>    | 2451/24            | 2440/22             | 2165/24                             | 1758/27                    | 1248/32                            | 843/30                     | 660/48           |
| Boulder                 | 40.0        | 741/37           | 988/38            | 1478/30            | 1006/37     | 1006/46            | 1935/40            |                     |                                     |                            |                                    |                            |                  |
| Colo Springs            | 38.8        | 890/28           | 1177/28           | - 1549/28*         | 1930/27     | 2127/31            | 2367/27            | 1917/30<br>2210/30  | 1818/42<br>2024/29                  | 151 <b>9/34</b><br>1758/26 | 1143/34<br>1358/24                 | 918/36<br>944/39           | 871/37           |
| Denver                  | 36.7*       | 840/33           | 1127/30           | 1530/29            | 1879/20     | 2134/30            | 2350/27            | 2272/27             | 2044/28                             | 1726/26                    | 1300/25                            | 683/30                     | 781/30<br>731/32 |
| Eagla                   | 30.6*       | 754/37           | 1077/32           | 1500/30            | 1931/28     | 2254/27            | 2507/22            | 2385/24             | 2083/27                             | 1706/24                    | 1307/25                            | 868/32                     | 000/36           |
| Grand Junction          | 36.1"       | 791/34           | 1118/31           | 1552/28            | 1985/27     | 2378/22            | <b>@587/20</b>     | 2464/22             | 2180/23                             | 1833/22                    | 1344/24                            | 918/30                     | 731/32           |
| Grand Lake              | 40.3*       | 782/32           | 1154/27           | 1559/25            | 1869/26     | 2035/33            | 2330/28            | 2212/28             | 1862/30                             | 1755/24                    | 1331/23                            | 863/31                     | 878/36           |
| Púeblo                  | 36.3*       | 894/29           | 1171/30           | 1563/26            | 1955/28     | 2161/30            | 2433/24            | 2310/27             | 2101/27                             | 1778/24                    | 1360/24                            | 953/20                     | 782/31           |
| CONNECTICUT<br>Hartford | 419*        | 477/66           |                   | A-0.00             |             |                    |                    |                     |                                     |                            |                                    |                            |                  |
| DELAWARE                | 419         | *///             | 714/53            | 978/53             | 1314/60     | 1567/48            | 1685/48            | 1648/47             | 1420/48                             | 1154/49                    | 852/48                             | 487/58                     | 384/90           |
| Wilmington              | 36.7*       | 371/51           | 827/48            | 1148/48            | 1479/45     | 1709/45            | 1362/41            | 1622/42             | 1813/42                             | 4347/44                    |                                    |                            | 400              |
| DC                      | 1           | "•               |                   |                    |             | 1.0240             | ,                  | 1445/44             | 1013/42                             | 1317/44                    | 984/44                             | 644/60                     | 480/54           |
| Washington              | 38.6*       | 571/54           | 815/50            | 1124/48            | 1458/48     | 1717/44            | 1899/41            | 1817/42             | 1617/44                             | 1340(44                    | 1003/44                            | 851/50                     | 481/67           |
| FLORIDA                 |             |                  |                   |                    |             |                    |                    |                     |                                     |                            |                                    |                            |                  |
| Apalachicola            | 20.7*       | 852/48           | 1125/45           | 1473/40            | 1877/34     | 2090/32            | 1907/37            | 1812/42             | 1686/42                             | 1534/40                    | 1370/36                            | 1039/40                    | 817/47           |
| Daytona Beach           | 20.2        | 958/42           | 1213/40           | 1547/37            | 1863/34     | 1966/38            | 1825/42            | 1783/42             | 1681/42                             | 1477/44                    | 1250/42                            | 1035/41                    | 870/46           |
| Gainesville 📏           | 20.0        | 1025/38          | 1353/33           | 1640/33            | 1987/30     | 2160/30            | 2006/37            | 1917/30             | 1873/38                             | 1637/37                    | 1357/37                            | 1172/32                    | 936/40           |
| Jacksonvilla            | 30.4        | 890/45           | 1162/41           | 1521/37            | 1854/34     | 1955/37            | 1884/41            | 1801/42             | 1003/42                             | 1441/44                    | 1222/42                            | 995/41                     | 817/48           |
| Miami                   | 35.         | 1067/42          | 1313/30           | 1603/37            | 1858/36     | 1642/40            | 1707/48            | 1762/44             | 1629/45                             | 1456/48                    | 1301/42                            | 1117/41                    | 1019/41          |
| Orlando<br>Pensecola    | 30%         | 999/41<br>922/44 | 1242/40           | 1581/36            | 1897/33     | 1967/36<br>2072/33 | 1830/42<br>2094/34 | 1800/42             | 1872/44                             | 1495/42                    | 1303/40                            | 1095/98                    | 925/42           |
| Tallahaasee             | 30.4        | 076/46           | 1136/42           | 1478/30            | 1828/36     | 1935/38            | 1882/41            | 1079/37             | 1876/36                             | 1585/38                    | 1452/31                            | 1025/40                    | 820/40           |
| Tampa -                 | 20.         | 1010/41          | 1258/40           | 1593/36            | 1907/32     | 1997/36            | 1847/41            | 1747/44<br>1751/44  | 1874/42<br>1852/44                  | 1492/42                    | 1317/ <b>36</b><br>134 <b>5/36</b> | 1007/41<br>1107/ <b>36</b> | 813/47<br>835/42 |
| EORGIA                  | 1           |                  |                   |                    |             | •                  |                    |                     |                                     | . 40 :/44                  |                                    | . 107/30                   | <b>5</b> 53742   |
| Atlanta                 | 30.6*,      | 717/61           | 909/48            | 1302/44            | 1665/36     | 1853/40            | 1911/40            | 1811/42             | 1707/41                             | 1421/42                    | 1199/40                            | 882/44                     | 874/50           |
| Augusta                 | 38.4        | 750/49           | 1014/48           | 1338/42            | 1728/36     | 1864/40            | 1903/40            | 1803/42             | 1806/42                             | 1409/44                    | 1219/00                            | 010/41                     | 720/4            |
| Griffin                 | 39.2        | 877/41           | 1113/40           | 1430/30            | 1913/31     | 2127/31            | 2130/33            | 2061/84             | 1929/33                             | 1811/36                    | 1372/31                            | 1062/32                    | 77444            |
| Macon                   | 27.         | 700/48           | 1019/46           | 1362/42            | 1734/38     | 1864/36            | 1918/40            | 1784/44             | 1716/41                             | 1438/42                    | 1246/30                            | 939/41                     | 728/48           |
| Savannah                | 22.1"       | 907/41           | 1158/40           | 1486/38            | 1906/32     | 2075/33            | 2042/36            | 1876/37             | 1847/37                             | 1486/41                    | 1283/36                            | 877/40                     | 780/45           |
| HAWAN                   |             | 1120/40          | 1246/40           |                    |             |                    |                    |                     |                                     |                            |                                    |                            |                  |
| Hilo ,<br>Honolulu      | 18.7        | 1180/40          | 1246/40           | 1348/40<br>1621/36 | 1434/40     | 1553/40            | 1658/48            | 1624/45             | 1582/48                             | 1546/40                    | 1372/40                            | 1104/40                    | 1019/4           |
| DANO                    | 51.3.       | 7                | 1.500.35          | 104 1190           | 1796/36     | 1949/30            | 2004/30            | 2002/98             | 1906/30                             | 1810/30                    | 1540/30                            | 1796/36                    | 1132/36          |
| Boise                   | 444         | 485/51           | 839/41            | 1302/34            | 1825/30     | 2275/25            | 2461/23            | -2611/18            | 2195/21                             | 1736/21                    | 1137/29                            | 628/44                     | 49-0-            |
| Pocatello               | 40.         | 539/48           | 001/36            | 1370/32            | 1819/30     | 2279/25            | 2478/23            | 2506/18             | 2238/20                             | 1766/21                    | 1202/25                            | 620/30                     | 437/61           |
| Twin Falls              | 44.         | 801/48           | 865/44            | 1309/38            | 1703/36     | 2035/33            | 2183/32            | 2219/20             | 1901/20                             | 1503/31                    | 1054/30                            | 949/48                     | 483/64           |
| LLINOIS                 |             |                  |                   |                    | •           |                    | ĺ                  |                     |                                     |                            |                                    |                            |                  |
| Chicago                 | 40.         | 506/63           | 750/40            | 1106/46            | 1456/45     | 1769/41            | 2006/38            | 1942/38             | 1718/38                             | 1353/40                    | 909/41                             | 565/61                     | 402/68           |
| Lemont                  | 41.7*       | × 630/42 i       | 855/44            | 1202/41            | 1438/48     | 183240             | 2030/37            | 1943/38             | 1792/38                             | 1416/36                    | 077/41                             | 579/61                     | 483/60           |

<sup>1</sup> Source Data From Klein Beckman and Duffe - Month'y Average Solar Radiation on Inclined Surfaces E. Report #42.2 - University of Wisconsin Revised 197



# INSOLATION AND PERCENT OFFUSE TABLES, CONTINUED BTU per sq. ft. per day /% DIFFUSE

| ity                        | Lat            | Jen                | Feb                | Mer                | Aèr                | May                | June                | July               | Aug                | Bapt.              | Out.               | Nev.                     |                                   |
|----------------------------|----------------|--------------------|--------------------|--------------------|--------------------|--------------------|---------------------|--------------------|--------------------|--------------------|--------------------|--------------------------|-----------------------------------|
| Moking                     | 41.4*          | 514/51             | 812 47             | 1117:48            | 1458-45            | 1752/42            | 1968/30             | 1937/38            | 1714/39            | 1356/40            | 995/40             | 594/60                   | 432/68                            |
| Penna                      | 40 7*          | 601.47             | 840/46             | 1187/44            |                    | 1876-39            | 2112/34             | 2075/33            | 1851/34            | 1500/34            | 1102/36            | 682/45                   | 512/60                            |
| Springheld                 | 30.4           | 585/50             | 860/46             | 1133/48            |                    | 1864/30            | 2096/34             | 2057/34            | 1804/36            | 1453/38            | 1067/38            | 878/47                   | 490/54                            |
| INDIANA                    |                |                    |                    |                    | i                  | 1                  |                     |                    |                    |                    |                    | ,                        |                                   |
| Evansviile                 | 38.0           | 573.55             | 822/50             | 1150/47            | 1500/46            |                    | 1981/38             | 1919/30            | 1734/30            | 1403/41            | 1087/40            | 682/50                   | 498/67                            |
| Fort Wayne<br>ndianapolis  | 41.0°<br>30.7° | 455/58<br>495/58   | 697/56<br>747/54   | 981 53             |                    |                    | 1840/42             | 1786/44            | 1593/44            | 1272/45            | 924/46             | 516/68                   | 369/64                            |
| Soi th Rend                | 41 7*          | 416/62             |                    | 1036/51<br>992/51  | 1397/48<br>1387/47 |                    | 1986/42             | 1805/42            |                    | 1323/44            | 977/45             | 579/88                   | 417/62                            |
| IOWA .                     | -,,            |                    | , 000,50           | 17231              | 130/14/            | 17 2 1744          | 1921/40             | 1851/41            | 1003/40            | 1290/44            | 909/48             | 497/58                   | 340/66                            |
| <b>A</b> 173 <b>4</b> 4    | 420°           | 642'40             | 933/30             | 1205/41            | 1486/44            | 1770/42            | 1994/38             | 1976/37            | 1696/38            | 1353/40            | 1010/36            | 689/41                   | 527/48                            |
| ,DesMines                  | 415"           | 580/47             | 860/44             | 1180/42            | 1556/41            | 1866/39            | 2123/34             | 2096/33            | 1826/34            | 1433/37            | 1067/37            | 853/45                   | 487/50                            |
| Mason City                 | 431*           | 553/48             | 636/42             | 1167/41            | 1517/41            | 1894/38            | 2112/34             | 2083/33            | 1832/33            | 1404/37            | 1010/37            | 600/47                   | 443/51                            |
| KANSAS                     | 42 4"          | 5n8/47             | 841 44             | 1169/42            | 1577/40            | 1900/38            | 2122/34             | 2120/32            | 1844/33            | 1420/87            | 1037/37            | 642/45                   | 469/50                            |
| f Dodge City               | 37.8           | 826/38             | 1121/33            | 147400             |                    | 2000.00            | ******              | 000.00             |                    |                    |                    |                          |                                   |
| Manhattan                  | 30.21          | 708/41             | 973/40             | 1476/32            | 1884/31            | 2069/32            | 2356/27             | 2294/27<br>1957/38 | 1939/31            | 1685/29            | 1300/28<br>1077/38 | 893/34                   | 732/38                            |
| Topaka                     | 30 1           | 681/46             | 940/42             | 1256/41            | 1640/38            | 1914/38            | 2125/34             | 2127/32            |                    | 1512/36<br>1515/36 | 1148/38            | 837/ <b>36</b><br>771/41 | 575/48<br>583/47                  |
| Wighita                    | 37 6*          | 783/40             | 1058/40            | 1405/35            | 1782/30            | 2035/35            | 2264/30             | 2239/26            |                    | 1616/30            | 1249/30            | 870/35                   | 690/46                            |
| KENTUCKY                   | '              |                    |                    | 1                  |                    | 1                  | - 127               |                    | 1                  | 1                  |                    |                          | 1                                 |
| Covington                  | 30 1°          | 372/69             | 512/68             | 1036/51            | 1486/45            | 1873/30            | 2142/33             | 2470/21            | 2016/29            | 1471/37            | 866/51             | 516/90                   | 200/73                            |
| Lexington - 3              |                | 545/57             | 779/84             | 1099/46            | 1478/48            | 1746/44            | 1896/41             | 1849/41            | 1685/41            | 1361/42            | 1043/42            | 657/61                   | 485/68                            |
| Louisville                 | 38.2           | 545/57             | 789/63             | 1102/46            | 1400/48            | 1719/44            | 1902/41             | 1836/41            | 1679/41            | 1360/42            | 1042/42            | 652/51                   | 488/67                            |
| " LOUISIANA<br>Baton Rouge | 30 5           | 704.4.             | 1063.45            | 1270.44            | 1480.4-            |                    | 1000-00             |                    |                    | ·                  |                    |                          |                                   |
| Lake Charles               | 30.2           | 785/51<br>728/55   | 1053/47<br>1009/48 | 1378/44            | 1680/41            | 1870/30            | 1925/30             | 1744/45            | 1678/42            | 1463/42            | 11301/38           | 619/46                   | 736/61                            |
| New Orleans                | 30.0           | 834'46             | 1111/46            | 1414/42            | 1779/38            | 1848/40            | 1989/38<br>2002/37  |                    | 1656/44            | 1484/42            | 1380/34            | 916/47                   | 705/ <b>54</b><br>77 <b>9/48</b>  |
| Shreveport                 | 32 4           | 833/46             |                    | 1394/41            | 1721/30            | 2020/34            |                     | 2072/33            | 1917/34            | 1530/30            | 1312/36            | 896/45                   | 730/48                            |
| MAINE                      |                |                    |                    |                    |                    | ,                  |                     |                    | 1                  |                    |                    |                          | , JUI 48                          |
| Caribou                    | 48 6"          | 425/80             | 726/44             | 1132/39            | 1407/44            | 1565/46            | 1749/46             | 1749/44            | 1486/45            | 1093/46            | 682/53             | 368/62                   | 318/57                            |
| Portland                   | 43 6 '         | 450/55             | 662/53             | 969/51             | 1303/46            | 1567/46            | 1710/47             | 1658/47            | 1460/47            | 1157/47            |                    | 459/58                   | 363/50                            |
| MARYLAND                   |                |                    |                    |                    | t                  |                    |                     |                    | ,                  |                    | i                  |                          |                                   |
| Annapolis                  | 39 0*          | 645/47             | 896/45             | 1254/41            |                    | 1799/41            | 2053/37             | 1996/32            | 1729/30            | 1411/40            |                    | 897/47                   | 571/48                            |
| Baitimore<br>Silver Hill   | 30.2           | 506/51             | 839/46             | 1161/48            |                    | 1713/45            | 1878/41             | 1822/42            | 1598/44            | 1330/44            | 987/44             | 800/46                   | 499/55                            |
| MASSACHUSETTS              | 281.           | 671/44             | 900/45             | 1253/42            | 1615/40            | 1091/38            | 2046/37             | 1902/36            | 1692/40            | , 1463/ <b>38</b>  | 1087/39            | 745/44                   | 600/46                            |
| Amnerst                    | 42.2*          | 428/90             | 852/68             | 1106/48            | 1279/51            | 1580/48            | 1895/41             | 1902/30            | 1622/41            | 1217/48            | 822/44             | 584/61                   | 457.00                            |
| Slue Hill                  | 42.2"          | 575/48             | 792/47             | 1121/45            | 1397/47            | 1736/44            | 1906/41             | 1843/41            | 1600/40            | 1298/40            | 918/45             | 583/80                   | 457/ <b>63</b><br>476/ <b>5</b> 0 |
| Boston                     | 42 4"          | 476/55             | 709/63             | 1015/50            | 1325/49            | 1619/47            | 1816/44             | 1748/45            | 1486/47            | 1259/44            | 880/48             | 503/87                   | 402/57                            |
| Lynn                       | 425            | 435/59             | 770/48             | 1106/46            | 1453/45            | 1674/45            | 1983/30             | 1987/37            | 1556/44            | 1253/44            | 852/48             | 490/67                   | 369/00                            |
| Natick                     | 42 3*          | 580/47             | 855/42             | 1202/41            | 1441/45            | 1843/39            | 1508/64             | 1891/40            |                    | 1323/41            | 982/41             | 542/84                   | 494/48                            |
| MICHIGAN #                 |                |                    |                    |                    | )                  | i .                | ' '                 |                    | ;                  |                    |                    |                          |                                   |
| <b>Detroit</b>             | 42.2*          | 417/60             | 680/54             | 999/51             |                    |                    | 1865/42             | 183,4/41           | 1574/44            | 1252/48            | 875/4 <b>7</b>     | 473/50                   | 343/64                            |
| East Lansing Flint         | 427*           | 446/57 -<br>383/63 |                    | 1139/44            |                    |                    | 2016/38             | 1981/37            | 1718/38            | 1375/38            | 940/42             | 501/56                   | 398/67                            |
| Grand Rapids               | 42 8           | 369/64             | 636/ <b>56</b> )   | 956/53<br>1014/48  | 1339/48            | 1657/48<br>1754/42 | 1812/44             | 1795/42<br>1913/30 | 1554/44<br>1675/40 | 1195/48            | 829/49             | 429/62                   | 309/66                            |
| Lansing                    | 42.8           | 498/53             | 785/48             | 1135/44            | 1320/48            | 1839/30            | 2038/37             | 2006/36            | 1773/36            | 1261/44<br>1390/38 | 858/47<br>951/41   | 446/60<br>516/66         | 311/66<br>413/56                  |
| Sault Sta Marie            | 46 5*          | 325/63             |                    | 1028/46            | 1382/45            |                    | 1810/44             | 1834/41            | 1522/44            | 1049/50            | 673/54             | 331/66                   | 253/66                            |
| Traverse City              | 44 7*          | 311/67             |                    | 1000/48            |                    |                    | 1911/40             | 1906/38            |                    | 1165/48            | 754/61             | 377/84                   | 250/00                            |
| MINNESOTA                  |                |                    |                    |                    |                    |                    | • ,                 |                    |                    |                    |                    |                          |                                   |
| Dulisth                    | 46 6.          | 388/55             | 673.47             | 1034/45            | 1372/48            | 1631/46            | 1766/45             | 1853/40            | 1546/42            | 1095/48            | 725/50             | 380/50                   | 291/90                            |
| internat : Falls           | 48 6 '         | 356/54             | 662/48             | 1045/41            | 1442/41            | 1715/42            | 1852/42             | 1920/38            | 1618/39            | 1121/45            | 704/48             | 345/90                   | 271/68                            |
| Minn St Pay<br>Rochester   | 43.6           | 464 50             | 763.45             | 1102 44            | 1440/44            | 1736/42            | 1927 40             | 1969/37            | 1686/39            | 1254/42            | 859/44             | 480/54                   | 353/57                            |
| St Cloud                   | 46 6           | 475/61<br>627/31   | 752/47             | 1061/46            |                    | 1694/45            | 1900/41             | 1907/30            | 1661/40            | 1250/44            | 869/45             | 494/65                   | 370/68                            |
| MISSISSIPPI                |                | 927 31             | 92331              | 1346129            | 1559/30            | 1038/38            | 1994/38             | 2046/34            | 1610/33            | 1327/38            | 888/41             | 538/47                   | 453/44                            |
| Jackson                    | 32.3           | 753/61             | 1026/46            | 1368/42            | 1707/30            | 1940/37            | 2023/37             | 1907/30            | 1780/38            | 1508/40            | 1271/38            | 901/45                   | 708/44                            |
| Meridian                   | 32 3.          |                    | 1012/47            |                    |                    | 1859/40            | 1961/30             |                    | 1736/40            | 1453/44            | 1257/38            | 896/45                   | 099/61                            |
| MISSOURI                   |                | ×                  | 1                  |                    | , 1                |                    |                     |                    |                    |                    |                    |                          |                                   |
| Columbia                   | 30 0           | 612/               | W47                | 1178/46            | 1525/44            | 1678/30            | 2088/36             |                    | 1876/33            | 1449/38            | 1100/38            | 703/47                   | 522/83                            |
| Kansas City                | 36.3 .,        | 647/4              | 4/45               | 1202/44            | 1574/41            | 1871/30            |                     | 2104/33            | 1862/34            | 1451/38            | 1092/38            | 737/44                   | 561/49                            |
| St Louis :                 | 36.7*          | 627/49             | <b>705/40</b>      | 1204/45            | 1563/42            | 1870/36            |                     | 2048/34            |                    | 1458/38            | 1099/38            | 718/48                   | 530/63                            |
| MONTANA                    | 372"           | 083/48             | 925/46             | 1235/45            | 1603/43            | 1881/39            | 2074/36             | 2061/34            | 1672/34            | 1479/38            | 1143/38            | 775/45                   | 602/48                            |
| Billings                   | 45.8*          | 406/46             | 763/42             | 1189/38            | 1525/40            | 1012/87            | 2172/32             | 2382/23            | 2021/25            | 1460/31            | 906/33             | 561/44                   | 421/47                            |
| Dillon                     | 45.2           | 526/44             |                    | 1279/33            | 1638/36            | 1988/34            | 2142/33             | 2391/23            | 2022/26            | 1520/29            | 1022/32            | 601/41                   | 450/45                            |
| Giasgow                    | 48.2"          | 387/50             | 671/46             | 1104/38            | 1487/40            |                    | 2046/37             | 2192/20            | 1862/30            | 1339/34            | 877/37             | 479/48                   | 333/60                            |
| Great Falls 6              | 475            | 420/48             | 719/42             | 1169/37            | 1487/40            |                    | 2100/34             | 2327/25            | 1932/28            | 1377/33            | 924/34             | 496/46                   | 335/63                            |
| Helena                     | 46.            | 419/51             | 700/45             | 1145/39            | 1486/41            | 1859/38            | 2038/37             | 2333/26            | 1929/29            | 1412/33            | 925/37             | 521/48                   | 364/51                            |
| Lewiston                   | 470            | 420/50             | 692/46             | 1128/39            | 1443/42            |                    | 2058/36             | 2286/27            | 1900/30            | 1371/34            | 904/37             | 502/47                   | 363/50                            |
| Miles City                 | 44.4*          | 457/47             |                    | 1184/37            | 1541/30 /          |                    | 2144/33             | 2296/27            | 1976/27            | 1443/31            | 960/34             | 550/44                   | 390/47                            |
| Missoula -                 | 44 1:          | 312/63             | 574/66             | 981/47             | J382/45 :          |                    | 1932/40             | 2326/25            | 1880/30            | 1857/36            | 612/44             | 409/57                   | 267/64                            |
| Summit<br>NEBRASKA         | 48.3           | 450/42             | 597/50             | 900/45 i           | 1526/38            | 1703/44            | 1817/44             | 2065/33            | 1880/30            | 1305/36            | 796/42             | 376/57                   | 280/58                            |
| Grand Island               | 41.0           | 660/41             | 917/40             | 1264/38            | 1692/37            | 107:144            | 2241/30             | 2214/20            | 1938/31            | 1508/24            | 1237/33            | 720140                   | 680:44                            |
| Lincoln                    | 40.8           | 700/38             |                    | 1279/36            |                    | 1829/40            | 2009/38             | 1979/37            | 1936/31            | 1508/34<br>1519/33 | 1198/30            | 738/40<br>763/38         | 5 <b>89/44</b><br>634/ <b>38</b>  |
| North Omaha                | 414.           | 633/42             | 891/41             |                    | 1558/41            | 1871/30            |                     | 2105/33            | 1857/33            | 1372/40            | 1049/38            | 644/47                   | 511/49                            |
| North Platte               | 41.1*          | 892/38             | 958/36 -           |                    | 1723/34            | 1987/34            | 2265/30             | 2275/28            | 1988/24            | 1564/31            | 1176/30            | 759/38                   | 605/40                            |
| Scotta Bluff               | 41.6"          | 675/38             |                    | 130 AST            |                    | 1932/37            | 2235/31             | 2282/28            | 1996/29            | 1596/29            | 1145/31            | 723/30                   | 375/41                            |
|                            |                |                    | ı                  | ,                  |                    |                    | - 1                 |                    |                    |                    |                    |                          |                                   |
| NEVADA                     |                |                    |                    |                    |                    |                    |                     |                    |                    |                    |                    |                          |                                   |
| NEVADA<br>Elko<br>Ely      | 408'           | 589/39<br>819/32   | 1034/33<br>1140/30 | 1462/30<br>1605/25 | 1898/29<br>2008/25 | 2302/24 2309/24    | 2532'21  <br>251122 |                    | 2314/18            | 1891/18            | 1322/22            | 812/34<br>925/29         | €16/40<br>722/34                  |



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# INSOLATION AND PERCENT DIFFUSE TABLES, CONTINUED BTU per ft. per day /% DIFFUSE

| City                       | Lee         | , Jen             | Feb               | Mer     | <b>A</b> #* .      | _ May              | June               | 349                | Aug                 | Sept.              | Cet                                     | Nev              | Dee            |
|----------------------------|-------------|-------------------|-------------------|---------|--------------------|--------------------|--------------------|--------------------|---------------------|--------------------|---|------------------|----------------|
| Las Vines                  | 38.1*       | 977/28            | 1338/23           | 1822/18 | 2310/10            | 204444             |                    | 2000               |                     | ,                  |   | `                | -              |
| Lovelock                   | 4           | 003/31            | 1185/27           | 1655/22 | 2484/18            | 2644/14<br>2553/18 | 2776/13            | 2587/18            | 2353/10             | 2036/18            | 1538/10                                 | 1085/26          | 880/           |
| Reno                       | 44.1        | - 800/33          | 1149/20           | 1648/23 | 2158/20            | 2521/10            | 2747/15<br>2700/18 | 2782/12<br>2690/14 | 2482/12<br>2404/15  | 2026/12<br>1996/14 | 1450/18<br>1430/18                      | 929/27           | 714            |
| Tonopah                    | <b>31</b> 1 | 818/26            | 1273/23           | 1770/10 | 2250/18            | 2576/18            | 2786/13            | 2701/14            | 2437/14             | 2041/14            | 1520/18                                 | 911/30           | 705            |
| Winnemucca                 | 40.0        | 900/30            | 1027/33           | 1471/30 | 1986/25            | 2360/23            | 2568/20            | - 2676/14          | 2347/18             | 1906/18            | 1321/22                                 | 809/34           | 826/           |
| NEW HAMPSHIRE<br>Concord   |             |                   |                   |         |                    | 1                  |                    | 20.0.1             |                     |                    | 1321/22                                 | 009734           | 010            |
| NEW JERGEY                 | 40.2        | 450/66            | . social          | 973/51  | 1316/49            | 1581/48            | 1704/47            | 1873/47            | 1455/47             | 1139/46            | 816/48                                  | 462/58           | 362/           |
| Atlantic City              | 30.4*       | 652/48            | 940/41            | 1419/33 | 1563/40            | 3017/41            | 2112/34            | 2084/33            | 1758/38             | 1445/38            | 1103/37                                 | 778/40           | 586/           |
| Lakehurst                  | 40.0        | 550/63            | 796/49            | 1106/48 | 1455/40            | 671/48             | 1773/45            | 1702/48            | 1531/48             | 1260/48            | 955/45                                  | 621/51           | 475/           |
| Newark                     | M 44.7      | 551/61            | 783/48            | 1106/47 | 1448/48            | 1686/45            | 1794/45            | 1758/44            | 1584/45             | 1272/45            | 950/45                                  | 596/51           | 454/           |
| Trenton<br>NEW MEXICO      | 443.        | 636/46            | 900/42            | 1264/40 | 1563/41            | 1810/41            | 2013/36            | 1991/37            | 1729/39             | 1434/34            | 1084/38                                 | 719/42           | 571/           |
| Albuquerque                | 36.0        | 1016/28           | 1341/25           | 1766/23 | 2227/20            | 2537/18            | 2677/18            | 2487/21            | 2289/21             | 1971/20            | 1545/20                                 | 1133/24          |                |
| Farmington                 | 30.7*       | 944/29            | 1280/26           | 1002/24 | 2132/22            | 2450/21            | 2004/18            |                    | 2251/21             | 1933/20            | 1478/21                                 | 1046/27          | 1927/<br>837/  |
| Roewell                    | 38.4        | 1046/30           | 1372/27           | 1806/23 | 2216/21            | 2458/21            | 2606/18            | 2439/22            | 2240/23             | 1912/23            | 1526/23                                 | 1131/20          | 951/           |
| Zuni<br>NEW YORK           | #L1*        | 995/30            | 1296/26           | 1886/27 | 2165/22            | 2472/20            | 2600/10            | 2263/28            | 2077/20             | 1893/23            | 495/23                                  | 1087/28          | 892/           |
| Albany                     | .42.7*      | 502/63            | 7                 | 1104/46 | 1483/42            | 1760/42            | 1950/38            | 405340             |                     |                    |   |                  |                |
| Binghamton                 | . 41.       | 300/64            | 675/82            | 860/58  | 1241/53            | 1493/51            | 1680/48            | 1957/37<br>1658/47 | 1899/38<br>1424/48  | 1316/41            | 916/44                                  | 525/84           | 399/           |
| Buffalo                    | 44.9        | 346/06            | 546/63            | 888/66  | 1314/48            | 1596/48            | 1806/44            | 1776/44            | 1512/48             | 1151/48            | 778/53                                  | 414/65           | 297/           |
| Rhaca                      | 48.4        | 450/57            | 748/48            | 1040/48 | 1283/61            | 1729/44            | 1987/38            | 1972/37            | 1896/38             | 1312/41            | 784/51<br>914/45                        | 403/64<br>461/60 | 284/<br>365/   |
| Massena                    | 44.0        | 431/64            | 602/40            | 1095/44 | 1500/41            | 1808/40            | 2006/38            | 1987/37            | 1087/38             | 1267/41            | 630/46                                  | 448/67           | 330/           |
| New York                   | 400.        | 500/66            | 720/54            | 1036/60 | 1363/48            | 1635/47            | 1709/47            | 1686/46            | 1482/47             | 1213/47            | 885/48                                  | 539/87           | 403/           |
| Rochester                  | 48.1        | 384/66            | 500/02            | 903/55  | 1338/48            | 1605/47            | 1818/44            | 1780/44            | 1518/48             | 1159/48            | 781/81                                  | 403/64           | 281/           |
| Scheriectady               |             | 47964             | 741/40            | 1010/50 | 1253/61            | 1526/60            | 1855/49            | 1637/46            | 1471/47             | 1106/50            | 807/50                                  | 470/50           | 383/           |
| Syrecuse<br>IORTH GAROLINA |             | F#26663           | 571/60            | 890/56  | 1323/49-           | 1577/48            | 1777/45            | 1757/44            | 1502/48             | 1 165/48           | 777/51                                  | 396/65           | 285/           |
| Asheville -                |             | 721/48            | 870/46            | 1305/42 | 1680-40            | 4800444            | 1851-17            | ٠٠                 |                     |                    |   |                  |                |
| Cape Hatteres              | 23.         | 005/61            | 952/47            | 1305/42 | 1660/40<br>1773/36 | 1803/41<br>1960/37 | 1854/42            | 1775/44<br>1910/39 | 1826/44<br>-1705/41 | 1360/45<br>1470/40 | 1148/40                                 | 848/42           | 657/           |
| Charlotte                  | <b>31.</b>  | 719/40            | 870/40            | 1314/42 | 1004/30            | 1854/40            | 2035/37<br>1929/40 | 1830/41            |                     | 1415/42            | 1136/41                                 | 073/41           | 059/           |
| Cherry Point               | 34.9*.      | 750/47            | 1024/44           | 1386/30 | 1783/36            | 1923/38            | 1937/30            | 1828/41            | 1894/41<br>1833/44  | 1433/42            | 1173/39.<br>1189/40                     | 865/42           | 072/           |
| Greeneboro                 | 36.1*       | 715/47            | 960/45            | 1312/41 | 1882/38            | 1867/30            | 1952/30            | 1862/40            | 1895/41             | 1417/41            | 1140/40                                 | 906/40<br>838/42 | 718/           |
| Relèigh                    | 36.8*       | 003/48            | 942/47            | 1275/44 | 1643/40            | 1807/41            | 1863/42            | 1774/44            | 1810/44             | 1370/44            | 1104/42                                 | 812/45           | 658/4          |
| Releigh-Durhem             | , 20.0°.    | 79342             | 1043/41           | 1379/30 | 1780/36            | 1905/38            | 1076/30            | 2038/36            | 1773/38             | 1483/40            | 1105/30                                 | 885/39           | 719/           |
| ORTH DAKOTA                |             |                   |                   | 1       |                    |                    |                    |                    |                     |                    | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |                  | . ,            |
| S(smarck<br>Farso          | 46.8°       | 467/46            | 775/30            | 1169/30 | 1458/42            | 1847/38            | 2059/36            | 2182/30            | 1876/31             | 1353/36            | 907/38 1                                | 507/47           | 372/           |
| Minot                      | 42.         | 415/51<br>383/61  | 705/48<br>655/48  | 1097/41 | 1475/41            | 1833/38<br>1845/38 | 1993/38            | 2119/32            | 1824/32             | 1303/38            | 074/30                                  | 457/51           | 337/           |
| HIO '                      |             |                   | 400144            | 1043/42 | 1460/41            | 1840/36            | 1073/30            | 2097/32            | 1799/32             | 1276/38            | 849/38                                  | 439/50           | 310/           |
| Akron                      | 40.9        | 428/62            | 849/58            | 963/54  | 1356/48            | 1887/48            | 1638/44            | 1786/44            | 1595/44             | 1271/45            | 907/47                                  | /505/60          | 353/           |
| Cleveland                  | 41.4        | 300/06            | 801/60            | 022/6   | 1349/48            | 1680/45            | 1842/42            | 1826/41            | 1581/44             | 1239/46            | 806/46                                  | 466/62           | 318/0          |
| Columbus                   | 40.0        | 450/00            | <b>87€/5</b> 7    | 879/64  | 1352/48            | 1846/48            | 1811/44            | 1754/48            | 1640/42             | 1270/45            | 949/48                                  | 537/57           | 387/           |
| Dayten                     | 30.9        | 480/58            | 725/88            | 1025/61 | 1402/48            | 1600/45            | 1872/42            | 1809/42            | 1644/41             | 13/17/44           | 969/45                                  | 564/68           | 407/           |
| Put-in-Bay<br>Teledo       | 41.8*       | 442/68            | 734/61            | 1077/48 | 1300/48            | 1821/40            | 1998/38            | 2090/33            | 1902/32             | 1471/34            | 1087/34                                 | 579/51           | 409/8          |
|                            | 41.8°       | 435/80<br>365/84  | 680/65            | 996/61  | 1363/48            | 1715/44            | 1077/41            | 1848/41            | 1015/42             | 1275/44            | 910/48                                  | 498/58           | 355/6          |
| Youngstown-<br>KLAHOMA     | 71.0        | 30000             | 586/62            | 889/67  | <b>4</b> 278/61    | 1585/48            | 1758/48            | 1733/45            | 1506/46             | 1193/48            | 851/48                                  | 456/63           | 315/           |
| Oklehoma City              | 35.4%       | \$00/42           | 1054/41           | 1399/38 | 1724/38            | 1917/38            | 2142/33            | 2127/32            | 1949/32             | 1553/37            | 1232/36                                 | 901/39           | 725/4          |
| <b>Stillweter</b>          | 36.11       | 900/42<br>03/44   | 1054/40           | 1430/37 | 1681/30            | 1851/40            | 2186/32            | 2186/30            | 1998/20             | 1877/31            | 1268/31                                 | 947/34           | 752/4          |
| Tulsa                      | 30.2        | 731/48            | 877/45            | 1305/42 | 1002/41            | 1821/41            | 2019/37            | 2029/36            | 1864/34             | 1471/39            | 1163/39                                 | 027/42           | 859/4          |
| REGON<br>Astoria           | 44.2        | ا                 | alama a           |         |                    |                    |                    | _                  |                     | i                  | İ                                       |                  | 3              |
| Bums                       | 1 au        | 314/64<br>490/61  | 545/58            | 866/54  | 1252/60            | 1607/47            | 1625/48            | 1745/44            | 1498/45             | 1183/45            | 712/51                                  | 387/60           | 261/6          |
| Cervallis                  | 443.        | 500/48            | 792/45<br>738/47  | 1186/40 | 1848/37            | 2051/32            | 2278/29            | 2459/21            | 2082/24             | 1619/27            | 1042/34                                 | 593/46           | 431/5          |
| Medford                    | 44.         | 407/82            | 737/50            | 1027747 | 1397/48<br>1638/36 | 1671/48 2032/33    | 1836/44<br>2276/29 | 1770/44            | 1633/40             | 1310/40            | 989/36                                  | 588/45           | 432/4          |
| North Bend .               | 44.         | 439/57            | 704/50            | 1058/47 | 1508/42            | 1858/30            | 1993/38            | 2473/21<br>2106/32 | 1785/36             | 1588/29            | 981/40                                  | 504/56           | 336/6          |
| Pendleton -                | 44.7        | 348/62            | 813/54            | 1043/46 | 1501/41            | 1924/37            | 2143/33            | 2394/23            | 1993/27             | 1376/38<br>1501/30 | 692/44<br>908/39                        | 524/53<br>438/56 | 380/5          |
| Portland                   | 46.0        | 310/66            | 554/68            | 885/84  | 1307/48            | 1662/45            | 1772/45            | 2036/34            | 1872/39             | 1256/44            | 723/51                                  | 438/56<br>387/62 | 292/8          |
| Redmend                    | 44.3        | 490/40            | 774/45            | 1190/39 | 1682/34            | 2078/31            | 2280/29            | 2444/22            | 2068/24             | 1583/28            | 999/38                                  | 571/47           | 260/8<br>424/5 |
| Salem                      | 44.9*       | 332/66            | 587/57            | 947/64  | 1309/47            | 1796/42            | 1847/42            | 2141/31            | 1773/36             | 1328/39            | 769/50                                  | 410/00           | 277/           |
| INNEYLYANIA<br>Allentown   |             | .,,_,             | ***               |         |                    |                    |                    |                    |                     | - 1                | - 1                                     | 1                |                |
| Alientown<br>Avoca         | 40.0        | 527/64<br>454/50  | 763/61            | 1078/48 | 1409/47            | 1836/47<br>1589/48 | 1776/45            | 1764/44            | 1545/45             | 1237/48            | 925/48                                  | 568/54           | 430/5          |
| Erie '                     | 42.1        | 345/66            | 577/62            | 919/55  | 1358/48            | 1589/48            | 1739/46            | 1744/45            | 1512/48             | 1198/47            | 896/47                                  | 490/59           | 368/6          |
| Harrisburg                 | 402.        |                   | 770/61            |         | 1410/47            |                    | 1846/42<br>1803/44 | 1832/41<br>1762/44 |                     | 1200/47            | 827/50                                  | 416/05           | 277/7          |
| Philadelphia               | 30.         | 535/54<br>555/63  | 794/50            |         | 1433/47            |                    | 1810/44            | 1757/44            |                     | 1265/45            | 933/46<br>958/45                        | 579/54<br>619/51 | 447/5          |
| Pittsburgh                 | 40.5*       | 42462             | 625/00            |         |                    |                    | 1761/46            | 1689/46            |                     | 1208/48            | 695/48                                  | 504/58           | 346/6          |
| State College              | 40.0        | 512/66            | 745/61            |         |                    |                    | 2006/38            | 1947/38            |                     | 1331/42            | 1014/40                                 | 571/54           | 442/5          |
| IODE ISLAND                |             |                   | •                 | ]       |                    |                    | .                  |                    |                     | -                  |   |                  | 4              |
| Newport                    | 41.5        | 571/48            | 852/44            |         |                    |                    | 1963/30            | 1017/39            | 1655/41             | 1401/38            | 1006/48                                 | 645/48           | 520/4          |
| Previdence                 | 41.7*       | <b>\$06/64</b>    | 739/61            | 1031/50 | 1373/40            |                    | 1774/45            |                    |                     | 1208/47            | 906/45                                  | 537/55           | 418/5          |
| NUTH CAROLINA              |             | 344               |                   |         |                    |                    | 1                  | 1                  | .                   |                    | 1                                       |                  |                |
| Charleston<br>Charles      | : :         | 744/60.<br>761/46 | 985/47<br>1020/48 |         |                    |                    | 1843/42            |                    |                     |                    | 1192/41                                 | 933.41           | 720/4          |
| Gravie-Setabro             | 379.        | 729/40            | 961/48            |         |                    |                    | 1946/39            |                    |                     |                    | 1211/30                                 | 920/40           | 721/47         |
| NITH DAKOTA                |             |                   | ~"7               | 132041  | 1697/39            | 1936/30            | 1918/39            | 1830/40            | 1699/40             | 1405/42            | 1180/34                                 | 880/40           | 670/40         |
| Huren                      | 44.4        | 489/40            | TARMEN            | 1113/44 | 1529/40            | 1870/38            | 2100/34            | 2181/30            | 1691/31             | 1417/34            | 988/37                                  | 577/48           | 405/53         |
| Pierre                     | 44.4        | 529/46            |                   |         | 1613/38            |                    |                    | - 10 11 00         | J                   | 14 17 (34)         | JUN 31                                  | J 7 8 9 8        | 402/3          |

# INSOLATION AND PERCENT DIFFUSE TABLES, CONTINUED BTU per ft. per day/% DIFFUSE

| Catu 3          | [ ]     | jen              | Feb     | Mar                 | Apr -    | May     | June                                    | July            | Aug      | Sept                | Oct       | Nov      | Dec             |
|-----------------|---------|------------------|---------|---------------------|----------|---------|---|-----------------|----------|---------------------|-----------|----------|-----------------|
| City 3          | Lat     | Jan              | , P80   | - Mai               | ~        | May     | Julia                                   | July            | ~~       | - Jeps              | ,<br>,    | 3        |                 |
| Rapid City      | 441.    | 542/45           | 826/41  | 1228/38             | 1588/38  | 1885/38 | 2130/33                                 | 2222/29         | 1961/29  | 1517/31             | 1063/32   | 646/40   | <b>~478/4</b> 9 |
| Sioux Falls     | 438     | 532/47           | 801/44  | 1152/42             | 1542/40  | 1892/38 | 2098/34                                 | 2149/31         | 1843/33  | 1409/36             | 1005/37   | 607/45   | 44 1/50         |
| TENNESSEE       | 175     | 3004.            | 00,,44  | 1102142             | 104240   | .002.00 |   |                 | 10.000   |                     |           |          |                 |
|                 | 35.0    | 630/53           | 858/53  | 1178/48             | 1549/44  | 1730/44 | 1830/42                                 | 1734/45         | 1629/44  | 1335/48             | 1108/42   | 772/48   | 580/59          |
| Chattanooga     | 35.0    | 682/51           | 944/48  | 1277/44             | 1638/41  | 1884/38 | 2043/37                                 | 1971/37         | 1823/37  | 1470/40             | 1204/38   | 818/48   | 628/6           |
| Memphis         |         | 601/55           | 882/50  | 1188/56             | 1638/49  | 1911/48 | 2081/43                                 | 2033/43         | 1845/44  | 1561/44             | 1199/46   | 608/57   | 605/6           |
| Nashviile       | 360.    |                  |         |                     |          | 1898/30 | 2009/38                                 | 1921/30         |          | 1537/37             | 1176/38   | 778/47   | 593/8           |
| Oak Ridge       | 360.    | 612/55           | 877/50  | 1202/47             | 1648/40  | 1030/36 | 2009/38                                 | 1921/30         | 1755/39  | 15,37797            | 11/0/30   | //04/    | 3874            |
| TEXAS :         | 1 . 1   |                  | i       |                     |          |         |   |                 |          |                     | 4040404   | 1007/38  | 863/3           |
| Abilene         | 324     | 923/40           | 1182/38 | 1575/33             | 1842/34  | 2036/34 | 2208/31                                 | 2138/32         | 1955/32  | 1596/37             | 1313/36   |          |                 |
| Amarillo        | 35 2    | 960/31           | 1242/31 | 1630/29             | 2017/27  | 2210/29 | 2392/25                                 | 2279/28         | 2102/27  | <b>1√59/29</b>      | 1403/28   | 1032/31  | 871/3           |
| Big Spring      | 32 2    | 988/36           | 1268/33 | 1718/28             | 2126/23  | 2109/32 | 2186/31                                 | 2035/34         | 1725/41  | 1928/23             | 1423/30   | 1073/33  | 958/3           |
| Brownsville     | 25 9*   | 912/50           | 1135/47 | 1456/42             | 1736/40  | 1926/38 | 2114/32                                 | 2211/ <b>29</b> | 2026/31  | 1892/37             | 1438/37   | 1054/45  | 862/1           |
| Corpus Christi  | 278*    | 897/48           | 1146/45 | *1437/42            | 1641/42- | 1865/39 | 2092/33                                 | 2184/30         | 1909/32  | 1686/36             | 1415/36   | 1072/42  | 844/4           |
| Dallas          | 32 8°   | 821/48           | 1071/44 | 1421/40             | 1826/42  | 1887/39 | 2134/83                                 | 2120/32         |          | ≠.15 <b>86/37</b> . | 1275/37   | 936/41   | 779/4           |
| El Paso         | 31 8*   | 1124/28          | 1479/23 | 1908/20             | 2362/18  | 2599/19 | 2680/19                                 | 2449/22         | .2283/22 | 1986/22             | 1638/21   | 1243/24  | 1030/2          |
| Fort Worth      | 32 8*   | 800/47           | 1083/44 | 1401/40             | 1810/42  | 1882/30 | 2145/33                                 | 2146/31         | 1972/32  | 1910/36             | 1276/37   | 926/42   | 757/4           |
| Houston         | 30.0    | 712463           | 1034/48 | 1296/47             | 1522/47  | 1773/42 | 1897/40                                 | 1827/41         | 1685/42  | 1470/42             | 1275/40   | 924/47   | 729/1           |
|                 | 275     | 91144            | 1161/45 | 1434/42             | 1662/42  | 1863/36 | 2035/36                                 | 2110/32         | 1921/34  | 1624/38             | 1309/37   | 1034/44  | 849/4           |
| Kingsville      | 33 .    | 1030 00          | 1331/29 | 1761/24             | 2166/22  | 2394/22 | 2543/21                                 | 2410/23         | 2207/24  | 1819/27             | 1467/27   | 1116/29  | 934/3           |
| Lubbock         |         | 702              | 1068/48 | 1375/42             | 1623/42  | 1865/40 | 2054/38                                 | 2005/36         | 1862/36  | 1529/40             | 1348/36   | 962/42   | 767/4           |
| Lufkin          | : 31.2* | 793              |         |                     |          |         |   |                 | 2208/24  | 1843/28             | 1521/27   | 1176/28  | 999/1           |
| Midland         | 31 0    | 1080 M           | 1382/29 | 1838/23             | 2191/22  | 2429/21 | 2561/20                                 | 2388/23         |          |                     |           |          | 754/1           |
| Port Arthur     | 20 0    |                  | 1070/47 | 1353/45             | 1609/44  | 1869/39 | 2009/37                                 | 1845/41         | 1735/41  | 1526/41             | 1321/38   | 952/45   |                 |
| San Angelo      | 31 4 *  | 961/30           | 1207/38 | 1605/33             | 1849/34  | 2030/34 | 2185/31                                 | 2121/32         | 1965/32  | 1606/37             | 1336/36   | 1043/37  | 894/3           |
| San Antonio     | 29 5    | 895/48           | 1154/44 | 1449/41             | 1811/44  | 1893/39 | 2068/34                                 | 2120/32         | 1946/33  | 1634/37             | 1349/37   | 1008/42  | 846/4           |
| Waco            | 31 8*   | 832/47           | 1095/44 | 1427/40             | 1811/42  | 1773/42 | 2111/33                                 | 2129/32         | 1957/33  | 1600/37             | 1301/37   | 958/42   | 802/4           |
| Wichita Fails.  | 340     | 861/41           | 1122/39 | 1471/37             | 1782/37  | 2016/34 | 2220/31                                 | 2165/31         | 1968/32  | 1601/36             | 1291/34   | 954/38   | 799/4           |
| TAH             | 1       |                  |         |                     | 1        | l       | 1                                       |                 |          | }                   | 1         |          | i               |
| Cedar City      | 377     | 681/31           | 1179/30 | 1634/25             | 2091/23  | 2466/20 | 2704/18                                 | 2502/20         | 2240/21  | 1967/19             | 1459/21   | 992/28   | 785/3           |
| Salt Lake City  | 40 8    | 838/44           | 988/37  | 1453/30             | 1893/29  | 2361/23 | 2559/21                                 | 2588/18         | 2252/20  | 1842/20             | 1293/24   | 787/36   | 570/4           |
|                 | ~ •     | 0.5044           | 300131  | 1400100             |          | 2001120 | 20000                                   |                 |          |                     |           |          |                 |
| ERMONT          |         |                  |         | .055.40             | 440044   | 1766/41 | 1949/38                                 | 1950/38         | 1872/39  | 1264/4              | 834/48    | 433/50   | 3204            |
| Burlington      | 445     | 425/50           | 678/51  | 1065/48             | 1449/44  | 1/00/41 | 1973/30                                 | 1950/30         | 10/239   | 1204/48             | 634/46    | 453/50   | 3200            |
| IRGINIA         |         |                  |         |                     |          | 1       |   |                 |          |                     |           |          | بمما            |
| Mt Weather      | 36 1    | 634/48           | 1010/38 | 1246/42             | 1526/44  | 1873/39 | 1935/40                                 | 1880/40         | 1585/44  | 1382/42             | 1036/41   | 745/44   | 919/4           |
| Nortoik         | 36 6    | 878/49           | 932/48  | 1280/42             | 1676/39  | 1886/38 | 1999/38                                 | 1852/41         | 4679/41  | 1395/41             | 1082/41   | 811/41   | 623/4           |
| Richmond        | 37 8    | 631/ <b>50</b> : | 876/48  | 1210/45             | 1565/42  | 1781/42 | 1871/42                                 | 3773/44         | 1599/44  | 1347/44             | 1032/44   | 733/47   | 586/            |
| Roanoke         | 37 3    | 660/49           | 899/47  | 1235/45             | 1581/42  | 1763/42 | 1881/41                                 | 1795/42         | 1819/44  | 1357/44             | 1080/41   | 764/45   | 590/5           |
| WASHINGTON      | I       |                  |         | l                   | 1        | }       | ļ                                       |                 |          |                     | Į.        | -        | l               |
| Olympia         | 470*    | 259/68           | 503/60  | 844/55              | 1255/50  | 1631/48 | 1992/47                                 | 1912/30         | 1548/42  | 1156/45             | 636/56    | 339/64   | 221/            |
|                 | 48.2    | 431/50           | 818/37  | 1294/31             | 1921/24  | 2271/24 | 2507/22                                 | 2606/19         | 2227/18  | 1689/20             | 1010/31   | 501/48   | 369/1           |
| Prosser         |         | 453/47           | 671/48  | 1095/41             | 1681/33  | 1998/33 | 2529/21                                 | 2603/19         | 2035/24  | 1578/24             | 944/34    | 542/44   | 354/9           |
| Pullman         | 48.7    |                  |         |                     |          | 1902/37 | 2385/25                                 | 2124/32         | 2216/19  | 1430/32             | 843/42    | 457/53   | 365/            |
| Richland -      | 48 3 *  | 317/64           | 741/44  | 1228/34             | 1721/32  |         |   |                 | 1685/38  | 1209/41             | 997/51    | 391/57   | 236/            |
| Seattle         | 47.4    | 288/95           | 501/59  | 973/47              | 1460/41  | 1847/38 | 1921/40                                 | 2090/32         |          |                     |           |          |                 |
| Spokane         | 477'    | 314/62           | 606/51  | 1040/44             | 1494/40  | 1917/36 | 2082/36                                 | 2355/24         | 1941/29  | 1434/31             | 840/40    | 397/56   | 255/            |
| Tacoma          | 47.2*   | 262/68           | 495/60  | 849/54              | 1293/48  | 1713/42 | 1801/44                                 | 2246/28         | 1815/40  | 1146/45             | 956/54    | 337/64   | 211/7           |
| Whidbey 1s      | 483     | 293/65           | 532/55  | 917/50              | 1345/45  | 1760/40 | 1820/45                                 | 1981/35         | 1592/40  | 1173/40             | 655/63    | 357/60   | 2334            |
| WEST VIRGINIA   |         | 1                |         | ŀ                   | 1        |         | 1                                       | ł               | 1        | 1                   | i         | 1        | !               |
| Charleston      | 38 4    | 498/60           | 706/57  | 1009/54             | 1355/50  | 1639/47 | 1774/45                                 | 1682/47         | 1514/47  | 1272/48             | 971/48    | 613/55   | 4404            |
| Parkersburg ,   | 30 3    | 527/56           | 745/54  | 1113/48             | 1397/48  | 1795/41 | 1994/38                                 | 1939/38         | 1784/37  | 1453/38             | 1047/41   | 616/53   | 487/            |
|                 | 30.3    | 327/30           | 140.04  | 11134               | 1031,45  | 1       | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 1000.00         |          | 110000              |           |          | 1               |
| VISCONSIN       |         | 450.50           | 740.40  | 108044              | 1425/45  | 1680/45 | 1870/42                                 | 1885/40         | 1619/41  | 1196/45             | 826/48    | 450/57   | 341/            |
| Eau Claire      | 44 9    | 452/53           | 746/4   | 1089444             |          |         |   | 1887/39         | 1621/41  | 1217/44             | 820/47    | 465/56   | 350/            |
| Green Bay       | 44 5    | 451/53           | 725/48  | 1103/44             | 1438/44  | 1718/44 | 1906/41                                 | 1899/30         |          | 1242/44             | 893/48 .  | 494/55   | 369/            |
| La Crosse       | 43 9    | 481/51           | 764/49  | 1100/45             | 1426/45  | 1712/44 | 1904/41                                 |                 | 1865/40  |                     |           |          | 388/            |
| Madison         | 431"    | 515/50           | 803/45  | 1135/44             | 1397/48  | 1742/42 | 1947/40                                 | 1933/38         | 1707/38  | 1299/41             | 910/44    | 504/\$\$ |                 |
| Milwaukee       | 42 9 '  | 479/54           | 736/49  | 1088/48             | 1441/45  | 1767/42 | 1976/39                                 | 1960/38         | 1718/38  | 1309741             | 907/44    | 524/64   | 37\$/           |
| MYOMING         | L .     |                  | İ       | I                   |          | 1       | t                                       | l .             | 1        |                     | 1         | 1        | <b>.</b> .      |
| Casper          | 429     | 682/34           | 1013/30 | 1441/29             | 1846/29  | 2202/29 | 2500/22                                 | 2533/19         | 2224/20  | 1749/21             | 1218/24   | 764/32   | 593/            |
| Cheyenne        | 411     | 765/31           | 1067/30 | 1432/31             | 1769/33  | 1994/34 | 2257/30                                 | 2229/29         | 1965/30  | 1666/27             | 1241/27   | 822/32   | 971/            |
| Lander          | . 42 8° | 848/19           | 1183/19 | 1662/18             | 2038/22  | 2156/29 | 2488/23                                 | 2389/23         | 2138/23  | 1711/23             | 1312/19   | 874/23   | 726/            |
|                 | 413     | 826/25           | 1099/28 | 1563/24             | 1836/31  | 2020/33 | 2311/29                                 | 2186/30         | 1939/31  | 1548/32             | 1176/30   | 837/31   | 675/            |
| Laramie         |         |                  |         |                     | 1943/27  | 2343/23 | 2573/20                                 | 2546/19         | 2238/20  | 1532/19             | 1305/22   | 826/31   | 650/            |
| Ro k Springs    | 410     | 734-33           | 1088/20 | 1530/25<br>1204/38  |          | 1882/38 | 2155/33                                 | 2327/25         | 2005/27  |                     | 1005/34   | 590/44   | 441/4           |
| Sheridan        | 44 8    | 517/45           | 787/42  | 1204/38             | 1537/40  | 1002/36 | 413333                                  | 2321123         | 2003/2/  |                     | 7 .000.00 | 1 220    | <del>-~~</del>  |
|                 | 1       | T                |         |                     |          | F       | 1                                       | ]               | 1        | i                   | ,         |          | l               |
| ALBERTA         | 1       |                  |         |                     |          | 1876/36 | 1891/41                                 | 1939/37         | 1508/41  | 1099/40             | 693/30    | 409/36   | 245/            |
| Edmonton        | 53 9 .  | 328/30           | 649/32  |                     | 1522/34  | 1 ,0.00 |   |                 |          |                     |           | 516/37   | 332/            |
| Lethbridge      | 40 0    | <b>442/38</b>    | 774/32  | 1253/29             | 1548/37  | 1917/36 | 2138/33                                 | 2249/28         | 1917/28  | 1364/31             | 885/33    | 310/3/   | 3321            |
| RITISH CÓLUMBIA | 1       | $\sim$           | تعسيا   | 7                   | l        | 1       |   | 1               |          | 000.0.              | 500.00    |          | 200             |
| √≱ncouver       | 490     | 280/83           | 383/67  | 689/62              | 1264/48  | 1725/42 | 1777/45                                 | 2009/36         | 1467/45  | 929/54              | 590/56    | 350/58   | 206/            |
| MANITOBA        | 1       | 1 .              | 4       | 1 -                 | i        | 1       | 1                                       | k               |          | 1                   | 1         |          |                 |
|                 | 58 7*   | 240/23           | 553/23  | 1124/18             | 1640/24  | 1880/33 | 1954/38                                 | 1862/38         | 1401/42  | 829/49              | 424/53    | 22W45    | 1,29/           |
| Winning         | 49 9    | 483/31           | 829/27  |                     | 1618/33  | 1880/37 | 1935/40                                 | 2094/32         | 1740/34  | 1179/41             | 756/42    | 439/48   | 3'39/           |
|                 |         | 403(3)           | 02721   | , , , , , , , , , , | 1.0.00   | 1       | 1                                       | 1               | 1        | 1                   | 1         |          | 1 .             |
| HEW BRUNSWICK   | 1       |                  |         | 10004               |          | 1622144 | 1659/48                                 | 1733/45         | 1512/45  | 1143/48             | 774/48    | 405/58   | 332/            |
| * Moncton       | 48 1**  | 369/ <b>56</b>   | 664/51  | 1069/44             | 1401/45  | 1622/46 | 1039/48                                 | 1733/45         | 1312143  | 1143748             |           | -55      | 302,            |
| NEWFOUNDLAND    | 1       | l .              |         | 1                   | 1        |         | 1                                       | 1               |          |                     |           | 205.42   | 258/            |
| St Johns        | 47.5    | 295/54           | 553/58  | 885/51              | 1180/53  | 1475/50 | 1585/50                                 | 1622/48         | 1253/54  | 1032/ <b>50</b>     | 627/56    | 295/67   | 254/            |
| ONTARIO         |         | 1                | 1       | 1                   |          | 1       | 1                                       | 1 '             | 1        | 1                   | 1         |          |                 |
|                 | 45 47   | 531/42           | 841/37  | 1235/36             | 1486/41  | 1832/39 | 2057/36                                 | 2016/38         | 1729/37  | 1309/39             | 815/48    | 453/55   | 402/            |
| Ottawa .        |         | 405/45           |         | 1143/34             | 1364/45  |         | 1770/45                                 | 1770/42         | 1475/45  | 995/50              | 590/56    | 295/64.  | 295/            |
| Sapuskasing     | 49 4    |                  | 700739  | 1077/45             | 1372/47  | 1762/42 |   |                 |          |                     |           | 453/58   | 350/            |
| Toror to        | 43 7    | 446/55           | 6H2/57  | 10///48             | 13/247   | 1/02/4  | 1517/40                                 | 1343738         | 1000142  |                     |           |          | 1               |
|                 |         | _                |         |                     |          |         |   |                 |          |                     |           |          |                 |
| QUESEC          | 455     | 405-56           |         | 1180,38             | 1435-42  | 1       | 1806/44                                 | 1880/40         | 1622/40  | 1143/47             | 737/51    | 369/84   | 295/            |

## COLLECTOR TILT FACTORS

|      |             |                      |            |              |              |                      |               |              |              |              |              |              |               | <u>, , , , , , , , , , , , , , , , , , , </u> |                      |
|------|-------------|----------------------|------------|--------------|--------------|----------------------|---------------|--------------|--------------|--------------|--------------|--------------|---------------|---|----------------------|
|      |             | ·                    | LATITUDE   | JAN          | FEB          | MAÑ                  | APR           | MAY          | JUNE         | JULY         | AUG          | SEPT         | ост           | NOV   | DEC                  |
|      |             | COLLECTOR            | 24         | 1 13         | 1 09         | 1 04                 | 1 00          | 0 97         | 0 96         | 0 97         | 1 00         | 1 04         | 1 10          | 1 12  | 1 15                 |
| ı    |             | TILT =               | 32         | 1 34         | 1 24         | 1 11                 | 0 99          | 0 93         | 0 94         | 0 92         | 0 98         | 1 11         | 1 28          | 1 34  | 1 42                 |
|      | •           | LAT 15               | 40<br>48   | 1 67         | 1 41         | 1 23.                | 1 01          | 0 90         | 0 90         | 0.89         | 1 02         | 1 21         | 1 42          | 1 73  | 1 76                 |
| . 1  | 20% Diffuse | <u> </u>             | <u> </u>   | 2 18         | 1 64         | 1 51                 | <b>≠</b> 1 10 | 0 96         | 0.80         | 0 95         | 1 08         | 1 43         | 1 73          | 2 26  | 2 56                 |
|      | Ħ           | COLLECTOR            | 24         | 1 31         | 1 21         | 1 08                 | 0 95          | 0 87         | 0 85         | 0 87         | 0 94         | 1 08         | 1 21          | 1 28  | 1 37                 |
|      | Ö           | TILT =               | 32         | 1 56         | 1 39         | 1 16                 | 0 97          | 0 79         | 0 76         | 078          | 0 96         | 1,15         | 1 45          | 1 56  | 1 71                 |
| I    | æ           | LATITUDE             | 40<br>48   | ₹95<br>253   | 1 55         | 1 2 <b>8</b><br>1 57 | 0.98          | 0 75         | 0 75<br>0 74 | 0.74         | 1 00         | 1 25         | 1 57          | 2 05  | 2 10                 |
|      | è           | <del></del>          |            | -            |              | -                    | +             | <u> </u>     | 0 /4         | 0 89         | 1 05         | 1 49         | 1 90          | 2 63  | 3 04                 |
| j    | 7           | COLLECTOR            | 24         | 1 40         | 1 25         | 1 06                 | 0.80          | 0 70         | 0 67         | 0 70         | 0 79         | 1 05         | 1 27          | 1 36  | 1 50                 |
| ı    |             | TILT =               | 32<br>40   | 169          | 1 45         | 1 1 <b>3</b><br>1 25 | 0.89          | 0 59<br>0 67 | 0 55<br>0 65 | 0 58<br>0 66 | 0.68         | 1 12         | 1 54          | 1 68  | 1 89                 |
| - 1  |             | LAT + 15             | 48         | 2 72         | 1 85         | 1 54                 | 1 00          | 0 79         | 0 65         | 0 78         | 0 92<br>0 97 | 1 23<br>1 45 | 1 63<br>1 98  | 2 24<br>2 84                                  | 2 30                 |
| ı    |             |                      | 24         | 1 10         | 1 07         | 1 03                 | 1 00          | 0 97         | 0 96         |              |              |              |               |   | -                    |
| 7    | _           | COLLECTOR            | 32°        | 1 27         | 1 20         | 1 09                 | 0 98          | 097          | 0 96         | 0 97         | 1 00<br>0 97 | 1 03<br>1 09 | 1 07<br>1 22  | 109   | ,1 12                |
| Į    | -           | TILT =  <br>LAT - 15 | 40"        | 1 52         | 1 33         | 1 18                 | 0 98          | 0 89         | 0.89         | 0 89         | 100          | 1 16         | 1 34          | 1 26  | 1 33                 |
| 1    | 3           |                      | , 48"      | 1 93         | 1 50         | 1 42                 | 06            | 0 94         | 0.78         | 0 93         | 1 04         | 1 35         | 1 57          | 2 02  | 2 23                 |
| ,    | 10% Diffuse | COLLEGIOS            | 24'        | 1 24         | 1 16         | 1 06                 | 095           | 0 88         | 0.86         | 0 88         | 0.94         | 1 05         | 1 17          | 1 21  | 1 28                 |
| ł    | ä           | COLLECTOR TILT =     | 32         | 1 44         | 1 31         | 1 12                 | 0 96          | , 0 79       | 0 76         | 0 78         | 0 95         | 1 11         | 1 36          | 1 43  | 1 56                 |
| I    | Ż           | LATITUDE             | 40°        | 174          | 1 44         | 1 21                 | 0 96          | 0 74         | 0 74         | 0 73         | 0 97         | 1 19         | 1 46          | 1 84  | 1 87                 |
| 1    | 호           |                      | 48"        | 2 20         | 1 61         | 1 45                 | 1 03          | 0 88         | 0 73         | 0 87         | 1 01         | 1 38         | 1 71          | 2 31  | 2 60                 |
| -    | •           | COLLECTOR            | 24^        | 1 32         | 1 19         | 1 03                 | 0.80          | 0 72         | 0 69         | 0 72         | 0 79         | 1 03         | 1 20          | 1 26  | 1 38                 |
| 1    |             | TILR =               | 32<br>40   | 1 53<br>1 85 | 1 36<br>1 47 | 1 09                 | 0 89<br>0 88  | 0 59<br>0 67 | 0 56         | 0.58         | 0.88         | 1 08         | 1 42          | 1 52  | 1 70                 |
| Į    | 1           | LAT. + 15            | 48"        | 2 34         | 1 64         | 1 41                 | 0 95          | 0.78         | 0 66<br>0 64 | 0 66         | 0 90         | 1 15<br>1 34 | 1 50<br>1 75  | 1 98<br>2 48                                  | 2 03<br>2 <b>8</b> 2 |
| 1    |             | 1                    | 24"        | 1 07         | 1 05         | 1 02                 | 1 00          | 0 98         | 0 97         | 0.98         | 0 99         | 1 02         | 1 05          | 1 06  | 1 09                 |
| - 1  |             | COLLECTOR            | 32         | 1 20         | 1 15         | 1 06                 | 0 97          | # 93         | 0.95         | 0 92         | 096          | 1 06         | 1 17          | 1 19  | 1 25                 |
| - [  | 4           | LAT - 15°            | ^ 40:      | 1 38         | 1 25         | 1 13                 | 0 96          | ó <b>86</b>  | 0 89         | 0 88         | 0.98         | 1 12         | 1 26          | 1 45  | 1 46                 |
| - [  | 3           |                      | 48*        | 1 69         | 1 35         | 1 33                 | 1 02          | 0 92         | 0 77         | 0 91         | 1 00         | 1 27         | 1 42          | 1 77  | 1 90                 |
| 1    | £           | COLLECTOR            | 24.        | 1 17         | 1 11         | 1 04                 | 0 94          | 0 89         | 0 87         | 0 89         | 0 93         | 1 03         | 1 12          | 1 13  | /1 20                |
|      | 60% Diffuse | TILT =               | 32*        | 1 31         | 1 24         | 1 07                 | 0 94          | 0 79         | 0 76         | 0 78         | 0 94         | 1 07         | 1 26          | 1 36  | 141                  |
| Į    |             | LATITUDE             | 40°        | 1 53<br>1 87 | 1 32         | 1 14                 | 093           | 0 73         | 0.74         | 0 73         | 0.95         | 1,12         | 1 35          | 1 63  | 1 65                 |
|      | Ż           |                      |            |              |              |                      | +             | 0.86         | 0 72         | 0.85         | 0 97         | 1 28         | 1 51          | 1.98  | 2 16                 |
| - [  | •           | COLLECTOR            | 24′<br>32′ | 1 22<br>1 37 | 1 13         | 1 00                 | 0.80          | 0 73         | 0 71         | 0 73         | 0 79         | 1 00         | 1 13          | 1 16  | 1 25                 |
|      |             | TILT =<br>LAT. + 15  | 32°        | 1 60         | 1 26<br>1 34 | 1 04                 | 0 88          | 0 59         | 0 56<br>0 66 | 0 58         | 0 87         | 1 03         | ,1 30<br>1 37 | 1 36<br>1 72                                  | 1 50                 |
|      | ļ           | LAI. + 15'           | 48"        | 196          | 1 43         | 1 29                 | 0.91          | 0 77         | 0 64         | 0 76         | 0 89         | 1 23         | 1 37          | 2 09  | 1 76<br>2.31         |
| Ì    |             |                      | 24°        | 1 04         | 1 03         | ,101                 | 1 00          | 098          | 0 97         | 0.98         | 0 99         | 1 01         | 1 03          | 1 04  | 1 05                 |
|      |             | COLLECTOR<br>TILT =  | 32         | 1 12         | 111          | 1 04                 | 0 96          | 0 93         | 096          | 0 92         | 0 96         | 104          | 1 11          | 1 12  | 1 16                 |
| ŀ    |             | LAT - 15°            | 40°        | 1 24         | 1 17         | 1 08                 | 0 94          | 0 88         | 0.88         | 0 87         | 0 96         | 1 07         |               | 1 30  | 1 31                 |
| Ì    | 80% Diffuse |                      | 48"        | 1 44         | 1 22         | 1 24                 | 0 98          | 0 90         | 0 75         | 89           | 0 97         | 1 19         | 1 27          | 1 53  | 1 57                 |
| - [: | €           | COLLECTOR            | 24         | 1 10         | 1 07         | 1 01                 | 0 94          | 0 90         | 0 89         | 0 90         | 0 93         | 1 01         | 1 07          | 1 06  | 1 11                 |
| ľ    | 5           | TILT =               | 32         | 1 19         | 1 16         | 1 03                 | 0 93          | 0 79         | 0 77         | 0.78         | 0.93         | 1 03         | 1 17          | 1 18  | 1 26                 |
| ľ    | 2           | LATITUDE             | 40         | 1 33         | 1 25         | 1 07                 | 0 90          | 0 73         | 0 74         | 0 72         | 0 93         | 1 06         | 1 23          | 1 42  | 1 43                 |
|      | 9           | <del>`</del>         |            |              |              | 1 22                 | 0 94          | 0.84         | 0 70         | 084          | 0 93         | 1 18         | 1 31          | 1 66  | 1 72                 |
| ľ    |             | COLLECTOR            | 24         | 1 12         | 106          | 0 98                 | 0.80          | 0 75         | 0 73         | 0 75         | 0 79         | 0 97         | 1 06          | 1 05  | 1 13                 |
| 1    | - 1         | TILT =               | 32<br>40   | 1 21         | 1 17         | 0 99                 | 0 87<br>0 83  | 0 60         | 0 57         | 0 59         | 0.86         | 0 99         | 1 18          | 1 19  | 1 31                 |
| ,    | -           | LAT. + 15°           | 48         | 1 58         | 1 23         | 1 16                 | 0 87          | 0 66         | 0 66         | 0 65         | 0 86         | 1 01         | 1 24          | 1 47  | 1 49                 |
| _    |             |                      |            |              |              |                      | <u> </u>      | ا            | 3 00         | , 5,5        | 000          | . '-         | . 23          | 171   | 1/9                  |

## STUDENT WORKSHEET

## CDA SUN-CHART CALCULATION WORKSHEET

| JOB<br>LOCATION<br>LATITUDE |  |   | COL  | LECTOR TYP<br>LECTOR TILI<br>PLICATION                          | PE   |                               |  |                                |             |             |  | •   |
|-----------------------------|--|---|--|---|--|-------------------------------|--|--------------------------------|-------------|-------------|--|---|
|                             | ٨  | В   | С  | D   | E  | F                             | G  | н                              | J           | к           | L  | RESULT  |
|                             | COLLECTOR<br>HEAT GAIN<br>FACTOR<br>(TABLE 8)<br>OR MFG S<br>LIT | COLLECTOR HEAT LOSS FACTOR (TABLE 8) OR MFG S LIT | AVERAGE<br>DAYTIME<br>AIR<br>TEMPERA<br>TURE F | HORIZONTAL<br>SOLAR<br>ENERGY<br>(FROM<br>TABLES)<br>APPENDIX B | COLLECTOR<br>TILT FACTOR<br>(FROM TABLE)<br>APPENDIX C | INCIDENT<br>ENERGY<br>F D x E | COLLECTOR<br>INLET<br>TEMPERA<br>TURE<br>(TABLE 9) | É<br>COLUMN G<br>COLUMN C<br>F | - J<br>Bx2H | K ½         | L IS<br>FOUND FROM<br>FIGURE 41<br>USING K | TOTAL<br>ENERGY<br>COLLECTED<br>F F x L<br>BTU SQ<br>FT DAY |
| JANUARY                     |  | ,   |  |   | • '  |                               |  |                                |             |             |  |   |
| FEBRUARY                    |  |   |  |   |  |                               |  | \                              |             |             |  |   |
| MARCH                       | 6  |   |  | ,   |  |                               |  |                                |             |             |  |   |
| APRIL                       | ·  |   |  |   |  |                               |  |                                |             |             |  |   |
| MAY                         | ,  |   |  |   | ,  | •                             |  |                                |             |             |  | - (   |
| JUNE                        |  |   |  |   |  |                               |  |                                |             |             |  |   |
| JULY                        |  | 7   |  |   | *  |                               |  |                                | <u>·</u>    |             | •  | 1,  |
| AUGUST                      |  |   |  | ,   | 4.   |                               | <del>/</del>                                       | . :                            | , ,         |             |  |   |
| SEPTEMBER                   |  | •   | -  |   | <i>'</i>   |                               |  |                                | •           | <del></del> |  | •   |
| OCTOBER                     | ,  | ī   |  | •   |  | •                             |  | -                              |             |             |  | *   |
| NOVEMBER                    |  |   |  |   |  |                               |  |                                |             |             |  | ٠,  |
| DECEMBER                    |  | *   |  |   |  |                               | · · · · · ·  |                                | · ·         |             |  |   |

worksneets are avaitable upon request from Copper Development Assn. Inc

Courtesy Copper Development Association Inc.



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Step 4: Find the combined space and water heating requirement for the month of March; in the completed worksheet, this figure is 275,200 Btu/day

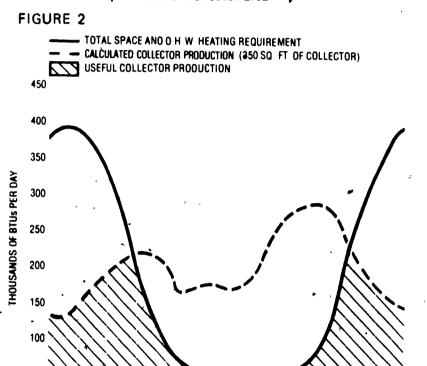
(NOTE: This figure must be interpolated from the chart in Figure 1, Assignment Sheet #2.)

- Step 5: Make a preliminary estimate of required collector area by dividing 544 into 275,200; the answer is about 500 square feet
- Step 6: Make a numerical check of estimated collector area by dividing the total solar heat collected (1,715,720 Btu from the chart in Figure 1) by the annual heat requirement (2,188,920 from the chart in Figure 1).

Example: In any month, only that portion of the collectable energy which can be applied to the load is considered; in May when only 68,950 Btu/day are required, only this portion of the available solar heat is applied to the load

For the sample Nashville application, the estimated collector area of 500 square feet would supply 78% of the annual load (see the chart in Figure 1). Since this is higher than desired, an adjusted collector area of 400 feet should be considered. This yields a result of 68% of the total load supplied by solar energy, and is consistent with the recommended guidelines of 60 to 70 percent. Another trail can be made using 350 square feet of collector area. This yields 62% of the annual heating requirement, so the collector selected should be between 350 and 490 square feet

Step 7: Check your calculations by drawing a graph to show the amount of useful solar heat produced by the square footage of the collector area; in the example in Figure 2, this availability of useful solar heat is indicated by the shaded area and is based on 350 square feet of collector area



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Assignment: Refer to the worksheet you completed in Assignment Sheet #1 and size a collector for the application assigned for that activity; interpolate from the chart in Figure 1 as required or make new entries for Btu/day requirements as your personal worksheet dictates; sketch a graph to check your calculations and model it after the graph in Figure 2.

# LOAD CALCULATIONS AND SOLAR COOLING UNIT III

|    |          | · NAME  |       | ·                       |
|----|----------|---|-------|-------------------------|
|    |          | TEST  |       |                         |
| 1. | Match th | ne terms on the right with their correct definitions.   |       |                         |
|    | a.       | British thermal unit; the amount of heat required to raise the temperature of one   | 1.    | <b>Psycho</b> metric    |
|    |          | pound of water one degree Fahrenheit  | 2.    | R-value                 |
|    | b        | British thermal units per hour; unit used to express hourly heat flow   | 3.    | Load                    |
|    | . с.     | The air temperature as measured by an   | 4.    | Heat loss               |
|    |          | ordinary thermometer  | 5.    | Btuh                    |
|    | d.       | The air temperature as measured by a thermometer whose bulb is covered with a wet cloth or wet wick and moved in air that has a                   | 6.    | Dry-bulb<br>temperature |
|    | ,        | velocity of one thousand feet per minute  | 7.    | Cfm                     |
|    | ·e.      | The amount of heat lost through all building surfaces, walls, floors, doors, and windows  | 8.    | Nomogram -              |
|    | •        | exposed to outdoors or to adjoining spaces with different temperatures  | 9.    | Refrigerant             |
|    | f.       | The amount of heat gained through all building surfaces, walls, floors, doors, and  | 10.   | Wet-bulb<br>temperature |
|    | •        | windows exposed to outdoors or from adjoining spaces with different temperatures  | 11.   | Absorbent               |
|    | g.       | The total heat loss and heat gain of a structure expressed in Btuh; this calculation is used to size heating and cooling equipment                | · 12. | Heat gain               |
|    | h.       | Controlled air brought into a structure   |       |                         |
|    | i.       | Uncontrolled air that leaks into a structure  |       |                         |
|    |          | The amount of water vapor or moisture that is present in the atmosphere or any material   |       |                         |
|    | k.       | The percentage of moisture in the air compared to the total amount of moisture the air could hold at the same temperature and barometric pressure |       | <i></i>                 |
|    | l.       | The science of measuring and changing the properties of air   |       |                         |

|            | m.               | The science of heating and cooling with liquids  | 13.          | Ton of refrigeration                            |
|------------|------------------|--|--------------|---|
| •          | n:               | A chart which can be used with a straightedge  | 14.          | Ventilation -                                   |
|            |                  | to determine the square footage requirements of a collector  | 15.          | Hydronics                                       |
| 7.7.       | o.               | A substance used in refrigerating mechanisms to absorb heat in the evaporator  | 16.          | Humidity  |
| 'n         | <b>' 'D.</b>     | A liquid which combines chemically with  | 17.          | Btu   |
|            |                  | a refrigerant and causes heat to be released in<br>the process of combination  | 18.          | Relative humidity'.                             |
|            | q.               | The rating given to a material's ability to resist heat transfer   | 19.          | Infiltration                                    |
|            | r.               | Cubic feet per minute  | 20.          | Chiller   |
|            | s.               | A refrigerating effect equal to 12,000 Btuh  |              | , c   |
|            | t.               | The component in an absorption cooling unit which absorbs heat from the circulating water supply   |              | •   |
|            | temperar         | ure of the inlet water supply easier or more difficul  |              | · · · · · · · · · · · · · · · · · · ·           |
| 3.         | The mea days for | following problem concerning the concept of don temperature on a given day is 47°F; what would this specific calendar day?   | d be         | the number of degree                            |
| 4.         | factor ar        | e following problem concerning the concept of ad its application: If the heating requirement for as been established at 28,000 Btuh, and the degree blished at 1.7, what would the adjusted heating recommend. | agiv<br>eday | en solar system appli-<br>adjustment factor has |
|            |                  |  |              |   |
|            |                  |  |              |   |
|            |                  |  | •            |   |
| 5.         | Use of           | to following problem concerning the sun-chart wor the sun-chart worksheet assumes certain character of those assumptions state that the collector is   | eristic      | pproxs of a solar system;                       |
| <b>5</b> . | Use of           | e following problem concerning the sun-chart wor<br>the sun-chart worksheet assumes certain charact<br>e of those assumptions state that the collector   | eristic      | pprox of a solar system;                        |

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|               |                          |                 |                     |                                  | •                        |                | · · ·                 |         |  |
|---------------|--------------------------|-----------------|---------------------|----------------------------------|--------------------------|----------------|-----------------------|---------|--|
| Sel<br>pla    | ect tr<br>cing a         | ue sta<br>n "X" | temen               | s concerr<br>appropria           | ning rules<br>te blanks. | of th          | umb for so            | olar re | frigeration systems by   |
|               | a.                       | air a           | s it co<br>r-comp   | mes in co                        | ontact wit<br>ooling sys | h a c          | old, refrige          | erated  | ving water from the<br>surface, conventional<br>notors are adaptable |
| <del></del> - | b,                       | ·Abs            | orption             | systems                          | are not                  | adapt          | able to sy            | /stems  | using solar energy   |
|               | c.                       | For<br>usab     | econo<br>le in so   | mic reaso<br>lar system          | ns, the a                | bsorp          | tion <b>s</b> yster   | ns app  | pear to be the most  |
| 45            | d.                       | Abso            | rption              | systems c                        | urrently a               | vailab         | le include:           |         | _  |
|               |                          | 1.              | Lithiu              | ,<br><b>m-</b> bromid            | e-water un               | its            | -                     |         | •  |
|               |                          | 2.              | Water-              | ammonia                          | ab <b>so</b> rption      | n units        | <b>;</b>              |         |  |
|               | e.                       | Wate<br>othe    | r-amm<br>r types    | onia abso<br>of units            | rption un                | iits ar        | e more c              | ommer   | cially available than  |
| Cor<br>wit    | npleto<br>h <b>abs</b> o | e the o         | followi<br>n syster | ng li <b>st</b> of<br>ns.        | <b>sta</b> tements       | s conc         | erning bas            | ic cond | cepts of solar cooling   |
| a.            |                          |                 | n syste<br>pressio  |                                  |                          |                | e to an ord           |         | electrically operated  |
| b.            | refr                     | i <b>ge</b> ran | ts, suc             | rigerant li<br>n as<br>absorbent |                          |                |                       |         | onditioner, inorganic<br>absorption machine                          |
| C.            |                          |                 |                     |                                  |                          |                | hemically the comb    |         |  |
| d.            | In a is th               | lithiu<br>e     | m-bror              | nide-water                       | unit, wat                | er is tl       | he refrig <b>e</b> ça | int and | the lithium-bromide  |
| €.            | In a                     | n amr           | nonia-v             | vater unit,                      | ammonia                  | i <b>s</b> the | refrigeran            | t and w | vater is the absorbent   |
| Mat           | <b>c</b> h th            | e type          | <b>s</b> of lit     | nium≀bron                        | nid <b>e-wa</b> ter      | units          | on the righ           | nt with | their characteristics.   |
|               | 3*                       |                 |                     |                                  | •                        |                |                       |         | •  |
|               |                          |                 |                     |                                  | itacts the               |                | •                     | 1.      | Water chiller  |
|               | b.                       | Cools<br>coils  | s wate              | er which                         | contacts                 | the            | cooling               | 2.      | Air chiller  |



| 10.  |  | true statements concerning operating principles of an absorption air condition-<br>placing an "X" in the appropriate blanks.   |
|------|--|--|
|      | <u></u>                                      | a. The cycle begins when water in the liquid mixture in the generator is boiled off and superheated with solar energy at a temperature between 170 and 210°F   |
|      | <del></del>                                  | b. The superheated water vapor passes from the generator to the condenser where it is cooled to about 100°F by the cooling water from an outdoor cooling tower   |
| 1    |  | c. The vapor condenses to a liquid and is then revaporized through an expansion valve which cools the vapor-liquid mixture to a temperature of 100°F in the evaporator coils   |
|      |  | _d. The heat in the room air or water which is brought in contact with the evaporator is removed by the cooled refrigerant in the evaporator   |
|      | <del></del>                                  | e. The refrigerant then passes to the absorber where it recombines with the concentrated ammonia solution from the generator at a temperature of about 100°F   |
|      |  | _f. In this recombination process, refrigerant is released, and the water is removed by the cooling water from the cooling tower   |
|      |  | g. The dilute solution of lithium-bromide and water in the absorber flows by gravity, or is pumped back to the generator, and the cycle is repeated  |
|      | <u>,,                                   </u> | _h. Some ammonia-water systems use a recouperator as a heat exchanger to make the system thermodynamically more efficient  |
| 11.  |  | the words which best complete the following statements concerning system in a water chiller application.   |
|      |  | The absorption chiller should be situated (away from, close to) the hot water storage tank to minimize heat loss from the pipelines connected to the tank-   |
|      |  | Hot water from the top of the storage tank is pumped through the (generator, condenser) by pump (P-2) and returned to the bottom of the tank; note that the piping connection goes through the auxiliary boiler                      |
|      |  | When the (water, temperature) in the storage tank is insufficient to operate the absorption chiller, the auxiliary boiler is used to provide heat to the generator   |
| ¥ -% |  | When the auxiliary boiler is used, the three-way valve at the bottom of the auxiliary boiler circulates the return water only through the auxiliary boiler so that auxiliary energy (is, is not) used to heat the solar storage tank |
|      |  | Pump size and head depend on the (flow, heat) rate and pressure loss through the system and also the size and length of piping   |
| 1    | f.   | A wet cooling tower is needed with the absorption chiller to discharge the (water, heat) from the condenser and the absorber to the atmosphere   |



- g. The (flow, size) of the cooling tower depends on the size of the absorption machine and the wet-bulb temperature of the ambient air
- h. A pump (P-3) is needed to circulate the cooling water from the (tower, generator) through the absorber and condenser of the absorption machine
- i. Chilled water from the evaporator is circulated to the fan-coil unit to cool the air in the (cooling tower, rooms)
- 12. Solve a problem concerning evaporative cooling with rock-bed storage: Would you recommend an evaporative cooling system with rock-bed storage for an application in Phoenix, Arizona, and why or why not?
- 13. Complete a sun-chart worksheet for a specific solar application.
- 14. Size a solar collector for a combination DHW and space heating solar system.

(NOTE: If these activities have not been accomplished prior to the test, ask your instructor when they should be completed.)

# LOAD CALCULATIONS AND SOLAR COOLING UNIT III

#### **ANSWERS TO TEST**

| 1. | a. | 1.7 |   | k. | 18          |
|----|----|-----|---|----|-------------|
|    | b. | 5   |   | I. | 1           |
|    | C. | 6   |   | m. | <b>'</b> 15 |
|    | d. | 10. |   | n. | 8           |
|    | e. | 4   |   | ο. | 9           |
|    | f. | 12  |   | p. | 11          |
|    | g. | 3   |   | q. | 2           |
|    | h. | 14  |   | r. | 7           |
|    | i. | 19  |   | S. | 13 '        |
| 1  | j. | 16  | 4 | t. | 20          |

- 2. Easier, because deep wells produce water at a relatively constant temperature
- 3. 18 degree days
- 4. Somebody has made a mistake in calculating the degree day adjustment factor because it can never be more than 1.0, so the adjustment factor will have to be calculated again
- 5. No
- 6. Size it so that it supplies 100% of the heat requirements for the month of May
- 7. c,d
- 8. a. Air conditioner
  - b. Water and ammonia
  - c. Refrigerant
  - d. Absorbent
- 9. a. 2
  - b. 1
- 10. a, b, d, g
- 11. a. Close to
- f. Heat
- b. Generator.
- ı. Size
- c. Temperature
- h. Tower
- d. Is not
- . Rooms
- e. Flow
- 12. Yes, Phoenix is in a semi-arid region with cool night and low wet-bulb temperatures
- 13. Evaluated to the satisfaction of the instructor
- 14. Evaluated to the satisfaction of the instructor

# PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

#### UNIT OBJESTIVE

After completion of this unit, the student should be able to discuss features of passive solar design, how these features can be used to complement each other, and the characteristics of other passive solar concepts. The student should also be able to list the functions of components in a photovoltaic solar system, discuss basic rules for solar access planning, calculate shadow patterns, orient and landscape a model house and lot for maximum solar benefit, and build and operate a solar still. This knowledge will be evidenced by correctly performing the procedures outlined in the assignment and job sheets and by scoring 85 percent on the unit test.

#### SPECIFIC OBJECTIVES

After completion of this unit, the student should be able to:

- 1. Match terms related to passive solar and other solar concepts with their correct definitions.
- → 2. Select true statements concerning orientation for natural ventilation.
- 3. Solve a problem concerning the importance of wall-roof ratios.
- 4. Complete a list of statements concerning ways to use atriums in passive solar design.
- 5. Circle the words which best complete statements concerning the uses of earth berms in passive solar applications.
- 6. Complete a list of statements concerning entry locks and their uses in passive solar design.
- 7. Select true statements concerning greenhouses and their uses as entry locks in passive solar design.
- 8. Solve a problem concerning window shutters and their uses in passive solar design.
- 9. List six passive solar design features that function to complement each other.
- 10. Match other passive solar concepts with their characteristics.
- 11. Arrange in order the process for making photovoltaic solar cells.
- 12. State how a photovoltaic solar cell works.
- 13. Match components of a photovoltaic system with their functions.



- 14. Match terms concerning solar access with their definitions.
- 15. Complete a list of statements concerning solar azimuth and its use in solar access planning.
- 16. Select true statements concerning skyspace and its use in solar access planning.
- 17. Circle the words which best complete statements concerning rules of thumb for planning solar access.
- 18. Match basic levels of solar access with their requirements.
- 19. Select true statements concerning shadow patterns and their significance.
- 20. List three tree characteristics that must be considered in solar access planning.
- 21. Solve a problem concerning topography and its relation to solar skyspace.
- 22. Complete a list of statements concerning regulations and codes affecting solar applications.
- 23. Calculate the shadow pattern of a pole.
- 24. Demonstrate the ability to:
  - a. Orient a model house and landscape a model lot for maximum solar benefit.
  - b. Build and operate a solar still.

# PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

#### SUGGESTED ACTIVITIES

- I. Provide student with objective sheet.
- II. Provide student with information, assignment, and job sheets.
- III. Make transparencies.
- IV. Discuss unit and specific objectives.
- V. Discuss information and assignment sheets.
- VI. Discuss and demonstrate the procedures outlined in the job sheets.
- VII. Locate homes or businesses in your area that use passive solar concepts effectively, and plan a field trip to two or three of the installations; earth-sheltered homes, effective earth berms, and Thrombe walls provide good-subjects.
- VIII. Invite a local or area building inspector to discuss building codes and regulations that affect solar installations in your area.
  - IX. Have students investigate the status of solar access laws in your state and make reports in class; local state\_representatives or state senators can usually-provide this information.
  - X. Visit a local greenhouse or invite the owner of a local greenhouse to talk to the class about the value of solar energy and how it affects to the economics of greenhouse operation.
  - XI. Assign groups of students to report on other energy and conservation devices, concepts, and techniques related to solar; such information is available from the Conservation and Renewable Energy Inquiry and Referral Service, P. O. Box 8900, Silver Springs, MD 20907; this organization also has a toll free telephone, 1-800-523-2929, to answer questions about energy and conservation; special reports might include:
    - A. Wind energy
    - B. Photovoltaic energy
    - C. Bio-mass energy (wood and other nonfossil fuels)
    - D. Solar ponds
    - E. Hydro-electric energy
    - F. Ocean thermal energy
- XII. Give test.

#### INSTRUCTIONAL MATERIALS

- I. Included in this unit:
  - A. Objective sheet
  - B. Information sheet
  - C. Transparency masters
    - 1. TM 1--Passive Solar Design with Complementary Features
    - 2. TM 2--Photovoltaic System
    - 3. TM 3--Solar Skyspace Angles
  - D. Assignment Sheet #1--Calculate the Shadow Pattern of a Pole
  - E. Job sheets
    - 1. Job Sheet #1--Orient a Model House and Landscape a Model Lot for Maximum Solar Benefit
    - 2. Job Sheet #2--Build and Operate a Solar Still
  - F. Test
  - G. Answers to test.
- II. References:
  - A. Logan, Joe D. Solar Energy: Passive Systems. St. Louis, MO: Milliken Publishing Co., 1980.
  - B. The American Planning Association. Protecting Solar Access for Residential Development: A Guidebook for Planning Officials. Washington, D.C. 20402: U.S. Department of Housing and Urban Development and U.S. Department of Energy, 1979.
  - C. Solar Energy Project, General Solar Topics. Washington, D.C. 20402: U.S. Department of Energy, 1979.
  - D. Solar Energy Project, Earth Science Activities Washington, D.C. 20402: U.S. Department of Energy, 1979.
  - E. Solar Energy Project, Text. Washington, D.C. 20402: U.S. Department of Energy, 1979.
  - F. Solar Energy Research Institute. *Photovoltaics Solar Electric Power Systems*. Washington, D.C. 20402: U.S. Department of Energy, 1980.

# PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

#### INFORMATION SHEET

#### Terms and definitions

- A. Atrium--A hallway or small court usually used as an entry way
- B. Earth berm--Earth placed around exterior walls to provide protection from extreme temperature changes, heavy winds, and air infiltration; may reach to window level, or, in the case of an earth-sheltered structure, it may cover three sides and even the roof
- C. Earth contact-Structures that use ground mass temperature to help heat in winter and help cool in summer, and usually constructed with a berm that abuts but does not cover the house to leave space for window light and ventilation
- D. Entry lock-An entrance-exit area constructed with two doors so arranged that when the outside door is opened, the second interior door is closed to prevent the infiltration of outside air into the interior of the structure, and the outside door is closed before the interior door is opened to further confine infiltration to a minimum
- E. Natural orientation--The careful attention to site planning that physically places a home so it can best take advantage of local geographical, meteorological, and ecological patterns

(NOTE: This usually means south facing windows for maximum winter sunshine, and summer cooling with prevailing southwesterly winds, few or no windows facing prevailing winter winds from the northeast, and the advantageous use of deciduous trees to the south and west for summer shade and winter sunlight with evergreens north and east to shield against winter wind.)

- F. Clerestory window-A vertical window placed in a wall or a roof; it permits a patural light supply to the interior; it is frequently placed above one's line of vision
- G. Photovoltaics--The science of producing electrical current and voltage from sunlight through a conversion medium of silicon solar cells
- H. Solid-to-void ratio--The relationship of solid materials to open spaces in a storage facility; usually expressed in percentages.

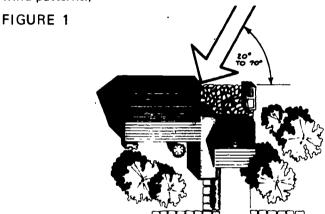
Example:

A storage facility with a 30 to 70% solid-to-void ratio means that 70% of the storage volume is occupied by solid materials and 30% of the storage volume is occupied by open or void spaces in which air can be stored or through which air can be moved



- II. Orientation for natural ventilation
  - A. Prevailing summer breezes can be used to cool a home
  - B. The ideal orientation of the side of the house through which the breezes should enter is an oblique angle 20° to 70° between the wall and wind direction (Figure 1)

(NOTE: Your local weather bureau can give you the prevailing winds in your area, and a local airport has extensive knowledge concerning local wind patterns.)



Courtesy U.S. Department of Energy

- C. Try to retain a south-facing orientation for large window areas
- D. To protect facades from winter winds, locate evergreens, fences, and earth berms on the north side of the home

(NOTE: This orientation may vary to northeast or northwest depending on prevailing winter winds.)

- E. On a south-facing hill, breezes tend to move up the hill during the day and down the hill at night
- F. Near a body of water, preezes move from the water to the land during the day, and move in a reverse pattern at night
- G. Natural ventilation and cooling can be increased by using casement-type windows or partially-opened shutters on the windward side of the house

(NOTE: Casement windows and shutters form projections which create mini-pressure zones in front of the window openings, and actually increase the velocity of the breeze passing into the openings.)



#### III. The importance of wall-roof ratios

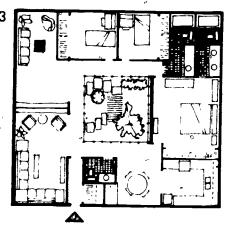
- A. During the winter months, a large amount of heat loss in a home occurs through exterior walls and particularly through and around windows and doors in those walls
- B. A rectangular house configuration increases foof area and decreases wall area; this is advantageous because it is possible to include more insulation in the roof than in the walls
- C. A rectangular house configuration also affords interior rooms with less exposure to the outside, and window area can be reduced, yet still provide major window exposure to the south (Figure 2)



Courtesy U.S. Department of Energy

### V. Ways to use atriums in passive solar design

- A. An atrium should be designed so that it is central to the other rooms in the home
- B. Windows should be exposed to the inner atrium instead of to the outside to obtain a significant reduction in heat loss through windows and walls (Figure 3)



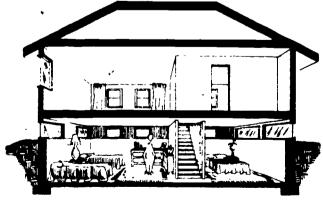
Courtesy U.S. Department of Energy



- C. Even if the atrium is unheated, the skylight will warm the atrium to a temperature higher than that outside in winter
- D. Double or triple energy savings can be experienced if the atrium is used with insulated shutters as a passive solar collector
- E. Heat gain in summer weather can be reduced if proper sun control and shading devices are used
- V. The uses of earth berms in passive solar applications
  - A. Earth-beiming and the introduction of below-grade living spaces requires careful attention to waterproofing, foundation drainage, insulation, exits and entrances, and humidity control
  - Earth-berming homes requires special attention to moisture proofing, rodents, insects, and even tree roots
  - C. Earth is usually not a good insulator; its major benefit is its capability to moderate temperature change and provide protection from cold winter winds

(NOTE: The insulating properties of earth vary with locale and application, so the general rule stated above does have exceptions.)

- D. From four to five feet below grade, earth has a relatively constant temperature of 55°F, and a duct with a small fan located in the berm can provide a simple passive cooling system
- E. When bedrooms or other living areas are located below grade, the amount of excavation need not be increased, but the first floor is raised slightly to provide a minimum 7'-6" ceiling height; this height will accommodate 2' high clerestory windows and make the below grade living areas much more liveable (Figure 4)



Courtesy U.S. Department of Energy



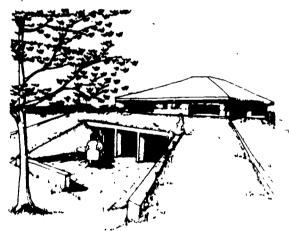
F. When conventional windows are used, say with 3' high sills, earth can be bermed to the first floor sills (Figure 5)

FIGURE 5



Courtesy U.S. Department of Energy

G. Maximum utilization of passive solar can be obtained with an earth berm that reaches to the roof eave; ventilation becomes an important concern in this design, and attention to ground water pressures and waterproofing are especially important (Figure 6)

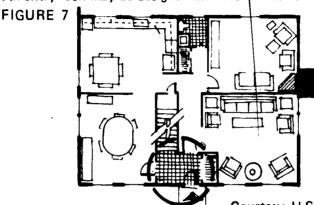


Courtesy U.S. Department of Energy

- VI. Entry locks and their uses in passive solar design
  - A. Large amounts of heated or cooled air may escape from a home each time a door is opened directly to the outside; entry locks decrease this heat loss and heat gain
  - B. An entry lock is designed to provide two doors, only one of which is normally open at any moment, separated by a small unheated or uncooled air space



C. An entry lock may be designed into the interior of the house (Figure 7)



Courtesy U.S. Department of Energy

D. An entry lock may be designed onto the exterior of the house or added to an existing house (Figure 8)

#### FIGURE 8



Courtesy U.S. Department of Energy

- VII. Greenhouses and their uses as entry locks in passive solar/design (Figure 9)
  - A. An entry lock designed as a greenhouse takes advantage of radiation through large glass areas to keep temperatures at reasonable levels, even without supplementary heating, in winter
  - B. By adding plants and other insulating and shading devices, an entry lock greenhouse can moderate heat gain in summer
  - C. An entry lock greenhouse increases the thermal resistance of the outside envelope of a house by
    - 1. Increasing the outside temperature of the main exterior wall in cold weather and decreasing it in warm weather
    - 2. Reducing infiltration losses around doors and windows



D. When so designed, an entry lock greenhouse can be utilized year round for growing vegetables and other plants



Courtesy U.S. Department of Energy

- VIII. Window shutters and their use in passive solar design (Figure 10)
  - A. Shutters must have genuine insulating value; the best shutter is one with a wood face and an insulating core
    FIGURE 10



Courtesy U.S. Department of Energy

B. Shutters should be opened in relation to sun movement (Figure 11) FIGURE 11

| Location of Shutters | Winter Opening Time  | Summer Opening Time |
|----------------------|----------------------|---------------------|
| East wall            | 8 a.m11 a.m.         | 1 p.m4 p.m.         |
| South wall           | 8 a.m4 p.m.          | 7-9 a.m.; 3-5 p.m.  |
| West wall            | 1 p.m4 p.m.          | 8 a.m11 a.m.        |
| North wall           | Any 3 daylight hours | 8 a.m7 p.m.         |

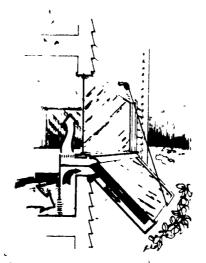
- IX. Passive design features that function to complement each other (Transparency 1)
  - A. One-story rectangular configuration
  - B. Minimum perimeter distance
  - C. Window shutters
  - D. Atrium and entry locks
  - E. Earth berming
  - F. Maximum insulation in roof and walls
  - G. Weatherstripping and storm windows

(NOTE: These features have been tested in a test situation in New York state and, in combination, have reduced heat loss by more than 30%, reduced heat gain by more than 20%, and reduced hot water costs by more than 35%.)



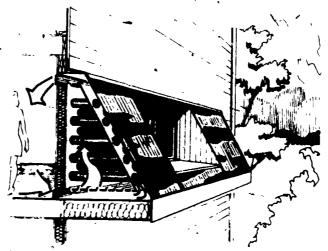
- X. Other passive solar concepts and their characteristics
  - A. Solar window shutter. This hinged shutter can be inclined to the appropriate radiation angle; it retains solar radiation and has operable vents to facilitate heat transfer into the room when the shutter is closed (Figure 12)

FIGURE 12



Courtesy U.S. Department of Energy

B. Solar window unit--This collector incorporates collection, storage, and direct venting into the room; would probably have to be used in a southeast room (Figure 13)

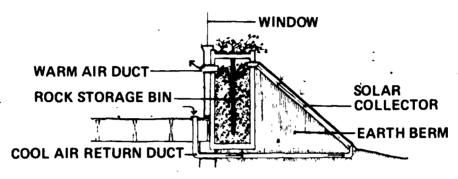


Courtesy U.S. Department of Energy



C. Solar collectors on earth berms. The berm angle should be the same as the average solar radiation angle for the locale; unit is self-contained and heat is transferred into the home by convection and by manually-operated vents (Figure 14)

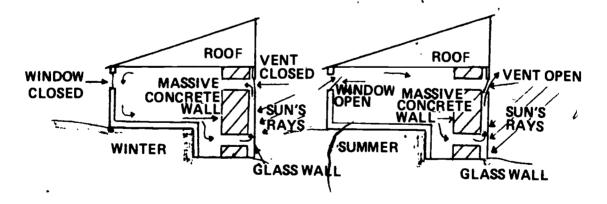
FIGURE 14



Courtesy U.S. Department of Energy

D. Thrombe, wall-A thick wall, usually of concrete or brick, that functions as a natural collector and storage area combined and takes advantage of the convection tendencies of heated air to circulate warmed air through a space (Figure 15)

FIGURE 15

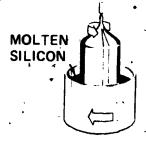


Courtesy U.S. Department of Energy



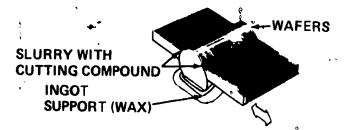
- XI. The process for making photovoltaic solar cells
  - A. Silicon crystals obtained from sand go through an extensive purification process
  - B. Silicon crystals are grown in cylindrical ingots from purified molten silicon (Figure 16)

FIGURE 16



Courtesy Solar Energy Research Institute

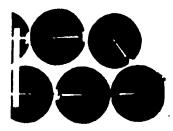
C. The cylindrical ingots are then sliced into wafers (Figure 17) FIGURE 17. ...



Courtesy Solar Energy Research Institute

D. The wafers are then connected and formed into easy to handle modules (Figure 18)

FIGURE 18



Courtesy Solar Energy Research Institute

- XII., How a photovoltaic solar cell works
  - A. When sunlight strikes the solar cell, internal electrons are energized and electricity is generated
  - B. Useful electricity is drawn off through wires attached to the cell
- XIII. Components of a photovoltaic system and their functions (Transparency 2)
  - A. Solar cells--Supply a fixed current through interconnections between modules or arrays of modules
  - B. Storage batteries—Act as buffers between the solar cell array and the load, the device using electricity; supplies power to the load during periods of insufficient sunlight and recharged during periods of high sunlight
  - C. Blocking diode-That part of the power conditioning equipment which prevents battery current from draining back into the array at night when the system is not producing power
  - D. Voltage regulator-That part of the power conditioning equipment which prevents the batteries from overcharging, a condition which shortens battery life
  - E. Inverters—That part of the power conditioning equipment which changes the direct current produced by the photovoltaic array into alternating current
  - F. Storage/backup system--An arrangement in a larger photovoltaic application whereby a local utility purchases excess electricity produced by the system during sunny days, and supplies the user with electricity during cloudy days or at hight when the system requiremente electricity than it can produce
- XIV. . Terms concerning solar access and their definitions
  - A. Solar skyspace-That portion of the sky a collector must "see" to perform effectively
  - B. Solar time-Time expressed in relation to the position of the sun in the sky
  - C. Solar noon-The time at which the sun is at its highest point in the sky

    (NOTE: Local time is often different from solar time; in other words, at solar noon the sun is at its highest point, but this time might not correspond with noon local time.)
  - D. Winter solstice-December 21; the time when the sun is at its lowest altitude in the sky and shadows are the longest
  - E. Summer solstice-Usually June 21; the time when the sun is at its highest altitude in the sky and shadows are the shortest

XV. Solar azimuth and its use in solar access planning

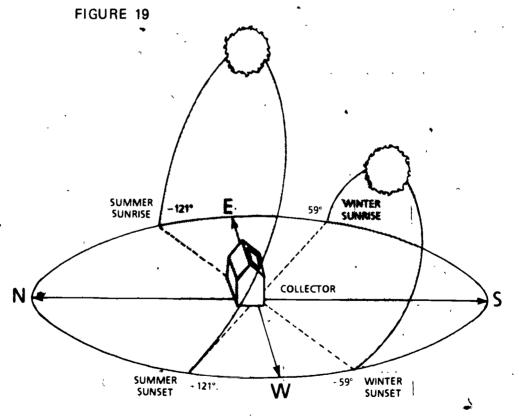
A. Solar azimuth is measured from true south, with a negative value to the east and positive value to the west

(NOTE: Do not confuse solar azimuth with true or magnetic north which is what azimuth means when used in a navigational sense.)

B. Since solar access planning involves protecting solar collectors from obstructions lying to the south of the collectors, the concept of a true south solar azimuth makes it easier to determine skyspace and analyze shading and the casting of shadows (Figure 19)

Example:

At 40 degrees north latitude on December 21, the altitude of the sun at sunrise is a large negative one, 59 degrees to the east of south, or a conventional azimuth of 121 degrees; the azimuth increases until it reaches the same positive azimuth as its negative rising azimuth, +59 degrees west of south, or a conventional azimuth of 239 degrees; in summer, the solar azimuth increases to a -121° at summer sunrise and a +121° at summer sunset

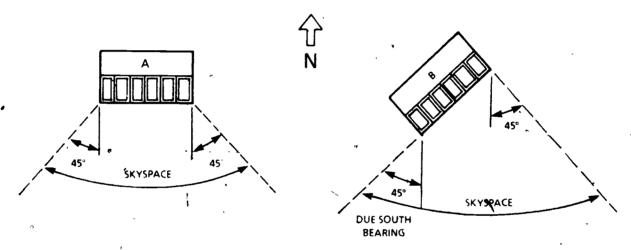


Courtesy U.S. Department of Energy

- XVI. Skyspace and its use in solar access planning
  - A. The angles of solar altitude and solar azimuth define skyspace, and it is skyspace that must be protected from shading by trees, buildings, or other obstructions
  - B. The altitude of the sun on December 21 and June 21 determines the upper and lower boundaries of needed skyspace
  - C. 45 degree solar skyspace azimuths are suitable for latitudes up to 40 degrees north (Figure 20)

FIGURE 20

Solar Skyspace (Plan View)



Courtesy U.S. Department of Energy

- D. At latitudes beyond 40 degrees north, solar skyspace\_azimuths should be 50 degrees for both a.m. and p.m. angles (Transparency 3)
- XVII. Rules of thumb for planning solar access
  - A. In most cases, it is the lowest altitude of the sun reached on December 21 that is most important for protecting solar access
  - B. On December 21, shadows are the longest, and it is usually safe to assume that if longer shadows do not shade a collector, then shorter shadows will not shade it, either
  - C. It is not necessary that solar collectors be guaranteed access to the sun from sunrise to sunset because solar altitudes below 12 degrees are essentially useless for solar energy collection purposes
  - D. It is almost impossible to maintain complete open space from horizon to horizon around a solar collector





E. The solar skyspace that must be protected is also dependent on the nature of the solar energy system being used, and the time of day and season of the year in which it is to be used (Figure 21)

### FIGURE 21

| anya <sub>t</sub> | oace and Solar Energy Use Table  |
|-------------------|--|
| Use               | Skyspace   |
| Hot Water Heating | Year-round—use lowest winter<br>and highest summer altitude to<br>determine skyspace         |
| Space Heating     | Heating season only—use lowest winter and medium spring/fall altitude to determine skyspace  |
| Air Conditioning  | Cooling season only—use mediur spring/fall and highest summer altitude to determine skyspace |

Courtesy U.S. Department of Energy

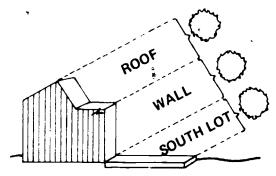
XVIII. Basic levels of solar access and their requirements (Figure 22)

- A. Rooftop protection--Protects the sunlight falling on south-facing rooftops of new dwellings and apartments constructed in a community
- B. South wall protection--Protects south walls of new construction
- C. South lot protection--Protects part of a lot adjacent to a south-facing wall

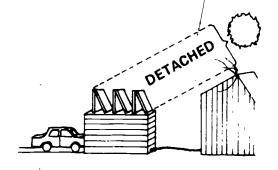


D. Detached collector protection-Protects part of a lot for use by detached solar systems

FIGURE 22



Courtesy U.S. Department of Energy



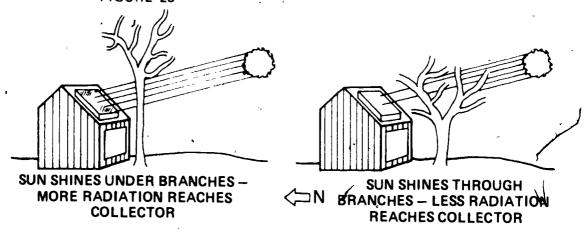
### XIX. Shadow patterns and their significance

- A. A shadow pattern is the composite shape of a shadow cast by an object over fixed solar azimuths
- B. A shadow pattern represents every spot shaded by an object during an entire time period, although only a small portion of shadow pattern will be shaded at any given time
- C. Winter shadow patterns are most valuable because they represent the worst-possible-case, and when solar access is protected in winter, it is usually protected in summer
- D. Shadow pattern data, whether collected by aerial photographs or taken in a car with a "windshield survey," should be taken at least three times; morning, noon, and afternoon on December 21
- E. Shadow patterns may be calculated by formula or by using shadow length tables

(NOTE: A sample procedure for calculating shadow patterns follows in Assignment Sheet #1.)

- XX. Tree characteristics that must be considered in solar access planning
  - A. Mature height of trees of a species
  - 8. Mature diameter of the tree crown
  - C. Seasonal variations in foliage, taking into account the distinction between deciduous species, most of which shed leaves in autumn, and evergreen or conjifers which mostly do not shed leaves

D. The distance from the ground to the crown (Figure 23) FIGURE 23

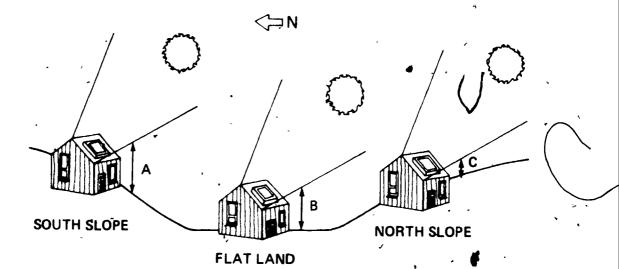


Courtesy U.S. Department of Energy

XXI. Topography and its relation to solar skyspace

- A. Changes in topography do not change solar skyspace, but it can change the distance between the ground and the lower edge of the skyspace
- B. A south slope automatically aims its collector higher, so neighboring objects can be higher without casting shadows on it
- C. A collector on a north slope will be aimed toward the crest of a hill, so even very short objects may cast shadows on the collector (Figure 24)

  FIGURE 24



DISTANCE A IS GREATER THAN B. AND B IS GREATER THAN C.

Courtesy U.S. Department of Energy



### INFORMÁTION SHÉET

### XXII. Regulations and codes affecting solar applications

- A. Solar access laws-Laws passed by state or local governments; these laws restrict the building of structures that would block neighboring sites from access to the rays of sunlight
- B. Solar easements-State or local laws which set specific space requirements for solar access in much the same manner that easements are set aside for utilities

(NOTE: A model ordinance for solar access laws and solar easements is available from HUD User, P. O. Box 280, Germantown, MD 20767.)

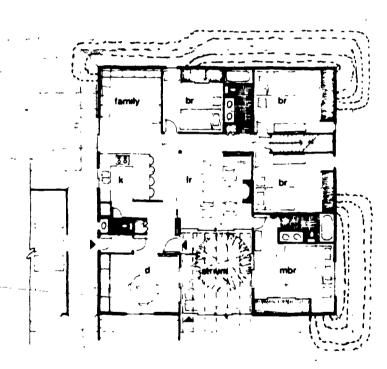
- C. State and local building codes--Codes setting up standards for plumbing, electrical, mechanical, and general structural component quality of structural materials; some codes have been modified to expressly treat solar applications and others have not; it is always best to check local codes, in particular, before starting a solar application
- D. Guidelines for solar collector installation on roofs-Since solar systems require maintenance, considerations must be given to the placement of collectors; rooftop traffic pads have to be installed so maintenance personnel can walk around the collectors, collectors must be a safe distance from the edge of the roof, and installation procedures should respect the integrity of the roof

(NOTE: These guidelines were prepared by the National Bureau of Standards and are available from the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C., 20402.)

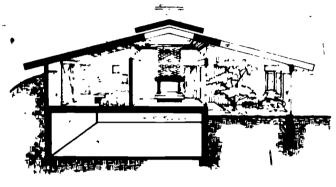




# Passive Solar Design with Complementary Features



Floor Plan



**Section** 

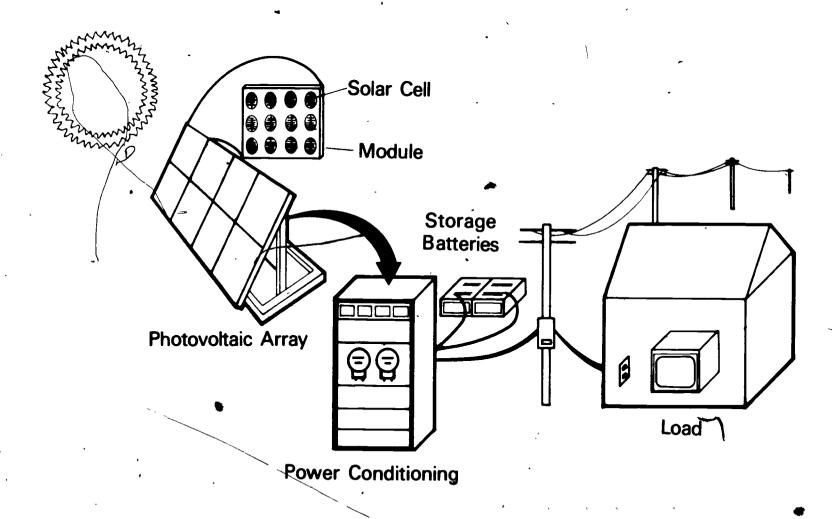


Perspective





# **Photovoltaic System**

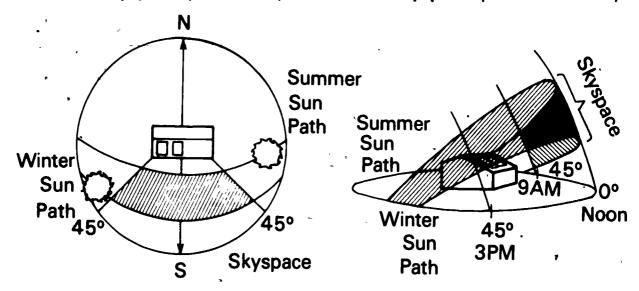


Courtesy U.S. Department of Energy

## **Solar Skyspace Angles**

Solar Skyspace (Plan View)

Solar Skyspace (Isometric View)



### Recommended Skyspace Angles for December 21st

|          | AM/PM   | Position*    | •              | Percent Percent |
|----------|---------|--------------|----------------|-----------------|
| Latitude | Azımuth | Altitude     | Noon Altitude  | Radiation***    |
| 25*      | 45*     | 25*          | 42*            | 76%             |
| 30       | 45°     | 20°          | 37°            | <b>8</b> 0% .   |
| 35•      | 45*     | 16°          | 32°            | 85%             |
| 40°      | . 45*   | 1 <b>2</b> ° | 27°            | ·               |
| 45***    | (50°)   | (12°)        |                | 88%             |
| 48***    | (50°)   | ´ (12°)      | / <b>18°</b> _ | 87%             |

The AM/PM angles presented in this chart are the same for both east of south and west of south. For example, if the skyspace azimuth is 50°, then the protected area goes from 50° east of south to 50° west of south.

Courtesy U.S. Department of Energy





<sup>\*</sup>The 50° azimuths are not based on December 21st, but are suggested as a compromise to assure solar access during the entire heating season exclusive of the winter solstice period. Similarly, the 12 degree altitudes apply only to those months when the sun's path is 12 degrees above the horizon within the 50 degree azimuth angles.

F\*\*Radiation is based on the percentage of total available radiation falling on a horizontal surface on December 21. Example: If the skyspace between 45° east of south and 45° west of south is protected at 30° latitude, then 80% of the available radiation will strike the collector if the collector is tilted, then these percentages may be even higher.

### PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

### ASSIGNMENT SHEET #1--CALCULATE THE SHADOW PATTERN OF A POLE

Directions: Use the shadow length table and the procedure in the following example to calculate and diagram shadow patterns of a pole.

DATA: Pole is 30 feet high, location is 40° north latitude, and the pole is on land that slopes to the southeast at a 10% grade; all data is for December 21

|           | Shadow Length Table for 40° North Latitude |      |      |      |      |      |     |          |      |               |      |     |     |      |     |
|-----------|--|------|------|------|------|------|-----|----------|------|---------------|------|-----|-----|------|-----|
| l<br>LATI | TUDE                                       | 40°  | _    | ٤    |      | _    |     |          |      |               |      | +-  |     |      |     |
|           |  | N    | ,    | _    | . NE |      | _   | <u> </u> | •    | <del></del> - | SE   |     |     | s    |     |
| SLOPE     | AM   | NOON | PM   | AM   | NOON | PM   | AM  | NOON     | PM   | AM            | NOON | PM  | AM  | NOON | PM  |
| 0%        | 4.8  | 2.0  | 4.8  | 4.8  | 2.0  | 4.8  | 4.8 | 2.0      | 4.8  | 4.8           | 2.0  | 4.8 | 4.8 | 2.0  | 4.8 |
| 5%        | 5.7  | 2.2  | 5.7  | 4.8  | 2.2  | 6.2  | 4.1 | 2.0      | 5.7  | 3.8           | 1.9  | 4.8 | 4.1 | 1.8  | 4.1 |
| 10% '     | 7.2  | 2.5  | 7.2  | 4.8  | 2.3  | 9.1  | 3.6 | 2.0      | 7.2  | 3.2           | 1.8  | 4.8 | 3.6 | 1.7  | 3.6 |
| 15%       | 9.6  | 2.9  | 9.6  | 4.8  | 2.6  | 16.6 | 3.2 | 2.0      | 9.1  | 2.8           | 1.7  | 4.8 | 3.2 | 1.6  | 3.2 |
| 20%       | 14.5                                       | 3.4  | 14.5 | ·4.8 | 2.8  | 97.5 | 2.8 | 2.0      | 14.5 | 2.4           | 1.6  | 4.8 | 2.8 | 1.5  | 2.8 |

STEP 1: From the above table, find the shadow length values for a.m., noon, and p.m.

STEP 2: Read the intersection of the columns labeled "SE" and "10%" as indicated on the shadow length table

STEP 3: Multiply all values by, in this case, 30, because the values given in the table are for a one-foot pole

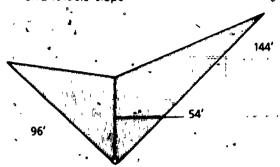
| a.m. value | x | pole height          | = | a,m. shadow length |
|------------|---|----------------------|---|--------------------|
| 3.2        |   | 30                   |   | 96 feet            |
| noon value | X | pole height          | = | noon length        |
| 1.8        |   | 30                   |   | 54 feet            |
| p.m. value | X | pole h <b>e</b> ight | = | p.m. length        |
| 4.8        |   | 30                   |   | 144 feet           |



### **ASSIGNMENT SHEET #1**

STEP 4: Scale the shadow lengths out on paper as viewed from overhead and connect the end points as shown in Figure 1

FIGURE 1 Shadow of pole on Dec 21 at 40° Latitude on a 10% S.E. Slope



45° boundaries of skyspace are used to define area of shadow that will block important sunlight.

Courtesy U.S. Department of Energy

STEP 5: Your instructor will provide you with the height of three poles in the vicinity of your classroom, and may assign actual or imagined grades to the land they are on; assume a latitude of 40° porth, calculate the a.m., noon, and p.m. shadow lengths as shown in STEP 3, and scale the shadow patterns to form diagrams as shown in STEP 4

(NOTE: Use graph paper the same size as that used by other students so that your scale diagrams can be compared with those of other students when the activity is completed.)

### PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

### JOB SHEET #1--ORIENT A MODEL HOUSE AND LANDSCAPE A MODEL LOT FOR MAXIMUM SOLAR BENEFIT

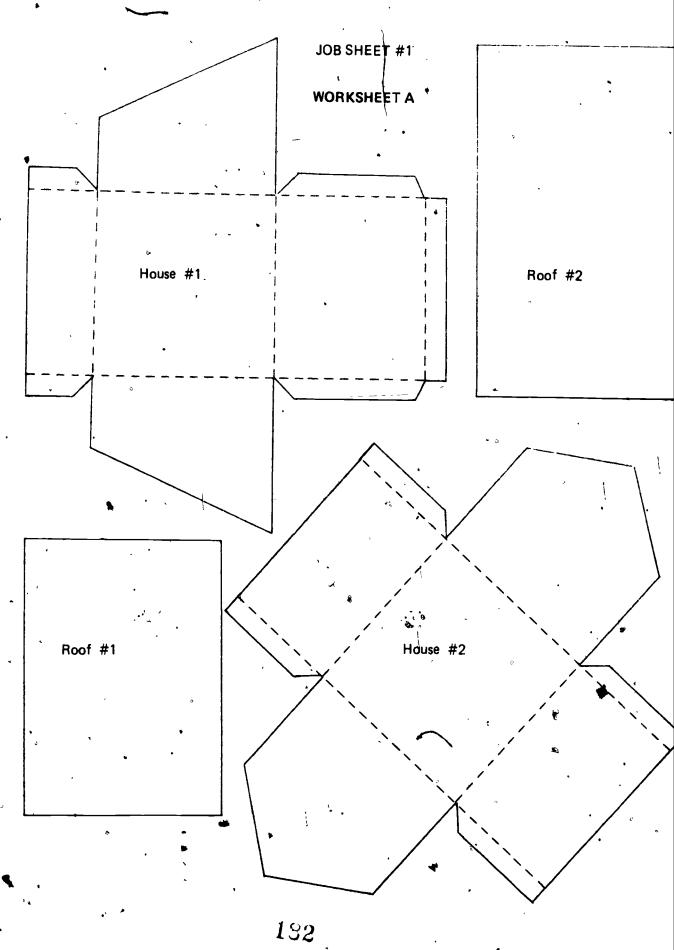
- I. Tools and materials
  - A. Scissors
  - B. Tapie
  - C. Straightedge
  - D. Worksheets A, B, and C
  - E. Lamp for light source

#### II. Procedure

- A. Cut and fold the model house in Worksheet A, and assemble it without taping
- B. Place the folded model house on the model plot plan in Worksheet B
- C. Determine the best location for room, window, and door placements
- D. Unfold the model house and draw in the windows and doors
- E. Refold the model house and tape it together
- F. Tape the roof in place
- G. Place the taped model house on the plot plan
- H. Cut out the model trees and shrubs in Worksheet C and fold the bases
- I. Tape toothpicks to the back of tree models to give them added strength
- J. Use as many tree models as you feel are necessary for the site, and tape all additional models into place as they should be in summer weather
  - (NOTE: Remember that most deciduous trees lose, their leaves in autumn.)
- K. Set the light source from the lamp at the approximate angles the sun would have in summer
- L. Check the effectiveness of summer shading on your model
- M. Remove the deciduous summer trees and replace them with deciduous winter tree models

|             | in winter   |
|-------------|---|
| Chec        | ck the effectiveness of available sunlight for your winter model  |
| Ans         | wer the following questions:  |
| 1.          | How does your model house compare to those of other students in placement of windows and doors?                     |
|             |   |
| <b>2</b> .  | In which direction should the largest roof overhang face to take advantage of winter sun while avoiding summer sun? |
|             | 4.8   |
| 3.          | If an earth berm were recommended for your model house, where would you place it?                                   |
|             | Would you place it.   |
|             |   |
| 4.          | If your model lot were on a south-facing hill, would that affect the orientation you selected?                      |
| 5.          | Explain your answer to question 42  |
| <b>.</b> 6. | If your model home site had a lake one-quarter mile due west, would   |
|             | that affect the orientation you selected?   |
| _           | that affect the orientation you selected?   |
| 7.          | •   |
| 7.          | that affect the orientation you selected?   |
|             | that affect the orientation you selected?   |





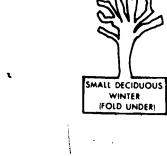
WORKSHEET B

| KEY                         |
|-----------------------------|
| <br>Fence (Indicaté Height) |
| Driveway.                   |
| Sidewalk                    |

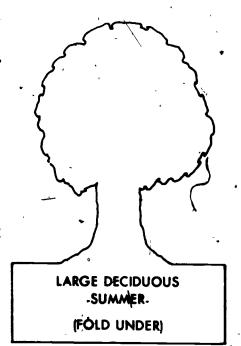


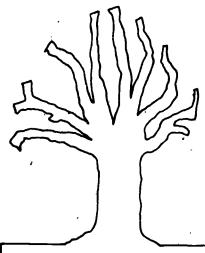






EVERGREEN (FOLD UNDER)





LARGE DECIDUOUS .
-WINTER.
(FOLD UNDER)

l 34

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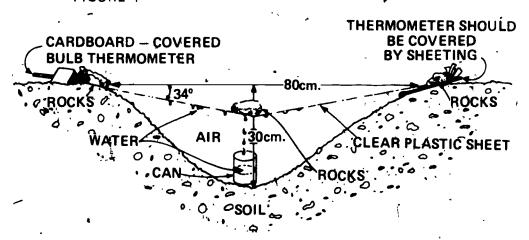
### PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

### JOB SHEET #2-BUILD AND OPERATE A SOLAR STILL

- I. Tools and materials
  - A. Strong, flexible, transparent plastic sheet at least 1m (39-inches) square (NOTE: Plastic storm window covering will do.)
  - B. Several fist-size rocks
  - C. Shovel
  - D. Two thermometers
  - E. Wristwatch or stopwatch
  - F. Piece of cardboard large enough to cover half a thermometer
  - G. Graph paper
  - H. Collecting vessel of graduated cylinder
  - I. Cobalt chloride test paper (optional)
  - J. Protractor
- II. Procedure
  - A. Dig a hole \*bout 80cm (32") in diameter and 30cm (12") deep, and place the soil to one side

B. Center the graduated cylinder or collecting vessel in the bottom of the hole (Figure 1)

#### FIGURE 1



Courtesy U.S. Department of Energy

- C. Place the plastic sheet over the hole and firmly anchor one edge with small rocks
- D. Place one small rock in the center of the plastic sheet directly over the collecting vessel, while allowing the plastic sheet to stretch to at least a 34° angle from the horizon

(NOTE: Have another student help with this step; one should manage the weighted plastic sheet while the other uses the protractor to properly attain the right angle.)

- E. Seal the other edge of the plastic sheet with soil and small rocks
- F. Insert. one thermometer under the plastic sheet with the bulb extending into the air chamber beneath the plastic sheet.

(NOTE: Be sure to position the thermometer so the scale can be read.)

- G. Place the other thermometer at the other edge of the sheet, cover the half of the thermometer with the bulb on it with cardboard, and position the thermometer so the scale can be read
- H. Simultaneously record the temperatures of both the inside and the outside thermometers at two-minute intervals

| JOB | SH          | EE | Ť | #2   |
|-----|-------------|----|---|------|
| 900 | <b>U</b> ., |    |   | TT-6 |

I. Enter your readings in the following data table:

| Reading # | Inside Thermometer | Outside Thermometer |
|-----------|--------------------|---------------------|
| 1         | •                  |                     |
| 2         | -                  | ,                   |
| 3         |                    |                     |
| 4         |                    | ,                   |
| 5         |                    |                     |
| 6         |                    |                     |
| 7         | ,                  | •                   |
| 8 .       | 1                  |                     |
| 9         | •                  | •                   |
| 10 .      | • '/               | n.                  |

| J. | Remove the | plastic s | sheet after | 20 | minutes | have i | assed |
|----|------------|-----------|-------------|----|---------|--------|-------|
|----|------------|-----------|-------------|----|---------|--------|-------|

- K. Retrieve the collecting vessel
- L. Pour the contents of the collecting vessel into a graduated cylinder and record the amount of liquid collected in milliliters (ml)
- M. Check the liquid collected to determine its identity

(NOTE: Cobalt chloride paper may be used for this test, but chances are you can identify the liquid with no great difficulty.)

- N. Fill in the hole and return the shovel and other equipment to a proper storage area
  - O. Answer the following questions:
    - 1. Where did the water come from?\_\_\_\_\_\_
    - 2. Why did the water collect on the underside of the plastic sheet?
    - 3. Why did the water drip into the collecting vessel?

| JOB SHE | ET | #2 |
|---------|----|----|
|---------|----|----|

| How did solar energy ca                          | use the still to operate?   |
|--|---|
| If you were stranded in equipment in your surviv | the desert with no water, and had the proposal gear, what would you do? |
| What do the readings in tion of a solar still?   | n your data table reflect concerning the oper                           |
|  |   |

## PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

NAME

|           | TEST   |
|-----------|--|
| Match the | e terms on the right with their correct definitions.   |
| a.        | A hallway or small court usually used as an entry way .  |
| b.        | Earth placed around exterior walls to provide protection from extreme temperature changes, heavy winds, and air infiltration; may reach to window level, or, in the case of an earth-sheltered structure, it may cover three sides and even the roof   |
| c.        | Structures that use ground mass temperature to help heat in winter and help cool in summer, and usually constructed with a berm that abuts but does not cover the house to leave space for window light and ventilation  |
|           | An entrance-exit area constructed with two doors so arranged that when the outside door is opened, the second interior door is closed to prevent the infiltration of outside air into the interior of the structure, and the outside door is closed before the interior door is opened to further confine infiltration to a minimum. |
| e.        | The careful attention to site planning that physically places a home so it can best take advantage of local geographical, meteorological, and ecological patterns  |
| •         | A vertical window placed in a wall or a roof; it permits a natural light supply to the interior; it is frequently placed above one's line of vision  |
|           | The science of producing electrical current and voltage from sunlight through a conversion medium of silicon solar cells   |
|           | The relationship of solid materials to open spaces in a storage facility; usually expressed in percentages   |

1.

- 1. Entry lock
- 2. Atrium
- 3. Photovoltaics
- 4. Natural . Orientation
- 5. Earth berm
- 6. Clerestory window
- 7. Earth contact
- 8. Solid-to-void ratio

|             |          | e statements concerning orientation for natural ventilation by placing an "X" propriate blanks.   |  |  |
|-------------|----------|---|--|--|
|             | a.       | Prevailing summer breezes can be used to cool a home  |  |  |
|             | b.       | The ideal orientation of the side of the house through which the breezes should enter is a right angle 20° to 90° between the wall and wind direction |  |  |
|             | c.       | Try to retain a north facing orientation for large window areas   |  |  |
|             |          | To protect facades from winter winds, locate evergreens, fences, and earth berms on the north side of the home  |  |  |
|             | e.       | On a south-facing hill, breezes tend to move up the hill during the day and down the hill at night  |  |  |
| -+          | f.       | Near a body of water, breezes move from the land to the water during the day, and move in a reverse pattern at night                                  |  |  |
| •           | g.       | Natural ventilation and cooling can be increased by using casement-type windows or partially-opened shutters on the windward side of the house        |  |  |
| - tn        | ese two  | conditions?   |  |  |
| ,—<br>4. Co | mplete   | the following list of statements concerning ways to use atriums in passive  |  |  |
| \$O         | lar desi | gn.   |  |  |
| a.          |          | atrium should be designed so that it is to the other ms in the home   |  |  |
| . b.        | outs     | should be exposed to the inner atrium instead of to the side to obtain a significant reduction in heat loss through windows and walls                 |  |  |
| c.          |          | n if the atrium is unheated, the will warm the atrium temperature higher than that outside in winter  |  |  |
| d.          | Dou      | Double or triple energy savings can be experienced if the atrium is used with as a passive solar collector  |  |  |
| e.          | and      | in summer weather can be reduced if proper sun control shading devices are used   |  |  |
| •           | ×        | 100   |  |  |



- 5. Circle the words which best complete the following statements concerning the uses of earth berms in passive solar applications.
  - a. Earth-berming and the introduction of below-grade living spaces requires careful attention to waterproofing, foundation drainage, insulation, exits and entrances, and (temperature, humidity)
  - b. Earth-berming homes requires special attention to moisture proofing, rodents, insects, and even (temperature change, tree roots)
  - c. Earth is usually not a good insulator; its major benefit is its capability to moder ate temperature change and provide protection from (tornadoes, cold winter winds)
  - d. From four to five feet below grade, earth has a relatively constant temperature of (65°F, 55°F), and a duct with a small fan located in the berm can provide a simple passive cooling system
  - e. When bedrooms or other living areas are located (above, below) grade, the amount of excavation need not be increased, but the first floor is raised slightly to provide a minimum 7'-6" ceiling height; this height will accommodate 2' high clerestory windows and make the below grade living areas much more liveable
  - f. When (conventional, clerestory) windows are used, say with 3' high sills, earth can be bermed to the first floor sills
  - Maximum utilization of passive solar can be obtained with an earth berm that reaches to the roof eave; (light, ventilation) becomes an important concern in this design, and attention to ground water pressures and waterproofing are especially important
- 6. Complete the following list of statements concerning entry locks and their uses in passive solar design.
  - a. Large amounts of heated or cooled air may escape from a home each time a door is opened directly to the outside; entry locks decrease this heat loss and \_\_\_\_\_\_
  - b. An entry lock is designed to provide two doors, only one of which is normally open at any moment, separated by a small unheated or uncooled
  - c. An entry lock may be designed into the interior of the house
  - d. SAn entry lock may be designed onto the exterior of the house or
- 7. Select true statements concerning greenhouses and their uses as entry locks in passive solar design by placing an "X" in the appropriate blanks.
  - a. An entry lock designed as a greenhouse takes advantage of radiation through large glass areas to keep temperatures at higher than average levels, even without supplementary heating, in winter
  - b. By adding plants and other insulating and shading devices, an entry lock greenhouse can moderate heat gain in summer



| c. An entry lock greenhouse increases the the envelope of a house by  | rmal resistance of the inside   | E        |
|---|---------------------------------|----------|
| Increasing the outside temperature of the weather and decreasing it in warm weather.  | e main exterior wall in cold    | <u> </u> |
| 2. Reducing infiltration losses around doors  | and windows                     |          |
| d. When so designed, an entry lock greenhouse of for growing vegetables and other plants  | an be utilized in the summe     | r        |
| Solve the following problem concerning window shutters are decorative, but they value; what is that value and what type of shutter would be   | / must have another genuing     | 2        |
| · · · · · · · · · · · · · · · · · · ·   |                                 | 1        |
|   | `                               | •        |
| b   |                                 |          |
| C   |                                 |          |
| d. ·  | •                               |          |
| e   |                                 |          |
| f   | · .                             |          |
| Match other passive solar concepts on the right with their of   | characteristics.                |          |
| ra. This can be inclined to the appropriate<br>radiation angle; it retains solar radiation and<br>has operable vents to facilitate heat transfer  | Solar window shutter            |          |
| , into the room when the shutter is closed  | 2. Thrombe wall                 |          |
| b. This collector incorporates collection, storage, and direct venting into the room; would probably have to be used in a southeast room  | Solar collectors on earth berms |          |
| c. The berm angle should be the same as the average solar radiation angle for the locale; unit is self-contained and heat is transferred into the home by convection and by manually-operated vents   | 4. Solar window unit            |          |
| d. Usually of concrete or brick, it functions as a natural collector and storage area combined and takes advantage of the convection tendencies of heated air to circulate warmed air through a space |                                 |          |
| all trillought a space  | `                               |          |

| Î1. | Arrange<br>sequence | in order the process for making photovoltaic solar number in the appropriate blanks.                                  | cells | by placing the correc    | t      |
|-----|---------------------|---|-------|--------------------------|--------|
|     | a.                  | The cylindrical ingots are then sliced into wafers  |       | •                        | 1      |
|     | b.                  | Silicon crystals are grown in cylindrical ingots fro  | om þ  | ourified molten silicor  | į<br>į |
| •   | c.                  | Silicon crystals obtained from sand go through process  | an    | extensive purification   | 1      |
|     | d.                  | The wafers are then connected and formed into   | ea:   | sy to handle modulés     | ì      |
| 12. | State hov           | w a photovoltaic solar cell works.  | ٠.    | •                        |        |
| •   | a                   |   |       | •                        |        |
| •   |                     |   | •     |                          | •      |
|     | b                   |   |       |                          | •      |
|     |                     |   |       |                          | •      |
| 13. | Match th            | ne components of a photovoltaic system on the ri  | ight  | with their functions.    |        |
|     |                     | Supply a fixed current through interconnections between modules of arrays of modules                                  | 1.    | 4                        |        |
| n = | b.                  | Act as buffers between the solar cell array   | 2.    | Blocking diode           |        |
| •   |                     | and the load, the device using electricity; supplies power to the load during periods of                              | 3,    | Solar cells              |        |
|     | - Same              | insufficient sunlight and recharged during periods of high sunlight   | 4.    | Voltage regulator :      |        |
|     | c.                  | That part of the power conditioning equip-  | 5.    | Storage/backup<br>system |        |
|     |                     | ment which prevents battery current from draining back into the array at night when the system is not producing power | 6.    | Storage batteries        |        |
|     | d.                  | That part of the power conditioning equip-  |       |                          |        |
|     |                     | ment which prevents the batteries from overcharging, a condition which shortens battery life                          |       |                          |        |
|     | e.                  | That part of the power conditioning equip-  |       |                          | `      |
|     | مر                  | ment which changes the direct current pro-<br>duced by the photovoltaic array into alter-<br>nating current           |       | •                        |        |
|     | 1                   | An arrangement in a larger photovoltaic   |       |                          |        |
|     | 1                   | application whereby a local utility purchases excess electricity produced by the system                               |       |                          | ,      |
| ,   | _                   | during sunny days, and supplies the user with electricity during cloudy days or at night                              |       |                          |        |
| ,   |                     | when the system requires more electricity than it can produce   |       |                          |        |

| 14,         | Match the terms concerning solar access on the right with   | their correct definitions.                             |  |  |  |
|-------------|---|--|--|--|--|
| ٠.,         | a. That portion of the sky a collector must "see" to perform effectively  | 1. Solar noon  |  |  |  |
|             |   | 2. Summer solstice                                     |  |  |  |
|             | b. Time expressed in relation to the position of the sun in the sky   | 3. Solar skyspace                                      |  |  |  |
|             | c. The time at which the sun is at its highest  | 4. Solar time  |  |  |  |
|             | point in the sky  | 5. Winter solstice                                     |  |  |  |
|             | d. December 21; the time when the sun is at its lowest altitude in the sky and shadows are the longest                            | · · · · · · · · · · · · · · · · · · ·                  |  |  |  |
|             | e. Usually June 21; the time when the sun is at its highest altitude in the sky and shadows are the shortest                      | · · · · · · · · · · · · · · · · · · ·                  |  |  |  |
| 15.         | Complete the following list of statements concerning solar access planning.   | azimuth and its use in solar                           |  |  |  |
|             | a. Solar azimuth is measured to the east and positive value to the west   | , with a negative value                                |  |  |  |
| •           | b. Since solar access planning involves protecting solar collectors, the concept of makes it easier to and the casting of shadows | ollectors from obstructions a true south solar azimuth |  |  |  |
| <b>1</b> 6. | Select true statements concerning skyspace and its use in placing an "X" in the appropriate blanks.                               | n solar access planning by                             |  |  |  |
| •           | a. The angles of solar altitude and solar azimuth skyspace that must be protected from shading b obstructions                     |  |  |  |  |
| ٥           | b. The altitude of the sun on December 31 and June 31 determines the upper and lower boundaries of needed skyspace                |  |  |  |  |
|             | c. 45 degree solar skyspace azimuths are suitable fo north  | r latitudes up to 40 degrees                           |  |  |  |
|             | d. At latitudes under 40 degrees north, solar sky 50 degrees for both a.m. and p.m. angles (Transpa                               |  |  |  |  |
| <b>4</b> 7. | Circle the words which best complete statements concerning solar access.  | ng rules of thumb for plan-                            |  |  |  |
|             | a. 'In most cases, it is the (lowest, highest) altitude of the 21 that is most important for protecting solar access              | e sun reached on December                              |  |  |  |
| ,           | b. On December (21, 31) shadows are the longest, and  |  |  |  |  |



shade it, either

|     | C.   | sun           | is not necessary that solar collectors be guaranteed<br>rise to sunset because solar altitudes below (12, 2<br>less for solar energy collection purposes | d a€<br>(2) d | ccess to the sun fror<br>degrees are essentiall | n<br>y            |
|-----|--|---------------|--|---------------|---|-------------------|
|     | d.   | ilt is<br>aro | s almost impossible to maintain complete open spacund (a solar collector, solar skyspace)  | e fro         | om horizon to horizo                            | n                 |
|     | e.   | sola          | e solar skyspace that must be protected is also deper<br>ir energy system being used, and the time of day an<br>r in which it is to be used              | nden<br>d (n  | nt on the nature of the nonth, season) of the   | e<br>e            |
| 18. | Mat  | ch ti         | he basic levels of solar access on the right with th   | eir           | correct requirements                            | š.                |
|     |  | a.            | Protects the sunlight falling on south-facing rooftops of new dwellings and apartments constructed in a community  |               | South lot protection                            |                   |
|     |  | b.            | Protects south walls of new construction   | 2.            | Detached collector protection                   |                   |
| •,  |  | c.            | Protects part of a lot adjacent to a south-<br>facing wall   | 3.            | Rooftop<br>protection                           |                   |
| L   |  | d.            | Protects part of a lot for use by detached solar systems   | 4.            | South wall protection                           |                   |
| 19. | Select true statements concerning shadow patterns and their significance by placing an "X" in the appropriate blanks.  |               |  |               |   | 1                 |
| ,   |  | a.            | A shadow pattern is the composite shape of a shad fixed solar azimuths   | ow e          | cast by an object over                          | r                 |
|     |  | b.            | A shadow pattern represents every spot shaded entire time period, although only a small portion of shaded at any given time                              | by<br>of sh   | an object during ar<br>nadow pattern will be    | )<br><del>)</del> |
|     |  | •             | Summer shadow patterns are most valuable bec<br>worst-possible-case, and when solar access is pro<br>usually protected in winter                         | ause<br>tect  | e they represent the<br>ted in summer, it is    | ;<br>;            |
|     | d. Shadow pattern data, whether collected by aerial photographs or taken in a car with a "windshield survey," should be taken at least two times; morning and afternoon on December 21 |               |  |               | )<br>   |                   |
|     |  | e.            | Shadow patterns may be calculated only by using  | ng s          | shadow length tables                            | ;                 |
| 20. | List 1   | three         | tree characteristics that must be considered in solar a  | acce          | ss planning.                                    |                   |
|     | a.   |               |  |               |   |                   |
|     | b.   | <del></del> - | <del>,                                     </del>  |               |   | ,                 |
|     | ,  |               |  |               | · .   |                   |
|     | c.   | 4             |  | ,*            | . \   |                   |



| 21. | A s                                     | ve the following problem concerning topography and its relation to solar skyspace: olar application dictates that the collector will be on a north slope aimed at the transfer of a hill; what shading and shadowing problems should be carefully considered? |  |  |
|-----|---|---|--|--|
|     |   |   |  |  |
|     |   | ,   |  |  |
| 22. |   | nplete the following list of statements concerning regulations and codes affecting rapplications.   |  |  |
|     | a.                                      | Solar access lawsLaws passed by state or local governments; these laws restrict the building of structures that would block neighboring sites from access to  |  |  |
|     | b.                                      | Solar easementsState or local laws which set specific space requirements for solar access in much the same manner that easements are set aside for  |  |  |
|     | C.                                      | State and local building codes-Codes setting up standards for and general structural component  |  |  |
|     |   | quality of structural materials; some codes have been modified to expressly treat solar applications and others have not; it is always best to check recodes, in particular, before starting a solar application  |  |  |
|     | d.                                      | Guidelines for solar collector installation on roofs-Since solar systems require maintenance, considerations must be given to the placement of collectors; rooftop have to be installed so maintenance personnel can  |  |  |
|     | •                                       | walk around the collectors, collectors must be a safe distance from the edge of the roof, and installation procedures should respect the integrity of the roof  |  |  |
| 23. | Calculate the shadow pattern of a pole. |   |  |  |
| 24. | Der                                     | nonstrate the ability to:   |  |  |
|     | a.                                      | Orient a model house and landscape a model lot for maximum solar benefit.   |  |  |
|     | b.                                      | Build and operate a solar still.  |  |  |
| =   |   | (NOTE: If these activities have not been accomplished prior to the test, ask your instructor when they should be completed.)  |  |  |

## PASSIVE SOLAR AND OTHER SOLAR CONCEPTS UNIT IV

### ANSWERS TO TEST

| 1. | a. | 2 |   | e. | 4 |
|----|----|---|---|----|---|
|    | b. | 5 | • | f. | 6 |
|    | c. | 7 |   | g. | 3 |
|    | d. | 1 |   | h. | 8 |

- 2. a, d, e, g
- 3. It is impossible to include more insulation in the roof than in the walls, and window area can be reduced, yet still provide major window exposure to the south
- 4. a. Central d. Insulated shutters b. Windows e. Heat gain c. Skylight
- 5. a. Humidity
  b. Tree roots
  c. Cold winter winds
  d. 55°F
  e. Below
  f. Conventional
  Ventilation
- 6. a. Heat gainb. Air spaced. Added to an existing house
- 7. b
- 8. Window shutters must have a genuine insulating value, and a shutter with a wood face and an insulating core would best fulfill that value
- 9. Any six of the following:
  - a. One-story rectangular configuration
  - b. Minimum perimeter distance
  - c. Window shutters
  - d. Atrium and entry locks
    - e. Earth berming
  - f. Maximum insulation in roof and walls
  - g. Weatherstripping and storm windows
- 10. a. \_1 b. '4
  - c. 3 d. 2
- . u. z
- 11. a. 3 b. 2
  - c. 1
  - d. 4

| 12. | a. | When sunlight strikes the solar cell, interi | nal electrons are energized and electricity |
|-----|----|--|---|
|     |    | is generated                                 | • .   |

- b. Useful electricity is drawn off through wires attached to the cell
- 13. a. 3
- d. 4
- b. 6
- e.

f.

- c. 2
- 14. a. 3
- d. 5
- b. 4
- e. 2
- C.
- 15. a. From true south
  - b. Determine skyspace and analyze shading
- 16. a; c
- 17. a. Lowest
- d. A solar collector
- b. 21
- e. Sea**so**n
- c. 12
- 18. a. 3
  - b. 4
  - c. 1
  - d. 2
- 19. a, b
- 20. Any three of the following:
  - a. Mature height of trees of a species
  - b. Mature diameter of the tree crown
  - c. Seasonal variations in foliage, taking into account the distinction between deciduous species, most of which shed leaves in autumn, and evergreen or conifers which mostly do not shed leaves
  - d. The distance from the ground to the crown
- 21. Even very short objects may cast shadows on the collector
- 22. a. The rays of sunlight
  - b. Utilities
  - c. Plumbing, electrical, mechanical
  - d. Traffic pads
- 23. Evaluated to the satisfaction of the instructor
- 24. Performance skills evaluated to the satisfaction of the instructor